

**Figure 1.** Schematic view of the epitaxial structure of the samples under investigation.

For optimizing the design of QD lasers and for being able to accurately characterize the presence of parasitic recombination processes, specific techniques need to be defined. At the laboratory level, it is desirable that such techniques are based on simple experimental measurements, such as, for instance,—on the analysis of optical power vs current curves, which are accessible to most laboratories.

One of the most common approaches to evaluate the nonradiative lifetime in semiconductor LDs based on simple optical measurements is the van Oopdorp method.<sup>13</sup> However, this model is incomplete since (a) it does not consider the role of Auger-Meitner recombination and (b) it is not suitable for modeling the dot-in-a-well (DWELL) structure in which carriers are supplied to QDs by a QW acting as a reservoir.

Within this paper, we propose a novel model based on rate equations that allows the evaluation of the contribution of radiative, Shockley-Read-Hall (SRH), and Auger-Meitner recombination, along with the SRH leakage component in the QWs. Such a methodology is based on the analysis of the subthreshold characteristics of QD lasers and significantly advances the state-of-the-art in this field. We demonstrate the validity of the model through the analysis of the  $L-I$  curves of QD LDs with self-assembled InAs QDs embedded in InGaAs QWs designed for 1.3  $\mu\text{m}$  wavelength emission. The results are consistent with previous reports<sup>14</sup> and indicate that the degradation is not promoted by the growth of defects inside the QDs but is rather caused by the increase in nonradiative recombination occurring in the QW.

## 2. SAMPLES UNDER INVESTIGATION

The devices analyzed within this work are state-of-the-art InAs QD LDs epitaxially grown by MBE (molecular beam epitaxy) on silicon substrates. The samples are designed for emission at 1.3  $\mu\text{m}$ . The epitaxial structure (Figure 1) is formed by a periodic active region enclosed within two GaAs wave-guiding layers and two  $\text{Al}_{0.4}\text{Ga}_{0.6}\text{As}$  cladding layers, grown on top of a  $\sim 3 \mu\text{m}$  thick GaAs buffer layer. The active region of the lasers is composed of seven equal DWELL layers, each featuring undoped GaAs barriers and a 10 nm thick Be-doped layer ( $N_{\text{A}} = 5 \times 10^{17} \text{ cm}^{-3}$ ), separated from the  $\text{In}_{0.15}\text{Ga}_{0.85}\text{As}$  well containing the layer of self-assembled InAs QDs, whose areal density is around  $5 \times 10^{10} \text{ cm}^{-2}$  (further details on the growth processes can be found in ref 15). The processing of the devices was then completed with the

etching of the 2.5  $\mu\text{m}$  wide ridge, the thinning of the silicon substrate, and the cleavage of the facets that form a 1350  $\mu\text{m}$  long Fabry-Pérot optical cavity.

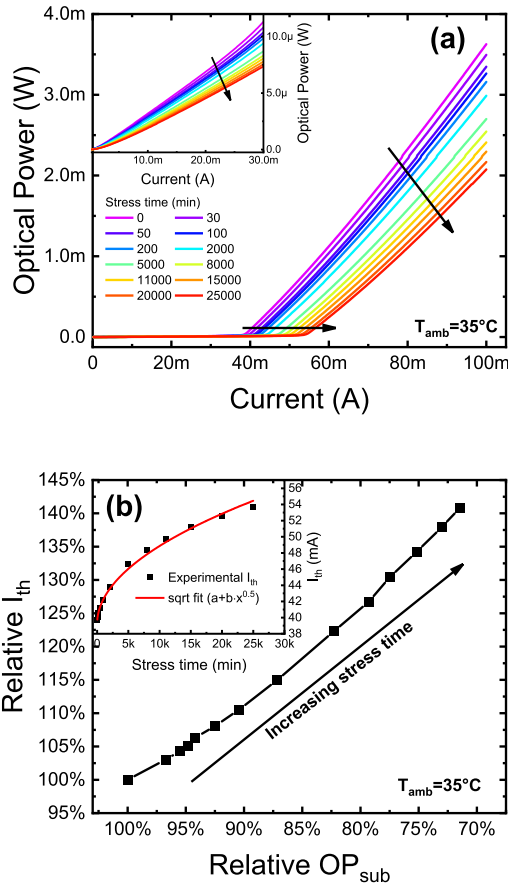
## 3. EXPERIMENTAL METHODS

For our experimental purposes, one representative device with threading dislocation density (TDD) equal to  $7 \times 10^7 \text{ cm}^{-2}$  has been stressed and characterized on-wafer. Temperature control was achieved by means of a TEC-controlled baseplate. The electrical supply was provided by a source meter, connected to the device in a four-wire (Kelvin) configuration. The optical measurements were carried out using an amplified Ge photodiode. The stress experiment was interrupted at different stages to evaluate the effects of device degradation by carrying out optical power versus current ( $L-I$ ) characterization. Both stress and characterization were carried out at a fixed baseplate temperature of  $T_{\text{AMB}} = 35 \text{ }^\circ\text{C}$ . Based on previous results on similar devices<sup>14,16</sup> (TDD =  $7 \times 10^6 \text{ cm}^{-2}$ , three QD layers), a constant stress current of 202.5 mA ( $5 \text{ kA/cm}^2$ ) was chosen in order to induce a sufficient amount of degradation in a time frame of 500 h (about 3 weeks).<sup>17</sup>

## 4. RESULTS AND DISCUSSION

**4.1. Modeling of Optical Degradation—Model Definition.** The variation of the  $L-I$  characteristics exhibited by the device during the aging procedure is shown in Figure 2a:

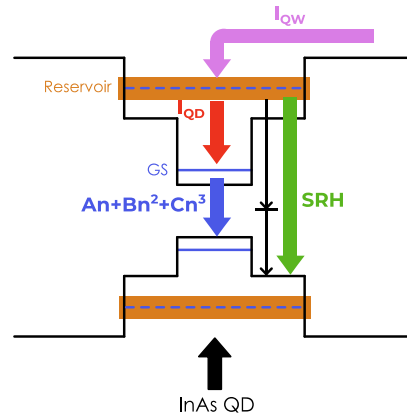
The reported curves show a decrease in the slope efficiency (SE), an increase of the threshold current ( $I_{\text{th}}$ ), and a decrease in the subthreshold emission ( $\text{OP}_{\text{sub}}$ ). The faster degradation of the optical characteristics shown in Figure 2a occurring within the first 2000–5000 min is compatible with a square root dependence on stress time (see inset of Figure 2b).<sup>16</sup> This feature suggests a diffusion process (regulated by Fick's second law of diffusion<sup>18</sup>) which can be interpreted with the migration of defects/impurities in the active region worsening the optical performance, as described in our previous study on similar devices.<sup>14</sup> Consistent with prior experiments,<sup>14,19</sup> the relative variations of  $I_{\text{th}}$  and  $\text{OP}_{\text{sub}}$  appear to be linearly correlated (Figure 2b), indicating that a common degradation process is affecting both parameters at the same time. Based on this observation, we developed a methodology for analyzing the recombination dynamics, which is based on the study of the



**Figure 2.** (a) Variation of the  $L$ – $I$  curves during the constant current stress: we can observe an increase in threshold current, a decrease in the slope efficiency, and decrease in subthreshold emission. (b) Correlation between threshold current and subthreshold emission.

optical degradation below threshold. This choice is justified by the fact that a comprehensive modeling of the optical characteristics above threshold would have strongly increased the number of fitting parameters required to describe the theoretical behavior of the device (see for example refs 20 and 21). Considering that many of these parameters cannot be experimentally or theoretically determined with reasonable accuracy, this would have ultimately increased the degrees of freedom of the model, thus, lowering the level of confidence of the results. To numerically describe the optical emission below  $I_{th}$ , we considered the simplified recombination scheme reported in Figure 3.

At first, we assumed that the input current ( $I_{QW}$ ) feeds entirely the QWs, which act as carrier reservoirs for the QDs, thus neglecting possible carrier escape/overflow processes. Carrier losses within the QWs are accounted for by a SRH recombination term, which mainly represents the effects of the nonradiative recombination centers (NRRCs) located in the InGaAs QW that subtract carriers from the reservoir.<sup>22</sup> With regard to the QDs, we consider only the ground state (GS)-related emission and recombination processes since in the subthreshold regime, the current densities are low enough to allow GS to be much more populated than ES1 (first excited state).<sup>23</sup> In Figure 3, the rate at which carriers are fed to the QD GS from the reservoir is represented by  $I_{QD}$ , whereas the recombination processes describing carrier dynamics within the QD itself are described by the coefficients  $A$  (SRH



**Figure 3.** Schematic representation of the main recombination processes occurring in the subthreshold regime: the input current feeds the InGaAs QW, which is supposed to act as a carrier reservoir for the QDs. Carrier within the QW can also be lost through SRH recombination rates taken into account.

recombination),  $B$  (spontaneous emission), and  $C$  (Auger-Meitner recombination). Also for the QDs, we do not consider any escape process. Based on previous considerations, the recombination dynamics within the system shown in Figure 3 can be represented by a set of two differential equations

$$\begin{cases} \frac{dN_{well}}{dt} = \frac{I}{qV_{well}} - \frac{N_{well}}{\tau_{nr}} - \frac{I_{QD}}{qV_{QD}} \\ \frac{dN_{QD}}{dt} = \frac{I_{QD}}{qV_{QD}} - AN_{QD} - BN_{QD}^2 - CN_{QD}^3 \end{cases} \quad (1)$$

where  $N_{well}$  is the carrier density in the QWs,  $N_{QD}$  is the carrier density in the QDs,  $V_{well}$  is the volume of the InGaAs wells,  $V_{QD}$  is the total volume of the QDs, and  $\tau_{nr}$  represents the nonradiative lifetime inside the QWs. In eq 1, the first equation represents the QW rate equation, whereas the second one describes recombination within the QDs. In steady-state conditions ( $dN_{well}/dt = 0$  and  $dN_{QD}/dt = 0$ ), we can write

$$\begin{cases} 0 = \frac{I}{qV_{well}} - \frac{N_{well}}{\tau_{nr}} - \frac{I_{QD}}{qV_{QD}} \Rightarrow \\ \Rightarrow \frac{I}{qV_{well}} = \frac{N_{well}}{\tau_{nr}} + \frac{I_{QD}}{qV_{QD}} \\ 0 = \frac{I_{QD}}{qV_{QD}} - AN_{QD} - BN_{QD}^2 - CN_{QD}^3 \Rightarrow \\ \Rightarrow \frac{I_{QD}}{qV_{QD}} = AN_{QD} + BN_{QD}^2 + CN_{QD}^3 \end{cases} \quad (2)$$

By combining the two equations, we obtain

$$\frac{I}{qV_{well}} = \frac{N_{well}}{\tau_{nr}} + AN_{QD} + BN_{QD}^2 + CN_{QD}^3 \quad (3)$$

Now we assume that the number of photons generated in the active region ( $L$ ) through spontaneous emission, per unit of time, is determined by the following relation

$$L = V_{QD}BN_{QD}^2 \quad (4)$$

Second, we hypothesize that the amount of photons emitted outside the laser per unit of time ( $L_{\text{ext}}$ ) is proportional to the rate of photons generated in the active region divided by a term called extraction efficiency ( $E$ ), which takes into account the contribution of absorption, diffraction, mode coupling, and collection losses that limit the fraction of output light that can be actually measured ( $L = L_{\text{ext}}/E$ ). The carrier density in the QDs can therefore be determined by

$$N_{\text{QD}} = \sqrt{\frac{L}{BV_{\text{QD}}}} = \sqrt{\frac{L_{\text{ext}}}{EBV_{\text{QD}}}} \quad (5)$$

By substituting eq 5 into (3), we obtain

$$\frac{I}{qV_{\text{well}}} = \frac{N_{\text{well}}}{\tau_{\text{nr}}} + A\sqrt{\frac{L_{\text{ext}}}{EBV_{\text{QD}}}} + \frac{L_{\text{ext}}}{V_{\text{QD}} \cdot E} + C\left(\frac{L_{\text{ext}}}{EBV_{\text{QD}}}\right)^{3/2} \quad (6)$$

The external quantum efficiency ( $\eta_{\text{ext}}$ ) can then be calculated as

$$\eta_{\text{ext}} = \frac{qL_{\text{ext}}}{I} = \frac{qL_{\text{ext}}}{q\left[V_{\text{well}}\frac{N_{\text{well}}}{\tau_{\text{nr}}} + V_{\text{well}}A\sqrt{\frac{L_{\text{ext}}}{EBV_{\text{QD}}}} + \frac{V_{\text{well}}}{V_{\text{QD}} \cdot E}L_{\text{ext}} + V_{\text{well}}C\left(\frac{L_{\text{ext}}}{EBV_{\text{QD}}}\right)^{3/2}\right]} \quad (7)$$

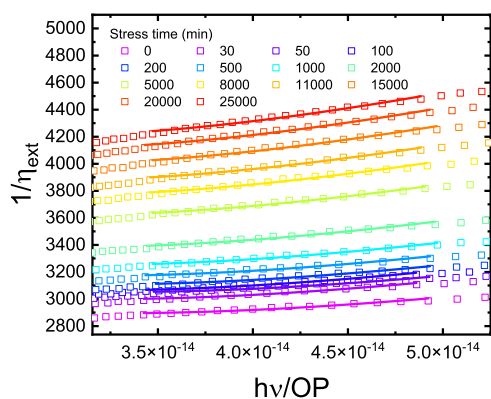
Finally, the inverse of the external quantum efficiency can be written as

$$\frac{1}{\eta_{\text{ext}}} = V_{\text{well}}\frac{N_{\text{well}}}{\tau_{\text{nr}}}\frac{1}{L_{\text{ext}}} + \frac{V_{\text{well}}}{V_{\text{QD}} \cdot E} + V_{\text{well}}A\sqrt{\frac{1}{EBV_{\text{QD}}}}\sqrt{\frac{1}{L_{\text{ext}}}} + V_{\text{well}}C\left(\frac{1}{EBV_{\text{QD}}}\right)^{3/2}\sqrt{L_{\text{ext}}} \quad (8)$$

This final equation describes  $1/\eta_{\text{ext}}$  as a function of  $1/L_{\text{ext}}$  similar to the van Opdorp method, where  $L_{\text{ext}}$  can be derived from experimental measurements by dividing the optical power of the  $L-I$  curves by the photon energy ( $L_{\text{ext}} = \text{OP}/h\nu$ ).

**4.2. Modeling of Optical Degradation—Model Validation.** Based on eq 8, we fitted the experimentally determined  $1/\eta_{\text{ext}}$  vs  $\text{OP}/h\nu$  plots acquired during the stress test. The results of the fit are shown in Figure 4:

The constraints for the fitting are listed in Table 1:



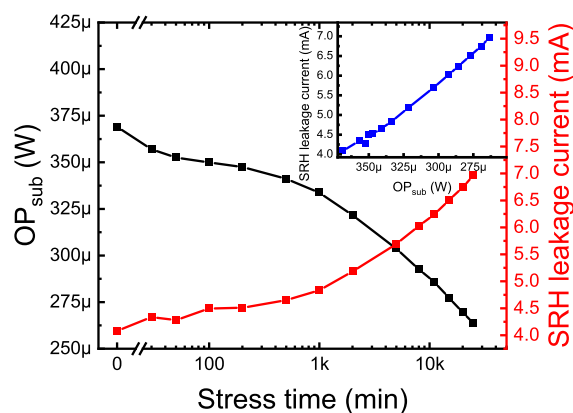
**Figure 4.** Figure shows the inverse of the external quantum efficiency as a function of the emitted optical power. The inset graph shows the fitting result for each curve collected during the stress procedure.

**Table 1.** List of Coefficients Used to Fit the Experimental  $L-I$  Curves below Threshold

parameter	value	description
$V_{\text{well}}$	$1.65 \times 10^{-10} \text{ cm}^3$	InGaAs well volume
$V_{\text{QD}}$	$4.72 \times 10^{-11} \text{ cm}^3$	InAs quantum dot volume
$A$	$1 \times 10^{-7} \text{ s}^{-1}$	InAs SRH recombination coefficient <sup>27</sup>
$B$	$1.1 \times 10^{-10} \text{ cm}^3 \text{ s}^{-1}$	InAs radiative recombination coefficient <sup>24</sup>
$C$	$1 \times 10^{-27} \text{ cm}^6 \text{ s}^{-1}$	InAs QDs Auger-Meitner recombination coefficient <sup>25,26</sup>
$E$	fitting param.	extraction efficiency
$N_{\text{well}}/\tau_{\text{nr}}$	fitting param. $\text{cm}^{-3} \text{ s}^{-1}$	SRH recombination rate (QWs)

Since QDs are sandwiched between the wetting layer and the InGaAs well, to determine  $V_{\text{QD}}$ , we assumed that in the 7 nm InGaAs well, an equivalent 2 nm layer of InAs QDs was placed in the middle of the DWELL. Actually, the real QD volume should be lower as QDs do not form a continuous layer, but from a dot to another, there is a little distance in between. In Figure 4, data were fitted from 9.5 to 13.5 mA, a bias range we opted for to evaluate the model enough below the lasing threshold, in order to avoid as much as possible the contribution of the stimulated emission to the detected light output. After calculating  $N_{\text{well}}/\tau_{\text{nr}}$  from each  $L-I$  curve, we estimated the SRH leakage current (first term of eq 8) in the QWs and compared the trend with the subthreshold emission extrapolated within the same bias range of the fitting.

Figure 5 shows that the degradation of the  $\text{OP}_{\text{sub}}$  and the increase in the SRH leakage current are linearly correlated,



**Figure 5.** Red curve represents the resulting SRH leakage current from the fit of each curve collected during the stress. The inset shows that there is a linear correlation between the degradation of the subthreshold emission and the trend of the SRH current.

indicating that the proposed model effectively describes the evolution of the  $L-I$  characteristics below threshold as the increase in QW loss current explains the radiative efficiency drop below threshold, thus reproducing the optical degradation. Despite that, if we look in more detail to the fitting results shown in Figure 4, we can see that the fitted curves tend to tilt upward for high bias currents, i.e., for high OP levels, with respect to the experimental data. This can be explained by considering that the model does not take into account the stimulated recombination: for this reason, when current is increased, the predicted increase in  $1/\eta_{\text{ext}}$  (decrease in  $\eta_{\text{ext}}$ ) due to the Auger-Meitner term (proportional to  $L_{\text{ext}}^{-1/2}$ ) is not compensated by any term related to stimulated emission. This would tilt the same curve

downward since stimulated emission is a much faster process with respect to spontaneous emission (in reasonable bias and photon-density conditions).

### 4.3. Interpretation of the Optical Degradation.

According to the proposed model, the degradation of the optical characteristics below threshold is driven by the increase in carrier losses in the QWs, possibly due to the increase in NRRCs within this region.<sup>16,19,28–31</sup> To link this behavior with the degradation of the optical characteristics above threshold, i.e., to the increase in  $I_{th}$  and the decrease in SE, we employed a second modified rate equation model to qualitatively analyze the variation of the  $L-I$  curves. The proposed model is valid for a QW laser, but the phenomenological considerations can be applied also to QD lasers.<sup>35</sup> The set of carrier and photon rate equations is the following

$$\begin{cases} \frac{dN}{dt} = \frac{\eta_{inj}I}{qV} - N(A + BN + CN^2) - g_0(N - N_{tr}) \\ \frac{dS}{dt} = \Gamma g_0(N - N_{tr}) \frac{S}{1 + EPS \cdot S} - \frac{S}{\tau_p} + \Gamma \beta BN^2 \end{cases} \quad (9)$$

where  $S$  is the photon density, and all remaining parameters are described in Table 2. We chose to adopt such values according to papers involving QD LDs in order to describe a plausible QD LD with similar characteristics to our devices.

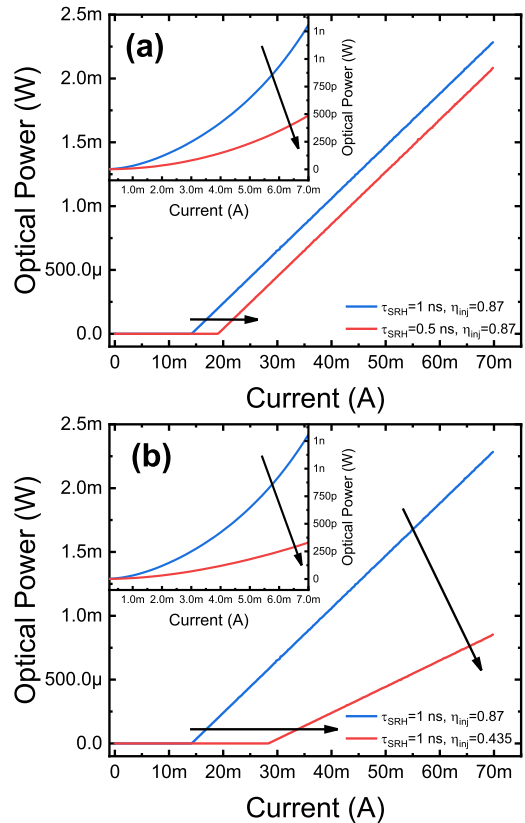
**Table 2. List of Parameters Employed to Model the Optical Characteristics above Threshold**

symbol	description	value	unit	ref.
$q$	electron charge	$1.6 \times 10^{-19}$	[C]	
$V$	active volume	$4.67 \times 10^{-11}$	[cm <sup>3</sup> ]	
$A = \frac{1}{\tau_{SRH}}$	SRH coeff.	$1/1 \times 10^{-9}$	[s <sup>-1</sup> ]	
$B$	radiative coeff.	$1.1 \times 10^{-10}$	[cm <sup>3</sup> s <sup>-1</sup> ]	24
$C$	Auger-Meitner coeff.	$1 \times 10^{-27}$	[cm <sup>6</sup> s <sup>-1</sup> ]	
$g_0$	gain slope constant	$0.926 \times 10^{-5}$	[cm <sup>-3</sup> s <sup>-1</sup> ]	36
$N_{tr}$	transparency carrier density	$1 \times 10^{18}$	[cm <sup>-3</sup> ]	37
$EPS$	gain compression factor	$1 \times 10^{-17}$	[cm <sup>3</sup> ]	36
$\Gamma$	confinement factor	0.02		38
$\tau_p$	photon lifetime	$8.56 \times 10^{-12}$	[s]	39
$\beta$	spontaneous emission factor	$1 \times 10^{-4}$		38
$\eta_{inj}$	injection efficiency	0.87		39

To incorporate the contribution of the SRH leakage current affecting the DWELLS into the simplified model described in eq 9, we included the apparent injection efficiency coefficient  $\eta_{inj}$ . In this case,  $\eta_{inj}$  can be defined as the ratio of radiative recombination rate per unit volume (i.e., the QD volume) over the rate at which carriers are injected into the device. The leakage current in the QWs is affecting the fraction of carriers being injected into the QDs; therefore, an injection efficiency term can effectively model this kind of phenomenon. To model the observed optical degradation, we simulated two distinct scenarios: (i) the increase in the SRH recombination rate in the active layers and (ii) a lowering of  $\eta_{inj}$ .

- (i) An increase the SRH recombination rate in the active layers (i.e., a decrease in the SRH lifetime) lowers the differential gain at a given bias current as the SRH

component is subtracting carriers from the radiative processes; therefore, the device will reach the threshold at higher currents. As shown by Figure 6a, this phenomenon



**Figure 6.** (a)  $L-I$  curves as a function of  $\tau_{SRH}$ : worsening of  $I_{th}$  and  $OP_{sub}$ . (b)  $L-I$  curves as a function of  $\eta_{inj}$ : worsening of  $I_{th}$ ,  $OP_{sub}$ , and SE.

can explain the worsening of the  $I_{th}$  and of the  $OP_{sub}$ , but not the decrease in SE, since this parameter should remain unaffected by the increment of the nonradiative recombination in the active layers, as the carrier density in the active layers is the same with varying the  $A$  coefficient. The demonstration that SE depends on  $\eta_{inj}$  but not on  $A$  is reported in Appendix A.

- (ii) When lowering  $\eta_{inj}$ , the carrier density in the active layers is lowered as an increasing part of the input current is lost through other nonradiative processes. Therefore, to reach lasing threshold, the device will require more current to compensate for the increased carrier losses. Since the SE is directly correlated to the external differential quantum efficiency, it represents the increment of coherent photons coming out of device per second with respect to the increment in the number of carriers injected in the laser in the same time interval. If some carriers are lost due to nonradiative processes (the QW loss in QD LDs decreases the injection efficiency inside QDs), the SE is also affected. Indeed, the SE can be defined as<sup>40</sup>

$$SE = \eta_{inj} \frac{\alpha_{mirror}}{\alpha_{mirror} + \alpha_{internal}} \frac{h\nu}{q} = \eta_{ext} \frac{h\nu}{q} \quad (10)$$

where  $\alpha_{\text{mirror}}$  and  $\alpha_{\text{internal}}$  are, respectively, the mirror and internal losses,  $q$  is the fundamental charge,  $h$  is Planck's constant, and  $\nu$  is the frequency.

Based on these considerations, and on the experimental results in,<sup>16,19</sup> the optical degradation of QD LDs has to be modeled by considering a reduction in the injection efficiency. This reduction can be ascribed to the increase in carrier losses within the DWELL, which is mainly driven by the increase of defects close to the InGaAs well,<sup>28,29,32,33</sup> which are responsible of enhancing the carrier losses affecting the QD reservoir (Figure 5). According to previous investigations, the origin of the defects contributing to the increase in SRH recombination could be related to point defects participating to the recombination enhanced growth of pre-existent misfit dislocations,<sup>28,29</sup> such as  $\text{As}_{\text{Ga}}$  or  $\text{V}_{\text{As}}$ ,<sup>16,34</sup> or, in general, to the extended defects themselves.

## 5. CONCLUSIONS

In summary, with this work, we developed a novel model that allows us to estimate the relative variation of the loss current, associated with SRH recombination in the well, during the aging of 1.3  $\mu\text{m}$  QD LDs grown on silicon by the  $L$ - $I$  characteristics below threshold. The outcome of our modeling confirmed that the optical degradation of the LDs is mainly caused by the increase in the NRRCs inside the InGaAs well. Our hypothesis is supported by the qualitative simulation of the optical characteristics above the threshold which demonstrates that the increase in the rate of SRH recombination inside QDs is not sufficient to explain the degradation of these devices, whereas lowering of the injection efficiency (which represents the increase of QW loss current) confirms the previous experimental results. The methodology proposed in this work can be useful also to QD LDs based on other materials, such as InGaN/GaN QD LDs featuring the DWELL structure.<sup>41,42</sup> Our approach can be applied as long as the degradation is dominated by lowering the injection efficiency over the decreases in the radiative efficiency in QDs.

## APPENDIX A

### Dependence of the Slope Efficiency on $\eta_{\text{inj}}$ and $A$

In this appendix, we show in which way SE is affected by  $\eta_{\text{inj}}$  and  $A$ . For the sake of simplicity, we can rewrite the first of the two equations in the system of eq 9 as

$$\frac{dN}{dt} = \frac{\eta_{\text{inj}} I}{qV} - \frac{N}{\tau} - S\nu_g g \quad (11)$$

where  $\tau$  is the reciprocal of  $A + BN + CN^2$ ,  $\nu_g$  is the group velocity, and  $g$  is the material gain. If we consider eq 11 around threshold (thus neglecting the second term on the right-hand side of the equation) in steady-state conditions, we can write

$$\frac{\eta_{\text{inj}} I_{\text{th}}}{qV} = \frac{N_{\text{th}}}{\tau} \Rightarrow N_{\text{th}} = \frac{\tau \eta_{\text{inj}} I_{\text{th}}}{qV} \quad (12)$$

Substituting  $N_{\text{th}}$  in eq 11 yields

$$\frac{dN}{dt} = \frac{\eta_{\text{inj}}(I - I_{\text{th}})}{qV} - S\nu_g g \quad (13)$$

In steady-state condition, the photon density  $S$  can be expressed as

$$S = \frac{\eta_{\text{inj}}(I - I_{\text{th}})}{qV\nu_g g} \quad (14)$$

by multiplying the photon density,  $S$ , by the energy per photon,  $h\nu$ , and the cavity volume,  $V_p$ , we obtain the stored optical energy in the cavity  $E_{\text{os}}$  ( $S \cdot h\nu \cdot V_p$ ). Then, by multiplying  $E_{\text{os}}$  by the energy loss rate through the mirrors  $\nu_g \alpha_m = 1/\tau_m$ , which is the product of the group velocity and the mirror losses, we obtain the optical power output from the mirrors

$$P_{\text{out}} = \frac{h\nu S V_p}{\tau_m} \quad (15)$$

Finally, the SE can be obtained from the derivative of the output power with respect to the current

$$\begin{aligned} \text{SE} &= \frac{dP_{\text{out}}}{dI} = \frac{d}{dI} \left( \frac{h\nu S V_p}{\tau_m} \right) \\ &= \frac{d}{dI} \left( \frac{h\nu V_p \eta_{\text{inj}} (I - I_{\text{th}})}{\tau_m qV\nu_g g} \right) = \frac{h\nu V_p}{\tau_m} \frac{\eta_{\text{inj}}}{qV\nu_g g} \end{aligned} \quad (16)$$

From this last equation, we can notice that the SE does not depend on the carrier lifetime  $\tau$ , accounting for the values of the ABC coefficients, which impacts on the value of  $I_{\text{th}}$ .<sup>40</sup> Therefore, eq 16 shows that SE depends on  $\eta_{\text{inj}}$  but not on  $A$ .

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## Notes

The authors declare no competing financial interest.

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