# Optimal Modulation of Triple Active Bridge Converters by an Artificial-Neural-Network Approach 

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#### Abstract

-lsolated multi-port converters can host loads and sources at different power and voltage levels to their ports by a single topology, giving potential merits in terms of power density and efficiency. However, the higher the number of ports, the higher the number of degrees of freedom in the modulation patterns. This high number of modulation variables complicates the optimization problem, making closed-form solutions impractical. This paper avoids the analytic solution to the optimization problem by proposing a data-driven solution. The presented approach is based on an artificial neural network (ANN) trained to minimize the rms value of the currents flowing through the switches and the transformer windings of a triple active bridge (TAB) converter. This minimization is achieved by determining suitable values of the duty-cycles for modulating the converter switches. The proposed ANN-based modulation is validated considering an experimental TAB prototype rated 5 kW .


Index Terms—Artificial neural network (ANN), multi-port converter, triple active bridge (TAB).

## I. Introduction

Isolated multi-port converters (IMPCs) present advantageous features for interconnecting loads or energy resources operating at different voltage and power levels while providing galvanic isolation between the ports and high power density [1], [2]. Applications of IMPCs can be found, for example, in electrified vehicles [3], electrified aircraft [4], [5], and in nanogrids [6] and microgrids [7], [8]. A common IMPC topology is the triple active bridge (TAB) converter, shown in Fig. 1(a) [9], [10]. The TAB consists of three full bridges with active switches (i.e., transistors), hence the name, connected through a three-winding high-frequency transformer.

To control the power flow among the ports, phase-shift modulation (PSM), shown in Fig. 1(b), is commonly applied, as done with dual active bridge (DAB) converters [11], [12]. With PSM, the three bridges generate ac voltages $v_{1}, v_{2}$, and

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Fig. 1: (a) Triple active bridge converter; (b) phase-shift modulation; (c) penta phase-shift modulation with modulation variables $\phi_{2}, \phi_{3}, D_{1}, D_{2}, D_{3}$ highlighted.
$v_{3}$ with duty-cycle fixed at $50 \%$ and variable phase-shifts $\phi_{2}$ and $\phi_{3}$. By controlling the phase-shifts magnitude and sign, it is possible to regulate the power flow intensity and direction, respectively [9]. PSM is simple and allows low switching and conduction losses at moderate to high load conditions, while operating with dc voltages such that $V_{1}: V_{2}: V_{3}=n_{1}: n_{2}: n_{3}$. Differently, at light-load conditions or with significant voltage mismatches among the transformer terminals, transformer rms currents increase with the possibility of losing zero voltage switching (ZVS), dramatically increasing switching and conduction losses relative to the transferred power [13]. Penta phase-shift modulation schemes, shown in Fig. 1(c), overcome these drawbacks [13]. By these approaches, the modulation exploits not only the phase-shifts $\phi_{2}$ and $\phi_{3}$ but also the duty-cycles $D_{1}, D_{2}, D_{3}$. The increased number of modulation variables significantly increases the complexity; controlling five modulation parameters gives a total number of possible switching patterns in the order of hundreds [12]. Tackling and analyzing each switching pattern separately to find the optimum operation, for example, in terms of losses, is timeconsuming or even impossible.
The literature reports different approaches pursuing efficiency optimization of the converter utilizing penta phase-shift modulation [13]-[21]. Based on the current literature, the most critical limits are $i$ ) the heavy mathematical analyses needed
for the modeling of the TAB, ii) the inevitable mismatch among the obtained models and the actual converter operation, which impairs the results of off-line searches based on converters models, $i i i$ ) the use of large and complex multidimensional look-up tables, and $i v$ ) the time-consuming searches, localminima issues, and low effectiveness during transients typical of on-line optimization methods.

In this context, data-driven approaches may overcome the mentioned limits [22]. In particular, the application of artificial neural networks (ANNs) in power electronics can be found in the literature, aiming at different purposes, such as, model predictive controllers [23], [24], fault diagnostic and management [25], optimal design of converters [26], [27], and efficiency-optimized modulation [28]-[30]. According to [31], ANN approaches emerge as promising tools when considering complex problems including non-linearities and uncertainties. Besides, ANNs can implement continuous non-linear maps between multiple inputs and outputs. For example, in [28], an ANN model is built for an interleaved boost with coupled inductors converter, showing its merits over a look-up table from the point of view of memory usage. Such an advantage is expected to be even more appreciable with the additional degrees of freedom of a TAB. In [29], based on simulation data, an ANN is trained to provide the peak current in the highfrequency transformer of a DAB converter. Then, to minimize the peak current stress of the DAB, the optimum duty-cycles are derived through a particle swarm optimization algorithm using a map implemented by an ANN. Differently, herein, the additional complexity of the TAB converter is tackled using an ANN that directly maps the operating points into the corresponding duty-cycles that allow to minimize the total rms current of the converter. This is done by avoiding mathematical modeling and control techniques. Besides, no applications of ANN for TAB modulation were found in the literature.
In this paper, an ANN approach is proposed for computing the optimum modulation parameters $D_{1}, D_{2}$, and $D_{3}$ for a TAB converter, given the operating conditions in terms of operating voltages and power flows. Optimality is measured in terms of total rms currents at the transformer ports. The ANN is trained off-line by exploiting the results from a systematic search of the optimal modulation parameters. This search is performed considering a simulation model calibrated to match the operation of the actual experimental TAB prototype.

The proposed approach details, implementation, and experimental verification are discussed in the following.

## II. Proposed ANN-Based Approach

The proposed approach consists in training an ANN to calculate the suitable modulation parameters for achieving optimal converter operation. The function to be optimized can have different expressions, including, for example, the overall converter efficiency, the switching and conduction losses of the power semiconductors, etc. Independently of the function adopted, the proposed approach can be used. For the sake of simplicity, the function considered in the following is the rms current on the active devices, that is, the focus is on rms current minimization, pursuing reduced converter conduction losses.

Specifically, the considered measurement for optimization is the total rms current defined as:

$$
\begin{equation*}
i^{r m s}=\sqrt{\sum_{p=1}^{3} r_{p}\left(i_{p}^{r m s}\right)^{2}}=f\left(\phi_{2}, \phi_{3}, D_{1}, D_{2}, D_{3}\right) \tag{1}
\end{equation*}
$$

where $r_{p}, p=1, \ldots, 3$, are the equivalent path resistances of the respective $p$-th port. Notably, the total rms current depends on five modulation parameters, as mentioned in Sec. I.

Solving this complex non-convex function to find the minimum total rms current is challenging [16]. Herein, this complexity is overcome by a data-driven approach, exploiting the information collected from a simulation model to compute the optimal TAB modulation parameters for rms current reduction.

The presented ANN approach consists of four steps:

1) validation of the simulation model and collection of the data-set, in Sec. III;
2) definition of the ANN structure, in Sec.IV;
3) training of the ANN based on the collected data, in Sec. V;
4) validation on the experimental prototype of the obtained results, in Sec. VI.
The aimed ANN has four inputs, representing the operating point of the TAB, and three outputs, which are the corresponding optimum duty-cycles $D_{1}, D_{2}$, and $D_{3}$. The four inputs are the port- 2 and port- 3 dc voltages and powers, $V_{2}, V_{3}$, $P_{2}$, and $P_{3}$, respectively. The other modulation parameters $\phi_{2}$ and $\phi_{3}$ are adjusted by a couple of proportional-integral regulators to provide closed-loop control of $V_{2}$ and $V_{3}$ (see, e.g., [21]). Remarkably, given the operating point, the solution to the optimization problem associated with (1) is unique.
As a final note about the defined control scheme, the phaseshifts are used to regulate the power flow between the ports, which determines the dc output voltages across the loads connected at the ports; whilst, the duty-cycles are modulated for optimizing the converter operation. The control organization is analogous to others described in the relevant literature for the DAB [11], [12] or the TAB [13]-[21] converters.

## III. Data-set Generation for ANN Training

The proposed approach involves training an ANN to map the operating point to desired modulation parameters $D_{1}, D_{2}, D_{3}$. The mapping is based on a data-set, which can be generated in different ways [13]-[21]. Herein, the data-set was generated in simulation considering a PLECS model of the TAB converter and considering the target of minimizing rms currents, as done in [29]. Remarkably, the same approach can be applied using a data-set generated considering different targets, like, for example, efficiency optimization. If efficiency optimization is considered, the data-set can even be generated on-line on the real converter, as done, for example, in [21]. These latter works may be used to generate the data-set to be considered within the scope of Sect. III-B. Sect. III-A describes the validation of the simulation model confronted with the actual converter. Sect. III-B describes the collection of the data-set for the training of the ANN.


Fig. 2: Verification of the simulation model confronted with the experimental prototype considering several test points.


Fig. 3: Deviations between simulation and experimental results.

## A. Model Validation

First, the simulation model has been calibrated and validated, considering parameters including transformer leakage inductance, switching frequency, deadtime, etc. The process aims at matching the simulation models with the experimental prototype in terms of transformer rms currents and instantaneous current and voltage waveforms, at various test points. Fig. 2 verifies the matching between simulation and experimental waveforms of transformer currents $i_{2}$ and $i_{3}$, while Fig. 3 shows the rms current deviation for the test cases, all presenting maximum deviation below $10 \%$.

## B. Data Collection

Second, a systematic, brute-force (BF) search (i.e., grid search) is run on the duty-cycles $D_{1}, D_{2}$, and $D_{3}$, changing each duty-cycle from 0.15 to 0.50 with a fixed step of 0.05 . Finer duty-cycles steps may be used for higher resolution datasets; on the other hand, this would increase the number of

(b)

Fig. 4: BF search simulation results: (a) optimum duty-cycles; (b) total rms current for different grid search granularities.
required simulations. An advantage of using the BF search, applied in simulation or experimentally, is that it is not affected by local minima, which may be a potential issue in the solution of the non-convex problem of minimizing (1). Fig. 4 illustrates the BF search simulation results with a step size of 0.05 and 0.01 . The maximum deviation between the obtained rms currents with the two different step sizes is below $1.5 \%$. The difference between the two currents is negligible, but the use of a finer resolution, from 0.05 to 0.01 , implies a number of simulations that increases from 512 to 46,656 points, for each power and voltage set point.

Considering a reasonable number of simulations for each set point, 0.05 duty-cycles step is used in the BF search. Phaseshifts $\phi_{2}$ and $\phi_{3}$ are adjusted by employing two separate linear regulators. The BF search, which finds duty-cycles giving minimum total rms current, is repeated for about 15,000 setpoints of different ports voltages and powers. Those points cover the power range from $1 \%$ to $100 \%$ of the rated power at port-2 and 3, with voltage levels spanning the range $80 \%$ to $120 \%$ of the rated ports voltages. The 15,000 records collected from the BF search constitute the data-set eventually used to train the ANN, as shown next.

## IV. ANN Basics and Design

Among various kinds of ANNs [32], the multilayer perceptron neural networks (MLP-NNs) are considered in this work. In MLP-NNs, the neurons are divided into layers that are typically fully connected. When the relationship between inputs and outputs is a non-linear static function, the MLP-NN is the most suitable architecture of ANN [33].

The essential elements in a MLP-NN are [34] i) the number of layers, ii) the number of neurons in each layer, iii) the activation function of each layer, $i v$ ) the algorithm used during the training process. There are at least three layers: the input,


Fig. 5: MLP-NN with $n$ inputs, $q$ hidden layers $p$ neurons each, and $m$ outputs.
the output, and the hidden layers in between. Commonly, the higher the problem's complexity (i.e., the complexity of the function to be estimated), the higher the number of neurons and hidden layers required.

Fig. 5 displays a standard configuration of MLP-NN, with $n$ inputs, $q$ hidden layers with $p$ neurons each, and $m$ outputs. The linear combination of the inputs of a neuron is processed through a so-called activation function, giving the neuron's output. The ability of an ANN to fit non-linear problems is provided by the use of non-linear activation functions. Among different types of activation functions [35], in this work, the sigmoid activation function is used for all the layers. A comprehensive evaluation of various activation functions commonly utilized in MLP-NNs, including sigmoid, rectified linear unit (ReLU), and hyperbolic tangent (tanh), was carried out too. The sigmoid function for all the layers of the ANN provided the lowest error values during the ANN development described in Sec. V.

The development of an ANN aims to find the hyperparameters. In machine learning, the hyperparameters are the variables that determine the network structure (e.g., number of layers and neurons, activation function) and its training procedure (e.g., learning rate). Hyperparameters are set before training and they need to be adapted if performance, in terms of estimation error, is insufficient.

The development of an ANN is divided into three stages:

1) Preliminary operations: the given data-set is split into portions for training ( $\simeq 80 \%$ ), validation $(\simeq 10 \%$ ), and test $(\simeq 10 \%)$. The data-set is partitioned randomly to guarantee homogeneity between the different portions. Training data are used for the learning phase, validation data are used for testing the generalization capability of the network during the training process, and the test data are used for performance assessment. The data-set is commonly normalized; in our case, between 0 and 1.
2) Training: the backpropagation algorithm for updating the network weights and biases is applied $n$ times, with $n$ the number of epochs. The training ends when the loss function, the mean squared error (MSE) herein, stops decreasing. The validation data-set is used to detect over/under-fitting.
3) Performance evaluation: the test-set is evaluated and the obtained output compared with the data-set output. If the performances of the ANN, in terms of error, are not

TABLE I: Hyperparameters used for training.

| Parameter | Value | Parameter | Value |
| :--- | :---: | :--- | :---: |
| Optimizer | Adam | Batch Size | 256 |
| Learning Rate | 0.01 | Activation Function | Sigmoid |
| Loss Function | MSE | Number of parameters | 883 |
| Epochs | 2000 | Training time | 15 s |

sufficient, the ANN hyperparameters should be updated.

## V. ANN Development for Optimal Modulation

Several deep learning frameworks and libraries are available, like, for example, Matlab Deep Learning, TensorFlow, PyTorch. Herein, the ANN is developed on Keras TensorFlow 2.6 on an Intel i9-12900KF CPU with 32 GB of RAM. With this setup, the average training time is less than 20 s .

Being not possible to determine a-priori the number of hidden layers or neurons needed in each layer, a systematic, BF exploration is adopted. As a design choice, the maximum number of layers $q_{\max }$ was set to 4 and the number of neurons per layer constrained between $p_{\min }=5$ and $p_{\max }=40$. Tab. I lists the used hyperparameters. The initial weights of the network are chosen randomly, and the entire training process (i.e., data splitting, training, and computation errors) is repeated three times to avoid non-optimal solutions resulting from specific unfavorable initial conditions.

To compare the different ANN architectures, the metrics mean absolute percentage error (MAPE) is used:

$$
\begin{equation*}
\operatorname{MAPE}_{i}(\%)=\frac{100}{K} \sum_{k=1}^{K} \frac{\left|D_{k, i}-\hat{D}_{k, i}\right|}{D_{k, i}} \tag{2}
\end{equation*}
$$

where $D_{k, i}$ is the estimated $i$-th duty-cycle, $\hat{D}_{k, i}$ is the $i$-th true duty-cycle, with $i \in\{1,2,3\}$, and $K$ is the dimension of the test-set. The metric is computed on the test data-set. Other metrics including the root mean square error (RMSE), and mean absolute error (MAE) were also considered during the process, bringing equivalent conclusions in the comparison.

The best results were obtained with an ANN with $q=4$ layers and 40,40,30, 10 neurons, respectively, providing an MAPE of $2.64 \%$; this solution involves 2,283 parameters for its implementation. A sub-optimal solution, whose performance in terms of MAPE displayed in Fig. 6, was obtained with $q=3$ and 20,20 , and 15 neurons, respectively. This last solution sports an MAPE of $2.85 \%$ and involves 883 parameters for its implementation. On this basis, this last, smaller network is deemed to provide the most convenient trade-off between accuracy and complexity and was chosen for deployment.

Fig. 7 shows the performance of the developed ANN. In Fig. 7(a), $P_{3}$ is constant at 500 W and $P_{2}$ varies from zero to nominal power, in Fig. 7(b), $P_{2}$ is constant and $P_{3}$ varies; voltages $V_{2}$ and $V_{3}$ are fixed. Solid lines represent the ANN output, dashed lines the results from the BF search. These latter present values on a discrete set because the BF search was performed with a duty-cycle quantization of 0.05. Remarkably, Fig. 7-displaying in (a)-(b) the duty-cycles as a function of the power at one port while keeping the other variables


Fig. 6: Errors as a function of number of neurons in $\mathrm{HL}_{1}$ and $\mathrm{HL}_{2}$, in (a) with two hidden layers and in (b) with 15 neurons on the third hidden layer.
composing the operating point constant-shows seemingly linear relations. Still, the overall relationship between the operating point $V_{2}, V_{3}, P_{2}, P_{3}$ and the duty-cycles is highly non-linear, as illustrated in Fig. 8.

The duty-cycle quantization in the BF search may cause sharp variations in the optimum parameters $D_{1}, D_{2}$, and $D_{3}$ because the optimization problem is non-convex with multiple local minima [16]. An example is visible in Fig. 7(b) around $P_{3}=2 \mathrm{~kW}$. Such abrupt variations with positive and negative slopes may originate detrimental effects in closed-loop control, like limit-cycle oscillations, and should be avoided. Instead, the ANN with the used sigmoid activation function inherently smooths the input-output relation, with a negligible impact on the resulting rms currents. To show this, PLECS simulations were run for the same points reported in Fig. 7(a) and (b) to evaluate the difference in terms of obtained rms currents by the duty-cycles from the BF search and the ANN. Fig. 7(c) shows that the difference is less than $5 \%$ for $95 \%$ of the test cases.

Fig. 8 shows a three-dimensions surface of the optimum three duty-cycles under the same voltage levels; this representation highlights better the complexity of the problem tackled by the ANN approach.

The performance of the ANN model are now evaluated in terms of MAPE as a function of the number of data points composing the data-set. The initial data-set of 15,000 operating points is gradually reduced by removing random points, finally leaving only 750 points for ANN development, that is, $5 \%$ of its initial size. The ANN architecture and the partitioning of the data-set into training, validation, and testing subsets are kept unchanged. The error at each decimation level is obtained by averaging the resulting MAPE over ten independent tests to limit the variability due to the random choices in the decimation and in the training. Fig. 9 displays the obtained results. Notably, the measured MAPE show only small increments up to a decimation of $\approx 60 \%$ of the initial size.


Fig. 7: ANN versus brute-force results. (a) $\mathrm{V}_{2}=400 \mathrm{~V}$, $\mathrm{V}_{3}=320 \mathrm{~V}, \mathrm{P}_{3}=500 \mathrm{~W}$; (b) $\mathrm{V}_{2}=400 \mathrm{~V}, \mathrm{~V}_{3}=320 \mathrm{~V}, \mathrm{P}_{2}=500 \mathrm{~W}$; (c) percentile of the test cases against rms current deviation.


Fig. 8: Duty-cycles as a function of power with $\mathrm{V}_{2}=320 \mathrm{~V}$ and $\mathrm{V}_{3}=400 \mathrm{~V}$.


Fig. 9: Effect on the MAPE as a function of the data-set size.


Fig. 10: Laboratory experimental setup with TAB prototype.

## VI. Experimental Validation

## A. Experimental Setup

The proposed ANN-based approach has been verified experimentally using the laboratory prototype displayed in Fig. 10, whose parameters are listed in Tab. II. The leakage inductances were designed to provide the nominal power at about $35^{\circ}$ phase shift [13], [36]; the phase-shifts were constrained to limit the values of peak and rms currents through the components (e.g., switches) [11], [36]. Fig. 11 illustrates the converter prototype structure, where port- 1 of the TAB converter is connected to a fixed dc power supply at rated voltage $V_{1}=400 \mathrm{~V}$, and port-2 and port-3 are connected to corresponding dc electronic loads. The ANN model and the converter control and modulation

TABLE II: Experimental Prototype Parameters

| Parameters |  | Value |
| :--- | :---: | :---: |
| Nominal power at each port $P_{\text {rated }}$ | kW | 5 |
| Switching frequency $f_{S}=1 / T_{S}$ | kHz | 40 |
| Rated dc voltages $V_{1}=V_{2}=V_{3}$ | V | 400 |
| Transf. turns ratio $n_{1}: n_{2}: n_{3}$ |  | $1: 1: 1$ |
| Transf. leakage inductances: |  |  |
| Port-1 leakage inductance $L_{1}$ | $\mu \mathrm{H}$ | 40 |
| Port-2 leakage inductance $L_{2}$ | $\mu \mathrm{H}$ | 47 |
| Port-3 leakage inductance $L_{3}$ | $\mu \mathrm{H}$ | 41 |
| Dead time | $\mu \mathrm{s}$ | 1 |
| Switching Devices | MMIX1Y100N120C3H1 |  |



Fig. 11: Structure of the experimental setup.
are deployed on an Imperix B-Box RCP controller driving six Imperix PEB8032-A half-bridges. Fig. 11 shows the clocking logic in the digital controller. The analog-to-digital conversion, PI control, and modulators are executed at the switching frequency (i.e., 40 kHz ). The ANN, which performs a secondary optimization process, can be run at a slower pace to conserve computational resources. Herein, the ANN is executed at a rate of 10 kHz . Anti-aliasing low-pass filters (LPF) are used at the interface with the ANN inputs.

The optimum five modulation variables corresponding to the actual operating point are generated as follows. The ANN computes the duty-cycles $D_{1}, D_{2}$, and $D_{3}$ based on the operating point $V_{2}, V_{3}, P_{2}, P_{3}$, given as input to the ANN. The duty-cycles are expected to bring to minimum rms current through the converter ports. Instead, the phase-shifts $\phi_{2}$ and $\phi_{3}$ are set by proportional-integrative regulators followed by a decoupling matrix, as done in [13].

## B. Considerations on the Digital Implementation

To evaluate the impact in terms of computation-burden of the designed ANN in a common low-cost microcontroller, the deployment on an STM32F334R8 of the same ANN has been considered. Operatively, the ANN developed in TensorFlow, with three layers and 20,20 , and 15 neurons, has been converted into C-language and deployed as a library on the microcontroller. The conversion was performed by exploiting the toolbox STM32Cube. AI provided by STMicroelectronics.

The deployment of the ANN, which involves a total of 883 parameters, implies the allocation of about 3.45 kB of readonly memory (ROM) and 188 B of random-access memory (RAM), of which 16 B are due to the input layer, 12 B to the output layer, and 160 B to the activation functions. The network complexity is measured in terms of multiply-and-accumulate (MAC) operations. In the considered case,


Fig. 12: Experimental results at $V_{1}=400 \mathrm{~V}, V_{2}=320 \mathrm{~V}$, $V_{3}=480 \mathrm{~V}, P_{2}=350 \mathrm{~W}$, and variable $P_{3}$ : (a) Optimum dutycycles found by the ANN and BF search; (b) total rms current for the ANN, BF search, and PSM.
the number of MAC operations involved is 1463. Further details are reported in Tab. III, layer-by-layer. Finally, the measured average computation time of the ANN is $127.43 \mu \mathrm{~s}$. Negligible deviations due to numerical errors of the digital implementation were recorded.

TABLE III: ANN deployment on an STM32 microcontroller.

| Layer | \# Neurons | Param. | Memory (ROM) | MAC |
| :--- | :---: | :---: | :---: | :---: |
| Input | 4 | - | - | - |
| Hidden 1 | 20 | 100 | $400 \mathrm{~B}(11.3 \%)$ | $100(6.8 \%)$ |
| Act. funct. | - | - | - | $200(13.7 \%)$ |
| Hidden 2 | 20 | 420 | $1.6 \mathrm{kB}(47.6 \%)$ | $420(28.7 \%)$ |
| Act. funct. | - | - | - | $200(13.7 \%)$ |
| Hidden 3 | 15 | 315 | $1.3 \mathrm{kB}(47.6 \%)$ | $315(21.5 \%)$ |
| Act. funct. | - | - | - | $150(10.3 \%)$ |
| Output | 3 | 48 | $192 \mathrm{~B}(5.4 \%)$ | $78(5.4 \%)$ |
| Act. funct. | - | - | - | $0(0.0 \%)$ |

## C. Results and Discussion

Eleven power and voltage setpoints are tested, covering a wide range of transferred power across TAB converter ports starting from low to high power levels and characterized by significant dc voltage mismatch between the converter ports. A comparison between the proposed ANN-based modulation, BF search, and PSM is shown for the test cases. The comparison with PSM is included for reference, demonstrating the operation performance compared to a common, standard, and simple test case often referred to in related literature


Fig. 13: Percentage reduction in the TAB overall losses using the proposed ANN-based modulation compared to PSM.


Fig. 14: Voltage and current waveforms with $V_{1}=400 \mathrm{~V}$, $V_{2}=320 \mathrm{~V}, V_{3}=480 \mathrm{~V}, P_{2}=350 \mathrm{~W}$, and $P_{3}=200 \mathrm{~W}$ : (a) using PSM; (b) using the proposed ANN-based modulation.

(a)
(b)

Fig. 15: Voltage and current waveforms with $V_{1}=400 \mathrm{~V}$, $V_{2}=320 \mathrm{~V}, V_{3}=480 \mathrm{~V}, P_{2}=350 \mathrm{~W}$, and $P_{3}=1400 \mathrm{~W}$ : (a) using PSM; (b) using the proposed ANN-based modulation.


Fig. 16: Step response: (a) power at port-2; (b) duty-cycles by the ANN; (c) phase-shifts by the PI regulators. Test condition: $V_{1}=400 \mathrm{~V}, V_{2}=320 \mathrm{~V}, V_{3}=480 \mathrm{~V}, P_{3}=220 \mathrm{~W}$.
and highlighting the advantage of applying duty-cycles optimization [15]-[17], [21]. The test cases present voltage levels $V_{1}=400 \mathrm{~V}, V_{2}=320 \mathrm{~V}$, and $V_{3}=480 \mathrm{~V}$, with port-2 power fixed at $P_{2}=350 \mathrm{~W}$, and port-3 power $P_{3}$ varying in the range from 200 W to 3650 W .

Fig. 12(a) shows the optimum duty-cycles computed by the ANN approach compared to the results by the BF search on the experimental prototype; BF results are deemed the true optimal values. Overall, a slight deviation between the ANN and BF search is noticed. In fact, Fig. 12(b) shows a deviation below $2 \%$ in the measured rms current, with a reduction in the total rms current of up to $60 \%$ at low power levels with respect to the PSM. Fig. 13 shows the percentage of measured reduction of converter total losses compared to PSM.
Fig. 14 and Fig. 15 show steady-state transformer voltage and current waveforms of the PSM and the proposed ANNbased modulation for two test cases, with $P_{3}=200 \mathrm{~W}$ and $P_{3}=1400 \mathrm{~W}$, representing low and high power operation, respectively. Fig. 14 shows that the total rms current reduces from about 8.3 A using PSM to about 3.9 A using the proposed ANN-based modulation, that is, a total rms current reduction of about $53 \%$. The total rms current reduction in Fig. 15 is about $19 \%$, because at high power levels the optimum operating point is located nearby the full duty modulation.

To demonstrate the dynamic performance of the ANN approach, a step change from $P_{2}=200 \mathrm{~W}$ to $P_{2}=800 \mathrm{~W}$ of the load at port-2 shown in Fig. 16. Fig. 16(b) shows the response of the ANN, which updates the computed optimum dutycycles within a few switching cycles immediately after the
transient. Fig. 16(c) shows the response of the PI regulators adapting the phase-shifts to keep the output voltage constant as the operating conditions evolve. Notably, the ANN response is almost instantaneous, which is a distinctive merit of the proposed approach compared to alternative solutions based on iterative or on-line search methods.

Fig. 17 and Fig. 18 display the current and voltage waveforms, respectively, of the transformer across the transition considered above. In particular, Fig. 17(a) shows the stepchange of current $i_{2}$ due to the corresponding change of power at port-2. A zoomed-in view of this detail is provided in Fig. 17(c). Fig. 17(b) and (d) show the steady-state current waveforms before and after, respectively, the applied stepchange transient. The corresponding voltage waveforms are provided in Fig. 18(b) and in Fig. 18(c), after and before the transient, respectively. Remarkably, the ANN is capable of promptly and automatically adapting the duty-cycles to the actual operating conditions within about four switching cycles.

## VII. Conclusion

An artificial neural network (ANN) approach for achieving reduced rms operation of triple active bridges (TAB) converters has been proposed and verified in this paper. A multilayer perceptron neural network was designed and trained in order to estimate the optimal modulation parameters of the TAB, aiming at converter operation with minimum total rms currents. The ANN was trained based on a data-set generated by means of a simulation model. The simulation model was preliminarily calibrated to accurately describe the actual TAB prototype. The approach features ease of data generation for ANN training, and deployability in real converter hardware, and allows significant improvements in terms of total rms current circulation compared to the classical phaseshift approach. The proposed ANN approach shows other potential benefits with respect to the use of a look-up table for the modulation of the converter, including smooth operation under different operating points, lower memory requirements, extension to converters with multiple ports, the possibility of tuning the model with a reasonably limited number of samples of operating points, and the potential advantage of providing solutions in conditions not included in the training data-set. Finally, the presented approach can be used to generate a pretrained ANN input/output map that can be adapted/refined by on-line learning techniques, thus speeding up and facilitating the on-line training. This possibility and the extension to converters with additional ports may be considered as future research directions.

## References

[1] M. Rashidi et al., "Design and Development of a High-Frequency Multiport Solid-State Transformer With Decoupled Control Scheme," IEEE Trans. Ind. Appl., vol. 55, no. 6, pp. 7515-7526, 2019.
[2] T. Pereira et al., "A Comprehensive Assessment of Multiwinding Transformer-Based DC-DC Converters," IEEE Trans. Power Electron., vol. 36, no. 9, pp. $10020-10036,2021$.
[3] A. Avila et al., "A Modular Multifunction Power Converter Based on a Multiwinding Flyback Transformer for EV Application," IEEE Trans. Transport. Electrific., vol. 8, no. 1, pp. 168-179, 2022.


Fig. 17: Transformer current waveforms during transient of port-2 power: (a) transformer currents during transient ; (b) steadystate initial transformer currents (c) zoom in of port-2 current during transient; (d) steady-state final transformer currents.


Fig. 18: Transformer voltages during transient of port-2 power: (a) transformer voltages; (b) steady-state initial transformer voltages; (c) steady-state final transformer voltages.
[4] C. Gu et al., "A Multiport Power Conversion System for the More Electric Aircraft," IEEE Trans. Transport. Electrific., vol. 6, no. 4, pp. 1707-1720, 2020.
[5] N. Swaminathan et al., "An Overview of High-Conversion High-Voltage DC-DC Converters for Electrified Aviation Power Distribution System," IEEE Trans. Transport. Electrific., vol. 6, no. 4, pp. 1740-1754, 2020.
[6] C. Samende et al., "Power Loss Minimization of Off-Grid Solar DC Nano-Grids—Part I: Centralized Control Algorithm," IEEE Trans. Smart Grid, vol. 12, no. 6, pp. 4715-4725, 2021.
[7] A. Vettuparambil et al., "A Modular Multiport Converter to Integrate Multiple Solar Photo-Voltaic (PV) Modules With a Battery Storage System and a DC Microgrid," IEEE Trans. Ind. Electron., vol. 69, no. 5, pp. 4869-4878, 2022.
[8] J. Zeng et al., "A Multiport Bidirectional DC-DC Converter for Hybrid Renewable Energy System Integration," IEEE Trans. Power Electron., vol. 36, no. 11, pp. 12281-12 291, 2021.
[9] Chuanhong Zhao et al., "A Novel Three-Phase Three-Port UPS Employing a Single High-Frequency Isolation Transformer," in IEEE 35th Ann. Power Electron. Specialists Conf., vol. 6, 2004, pp. 4135-4141 Vol.6.
[10] M. Michon et al., "A three-port bi-directional converter for hybrid fuel cell systems," in 2004 IEEE 35th Ann. Power Electron. Specialists Conf., vol. 6, 2004, pp. 4736-4742 Vol.6.
[11] De Doncker, R.W.A.A. and Divan, D.M. and Kheraluwala, M.H., "A three-phase soft-switched high-power-density DC/DC converter for high-power applications," IEEE Trans. Ind. Appl., vol. 27, no. 1, pp. 63-73, 1991.
[12] F. Krismer et al., "Closed Form Solution for Minimum Conduction Loss Modulation of DAB Converters," IEEE Trans. Power Electron., vol. 27, no. 1, pp. 174-188, 2012.
[13] C. Zhao et al., "An Isolated Three-Port Bidirectional DC-DC Converter With Decoupled Power Flow Management," IEEE Trans. Power Electron., vol. 23, no. 5, pp. 2443-2453, 2008.
[14] A. A. Ibrahim et al., "Conduction Loss Reduction of Isolated Bidirectional DC-DC Triple Active Bridge," in 2021 IEEE 4-th Intern. Conf. on DC Microgrids (ICDCM), 2021, pp. 1-8.
[15] P. Purgat et al., "Zero Voltage Switching Criteria of Triple Active Bridge Converter," IEEE Trans. Power Electron., vol. 36, no. 5, pp. 5425-5439, 2021.
[16] J. Li et al., "Efficiency Optimization Scheme for Isolated Triple Active Bridge DC-DC Converter with Full Soft-Switching and Minimized RMS Current." IEEE Trans. Power Electron., pp. 1-1, 2022.
[17] S. Dey et al., "Multivariable-Modulation-Based Conduction Loss Min-
imization in a Triple-Active-Bridge Converter," IEEE Trans. Power Electron., vol. 37, no. 6, pp. 6599-6612, 2022.
[18] S. Dey et al., "Multi-variable Multi-constraint Optimization of Triple Active Bridge DC-DC Converter with Conduction Loss Minimization," 2022 IEEE Appl. Power Electron. Conf. \& Expo (APEC), 2022.
[19] A. Chandwani et al., "Three-loop Multi-variable Control of Triple Active Bridge Converter with Power Flow Optimization," 2022 IEEE Appl. Power Electron. Conf. \& Expo (APEC), 2022.
[20] I. Kougioulis et al., "An Integrated On-Board Charger and AuxiliaryPower Module for Electric Vehicles," 2022 IEEE Appl. Power Electron. Conf. \& Expo (APEC), 2022.
[21] A. A. Ibrahim et al., "Multidimensional Ripple Correlation Technique for Optimal Operation of Triple Active-Bridge Converters," IEEE Trans. Ind. Electron., pp. 1-10, 2022.
[22] S. Zhao et al., "An Overview of Artificial Intelligence Applications for Power Electronics," IEEE Trans. Power Electron., vol. 36, no. 4, pp. 4633-4658, 2021.
[23] D. Wang et al., "Model Predictive Control Using Artificial Neural Network for Power Converters," IEEE Trans. Ind. Electron., vol. 69, no. 4, pp. 3689-3699, 2022.
[24] A. N. Akpolat et al., "Dynamic Stabilization of DC Microgrids Using ANN-Based Model Predictive Control," IEEE Trans. Energy Conv., vol. 37, no. 2, pp. 999-1010, 2022.
[25] Z. Li et al., "A Model-Data-Hybrid-Driven Diagnosis Method for OpenSwitch Faults in Power Converters," IEEE Trans. Power Electron., vol. 36, no. 5, pp. 4965-4970, 2021.
[26] Q. Xu et al., "Artificial Intelligence-Based Control Design for Reliable Virtual Synchronous Generators," IEEE Trans. Power Electron., vol. 36, no. 8, pp. 9453-9464, 2021.
[27] R. Rajamony et al., "Artificial Neural Networks-Based Multi-Objective Design Methodology for Wide-Bandgap Power Electronics Converters," IEEE Open Jour. Power Electron., vol. 3, pp. 599-610, 2022.
[28] F. Toniolo et al., "Implementation and experimental evaluation of an efficiency-improved modulation technique for IBCI DC-DC converters," in 2020 IEEE Appl. Power Electron. Conf. \& Expo. (APEC). IEEE, 2020, pp. 3430-3436.
[29] X. Li et al., "Artificial-Intelligence-Based Triple Phase Shift Modulation for Dual Active Bridge Converter with Minimized Current Stress," IEEE Trans. Emerg. Sel. Topics Power Electron., 2021.
[30] F. Lin et al., "AI-Based Design with Data Trimming for Hybrid Phase Shift Modulation for Minimum-Current-Stress Dual Active Bridge Converter," IEEE Trans. Emerg. Sel. Topics Power Electron., pp. 1-1, 2023.
[31] M. Meireles et al., "A comprehensive review for industrial applicability of artificial neural networks," IEEE Trans. Ind. Electron., vol. 50, no. 3, pp. 585-601, 2003.
[32] S. Zhao et al., "An Overview of Artificial Intelligence Applications for Power Electronics," IEEE Trans. Power Electron., vol. 36, no. 4, pp. 4633-4658, 2021.
[33] F. Murtagh, "Multilayer perceptrons for classification and regression," Neurocomputing, vol. 2, pp. 183-197, 1991.
[34] P. G. Benardos et al., "Optimizing feedforward artificial neural network architecture," Engineering applications of artificial intelligence, vol. 20, pp. 365-382, 2007.
[35] S. Sharma et al., "Activation Functions in Neural Networks," Inter. Jour. of Eng. Appl. Sciences \& Tech., vol. 4, pp. 310-316, 2020.
[36] L. F. Costa et al., "Optimum Design of a Multiple-Active-Bridge DCDC Converter for Smart Transformer," IEEE Trans. Power Electron., vol. 33, no. 12, pp. 10 112-10 121, 2018.


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