# Total-Ionizing-Dose Effects at Ultra-High Doses in AlGaN/GaN HEMTs

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*Abstract*— Total-ionizing-dose effects in AlGaN/GaN HEMTs are evaluated by DC and low frequency noise measurements. Devices with and without passivation layers are irradiated with 10keV X-rays up to 100 Mrad(SiO<sub>2</sub>) under different bias conditions. Irradiated devices show significant electrical shifts in threshold voltage and transconductance. At doses <10 Mrad(SiO<sub>2</sub>), the TIDinduced effects are related to the passivation of pre-existing acceptor-like defects via hole capture, which induces negative threshold voltage shifts and improvement of transconductance. At doses >10 Mrad(SiO<sub>2</sub>), dehydrogenation of defects and impurity complexes leads to the creation of acceptor-like defects, which degrade the transconductance, shift positively the threshold voltage, and increase the low-frequency noise. Effects are enhanced in unpassivated devices and when the gate is biased at high voltage.

*Index Terms*—Total ionizing dose, AlGaN HEMTs, DC, low frequency noise, charge trapping, bias condition.

#### I. INTRODUCTION

HE demands on electronics working in harsh radiation environments have increased in the last several decades. Experimental fusion reactor facilities, nuclear waste depositories, and next-generation particle accelerators require chips able to withstand ultra-high ionizing radiation doses on the order of >10 Mrad(SiO<sub>2</sub>). For example, the trackers of the future High-Luminosity Large Hadron Collider (HL-LHC) at CERN, Switzerland, will be exposed to total ionizing doses (TIDs) up to 1 Grad(SiO<sub>2</sub>) over ten years of operation [1].

TID effects at ultra-high doses above ~10 Mrad(SiO<sub>2</sub>) have been investigated in Si-based planar and FinFET technologies [2]-[12]. Studies at 1 Grad(SiO<sub>2</sub>) on 65 nm MOSFETs [2]-[4], 31 nm MOSFETs [6]-[8], 16 nm FinFETs [9]-[11], and Gate-All-Around FETs [12] have revealed issues related to radiationinduced charge buildup in dielectrics, e.g., in shallow trench isolation (STI) and in spacers and have underlined the important role of hydrogen transport for the activation of TID-induced traps.

On the other hand, power and RF systems often incorporate compound semiconductor devices, including GaN-based highelectron mobility transistors (HEMTs). AlGaN/GaN HEMTs are widely used in high-power and radio-frequency applications due to their enhanced carrier mobility in the two-dimensional electron gas (2DEG) and their high breakdown electric field [13]. The absence of gate dielectrics in AlGaN/GaN devices is a key factor for their high tolerance to ionizing radiation [14]. However, in the last ~10 years, several works have pointed out significant TID sensitivities of AlGaN/GaN HEMTs; these may prevent the proper functioning at the relatively low doses typical of space applications and are likely to be even larger in high-radiation applications [15]-[23].

X-ray and 1.8-MeV proton irradiations revealed that AlGaN/GaN HEMTs often exhibit threshold voltage shifts and reductions in transconductance [15]-[17]. These TID and DD effects are related primarily to trap activation and/or neutralization in the AlGaN and GaN layers with strong sensitivities to the bias applied during irradiation [15],[16]. Results of proton irradiations are often complicated to interpret, as they combine TID effects with displacement damage (DD) effects. X-ray irradiations in recent works focused on the exploration of pure TID mechanisms in AlGaN/GaN HEMTs. However, the cumulative dose in these studies is typically <1 Mrad(SiO<sub>2</sub>), much lower than the TID often induced by proton irradiations, which is often >10 Mrad(SiO<sub>2</sub>) [15], [16], [18]. Hence, the pure TID response of GaN HEMTs at ultra-high doses is still unknown. Its exploration is useful for improving knowledge of basic degradation mechanisms in GaN-based HEMTs.

This work explores ultra-high-dose effects in a developmentstage AlGaN/GaN HEMT technology through DC and low frequency noise measurements. The results evidence complex synergies between TID effects and electrical stress, each of which is strongly influenced by applied biases. The largest threshold-voltage shifts are observed for this technology when negative gate bias is applied during irradiation, i.e., when devices are irradiated in the OFF state. In contrast, the largest

|                 | TABLE I          |                 |         |
|-----------------|------------------|-----------------|---------|
| BIAS CONDITIONS | DURING IRRADIA   | ATION AND ANNE. | ALING.* |
| Bias condition  | $V_{\sigma}$ [V] | $V_d$ [V]       | $V_s$   |

| Bias condition | $V_g$ [V] | $V_d$ [V] | $V_s$ [V] |
|----------------|-----------|-----------|-----------|
| GND            | 0         | 0         | 0         |
| ON             | 0         | +10       | 0         |
| CUT-OFF        | -7        | +10       | 0         |
| OFF            | -7        | 0         | 0         |

\*The substrate is always biased at 0 V. The annealing bias condition is identical to the bias condition applied during the irradiation.

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Manuscript submitted October 31, 2022.

The portion of the work performed at Vanderbilt University was supported in part by the US Air Force Center of Excellence in Radiation Effects, Award FA9550-22-1-0012.

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transconductance degradation occurs under ON bias irradiation. Unpassivated devices show larger sensitivity to TID irradiation and bias stress than passivated devices, reinforcing the strong role of hydrogen transport and reactions on the radiation response and reliability of GaN-based HEMTs.

## II. DEVICES AND EXPERIMENTAL DETAILS

## A. Devices under test

The GaN HEMTs under test were fabricated in a development-stage AlGaN/GaN technology at the University of California, Santa Barbara (UCSB), USA [22]. The active region consists of 200 nm of unintentionally doped (UID) GaN that is grown by Ga-rich plasma-assisted molecular beam epitaxy on n-type free-standing GaN substrate having layer doped with Fe and C (Fig. 1). The transistor channel width is 150 µm and the channel length  $L_g$  is 0.7 µm, with gate-to-drain separation ( $L_{gd}$ ) of 1 µm and gate-to-source separation ( $L_{gs}$ ) of 0.5 µm. Transistors in this study are built in two configurations: (1) passivated by a thick SiN<sub>x</sub> layer (normal configuration) and (2) unpassivated (for comparison), as shown in Figs. 1(a) and (b).

## B. Test conditions

Irradiation tests were conducted using a 10-keV X-ray irradiator at a dose rate of 3.8 Mrad(SiO<sub>2</sub>)/h for a total exposure



Fig. 1. Schematic diagram of stack layers of AlGaN/GaN HEMTs (not to scale) and optical microscope images of (a) passivated and (b) unpassivated GaN-based HEMTs.

time of ~29 h to reach 100 Mrad(SiO<sub>2</sub>). All doses and rates are referred to equilibrium doses in SiO<sub>2</sub> for consistency in calibration and to facilitate comparison with other works [15]-[19]. Considering the relative atomic numbers, we infer from comparative studies of similar materials that the doses in GaN may be 2x-2.5x the quoted equilibrium SiO<sub>2</sub> dose [24]-[26].

The radiation exposure was stopped at several steps. At each step, devices were kept with all terminals grounded for about 60 s before transistors were electrically characterized. This minimizes annealing time and allows the device to stabilize before measurements. After completion, devices were annealed at room temperature (RT) for 27 h. Several bias configurations were applied to the HEMTs during irradiation and annealing, as shown in Table I. The DC static response and low-frequency noise of the transistors were measured at room temperature before exposure and at several irradiation steps. At least two devices were tested for each set of conditions; representative results are shown below. The threshold voltage  $V_{th}$  is defined as  $V_{gs-int} - V_{ds}/2$ ;  $V_{gs.int}$  is extracted in the linear region ( $V_{ds} = 0.1$  V) as the gate-voltage axis intercept of the linear extrapolation of the  $I_d$ - $V_{gs}$  curve at the point of its maximum first derivative.

## C. Evaluation of electrical stress effects

Irradiations up to 100 Mrad(SiO<sub>2</sub>) require about ~29 h. To distinguish degradation induced by electrical stress from that induced by irradiation, the GaN-based HEMTs were stressed



Fig. 2. Electrical stress-induced degradation of  $I_{d^-}V_{gs}$  curves in the saturation regime ( $V_{ds} = 5$  V) for (a) passivated and (b) unpassivated AlGaN HEMTs. The devices were biased for a total time of 50 h at room temperature in the cutoff bias, in order to evaluate the degradation induced by the electrical stress without X-ray exposure.

without X-ray under the bias conditions of Table I for the same amounts of time required for devices to be irradiated up to 100 Mrad(SiO<sub>2</sub>).

Fig. 2 shows the electrical stress-induced degradation for (a) passivated and (b) unpassivated devices irradiated in "CUT-OFF"-bias condition, which is the case in which the largest parametric shifts are observed. The stressed HEMTs exhibit increases in leakage current and shifts of threshold voltage  $V_{th}$ . The  $V_{th}$  undergoes a negative and rapid shift in the first 1 hour. After ~29 h, the passivated HEMT biased in the "CUT-OFF" condition shows an increase of maximum drain current of 4%, while the passivated HEMT shows a decrease of maximum oncurrent of 7%. For all biases, the unpassivated HEMTs show greater degradation than passivated devices.

Often electrical-stress induced effects of HEMTs may be substantial and comparable to the TID-induced effects. For this reason, the next sections report and compare the responses of biased irradiated and unirradiated devices at similar times.

#### **III. PASSIVATED DEVICES**

#### A. TID tolerance at different bias conditions

The DC characteristics in the saturation regime ( $V_{ds} = 5$  V) of passivated GaN-based HEMTs are shown in Fig. 3 when



Fig. 3.  $I_{d^*}V_{gs}$  curves of passivated GaN-based HEMTs in the saturation regime ( $V_{ds} = 5$  V). The devices were irradiated up to 100 Mrad(SiO<sub>2</sub>) and then annealed at room temperature for 27 h in (a) the "CUT-OFF"-bias and (b) the "ON"-bias.

devices are irradiated and annealed under the "CUT-OFF" and "ON"-bias conditions. During exposure, the drain leakage current at  $V_g=0$  V increases significantly regardless of the applied bias, a signature of drain-to-gate leakage. The  $V_{th}$  shifts monotonically to negative values as large as -270 mV in "CUT-OFF"-biased devices, and to positive values up to 50 mV in "ON"-biased devices. The "ON"-biased devices exhibit degradation of the transconductance  $g_m$ , which is evident as decreases in the slopes of the  $I_d$ - $V_g$  curves for -3 V <  $V_g < 0$  V. Slight performance recovery is visible after 27 h of room temperature annealing, suggesting the formation of a significant density of stable defects.

Fig. 4 shows the effects of applied bias on the degradation of the maximum drain current  $I_{on}$ , defined here as the drain current at  $V_{gs} = 0$  V and  $V_{ds} = 5$  V. Dotted lines refer to electrical stress-induced degradation without X-ray exposure; continuous lines are obtained with X-ray exposure. GaN HEMTs irradiated in the "CUT-OFF" and "OFF" biases show increases (improvement) in Ion by about 9% and 7% at 100 Mrad(SiO2). Room temperature annealing reduces this increase:  $\Delta I_{on} = 4\%$ after 27 h. The significant difference between the continuous and dotted lines demonstrates that the performance enhancement of "CUT-OFF" and "OFF" biased devices is affected more strongly by TID-induced effects than by biasinduced effects. In contrast, devices irradiated in the "ON" bias condition exhibit a degradation, as evidenced by the 5% decrease of Ion at 100 Mrad(SiO<sub>2</sub>). The degradation for devices irradiated or electrically stressed in the "ON"-bias condition is similar, showing that bias-induced stress dominates the changes in device response.

Fig. 5 shows the radiation-induced degradation of the DC parameters (a)  $\Delta V_{th}$  and (b) maximum transconductance  $\Delta g_{m-MAX}$ , calculated in the linear regime at  $V_{ds} = 0.5$  V. These values are for different GaN-based HEMTs irradiated and then annealed under different bias conditions. The  $I_{on}$  variation of irradiated GaN HEMTs of Fig. 4 is dominated by the negative shift of  $V_{th}$  for "CUT-OFF" and "OFF"-biased devices. Three interesting effects are evident in Fig. 5:

1) Insensitivity to TID when irradiated at 0 V gate bias. The best TID tolerance is found for "GND"-biased and "ON"-



Fig. 4. Degradation of maximum drain current  $\Delta I_{on}$  as a function of dose in passivated GaN-based HEMTs. Dotted lines refer to the electrical stress-induced degradation, where devices were tested without X-ray exposure; continuous lines refer to test results with X-ray exposure. Irradiations were performed up to 100 Mrad(SiO<sub>2</sub>) and then devices were annealed at room temperature for 27 hours in different bias conditions.



Fig. 5. Degradation of (a) threshold voltage  $\Delta V_{th}$  and (b) maximum transconductance  $\Delta g_{m:MAX}$  as a function of dose in passivated GaN-based HEMTs. Dotted lines refer to electrical stress-induced degradation without X-ray exposure; continuous lines refer to test results with X-ray exposure. Irradiations were performed up to 100 Mrad(SiO<sub>2</sub>); then devices were annealed at room temperature for 27 h in different bias conditions.

biased devices, for which the gate bias is 0 V. This enhancement of the TID tolerance is most likely related to the limited charge yield at low electric fields [15],[16],[27]. The "ON"-biased devices show a slight  $V_{th}$  increase and  $g_m$  decrease, but this degradation is related to a bias-stress-induced effect, as shown by the overlapping of the continuous and dotted (red) curves. It is more likely that "ON"-biased devices suffer from hotelectron stress, which can induce the activation of acceptor-like traps through the dehydrogenation of O<sub>N</sub>-H complexes in the GaN buffer layer [15],[17],[19]. In the case of "ON"-biased devices, post-irradiation annealing continues to induce a slight increase of the  $V_{th}$ , as "ON" bias is maintained for longer times.

2) Rebound of the  $V_{th}$  shifts at 10 Mrad(SiO<sub>2</sub>) of irradiated HEMTs. Irradiations in the "CUT-OFF" and "OFF" conditions induce an initial negative  $V_{th}$  shift. At 10 Mrad(SiO<sub>2</sub>), the  $\Delta V_{th}$  is about -280 mV for the "CUT-OFF"-biased HEMTs and -263 mV for "OFF"-biased HEMTs. The negative  $V_{th}$  shift and the increase of  $g_{m-MAX}$  indicates neutralization of acceptor-like defects [28]. After 10 Mrad(SiO<sub>2</sub>),  $V_{th}$  recovers somewhat, as

shown by the positive trend vs. dose. At 100 Mrad(SiO<sub>2</sub>),  $\Delta V_{th}$  is about -190 mV for both "CUT-OFF and "OFF"-biased HEMTs and it continues to recover during the RT annealing.

3) Rebound of  $g_{m-MAX}$  at 10 Mrad(SiO<sub>2</sub>) of irradiated HEMTs. At doses <10 Mrad(SiO<sub>2</sub>), the  $g_{m-MAX}$  of irradiated HEMTs increases with cumulative dose at a higher rate compared to electrically stressed devices, consistent with accelerated acceptor neutralization [17]. At doses >10 Mrad(SiO<sub>2</sub>),  $g_{m-MAX}$ degrades, suggesting activation of defects in the active GaN layer [15], [17], [19]. Increases of acceptor-like defect densities in the 2DEG may lead to TID-induced transconductance loss and positive  $V_{th}$  shifts, i.e., formation of N vacancies, Ga vacancies, and/or O<sub>N</sub> DX centers [15], [16], [18], [20], [29].

#### B. Low frequency noise responses

Additional insight into densities of defects contributing to charge trapping are obtained by low-frequency noise measurements [15], [16], [18], [30]-[33]. The drain-voltage noise power spectral density  $S_{vd}$  was evaluated in a frequency span between 1 Hz and 1 kHz at  $|V_{ds}| = 0.1$  V for several values of  $V_{gt} = V_{gs}-V_{th}$ . The low-frequency noise of GaN-based HEMTs is caused primarily by fluctuations of the numbers of carriers induced by the capture and emission of carriers at individual defect sites in the GaN layer or at the AlGaN/GaN border, which is often affected by the atomic reconfiguration of single defect sites in the GaN [27],[29].

Fig. 6 shows the low-frequency noise for (a) "CUT-OFF"biased and "ON"-biased HEMTs before irradiation, at 1 Mrad(SiO<sub>2</sub>), at 100 Mrad(SiO<sub>2</sub>), and after high temperature annealing. GaN-based HEMTs show typical 1/f low-frequency noise. In "ON"-biased HEMTs, the noise is constant and is relatively insensitive to the irradiation and electrical stress. On the other hand, the noise magnitude of "CUT-OFF"-biased devices is approximately constant at 1 Mrad(SiO<sub>2</sub>) and increases at 100 Mrad(SiO<sub>2</sub>). This increase of the noise, which is visible only at ultrahigh doses, indicates activation of new traps, in agreement with the  $V_{th}$  increases and  $g_m$  decreases occurring at > 10 Mrad(SiO<sub>2</sub>) in Fig. 5. During room temperature annealing, very little change occurs to the noise.



Fig. 6. Low-frequency noise magnitudes for GaN-based HEMTs irradiated and annealed in (a) the "CUT-OFF"-bias condition and (b) "ON"-bias condition. The noise was measured at  $V_{ds} = 0.5$  V and  $V_{gt} = 0.6$  V at room temperature.

To investigate the density distributions in space and energy of the border traps, Fig. 7 plots the low-frequency noise magnitude at 10 Hz as a function of  $V_{gt} = V_{gs}$  - Vth in GaN-based HEMTs irradiated in "CUT-OFF" and "ON"-bias conditions. When the slope  $|\beta|$  of the  $S_{\nu D}$ - $V_{gt}$  curve is approximately equal to 2, the effective density of the border traps is uniform in space and energy [27]-[29], [33], [34]. "CUT-OFF"-biased devices show a significant increase of low-frequency noise levels at 100  $Mrad(SiO_2)$  in agreement with Fig. 6(a). In both pristine and irradiated devices, the slope  $|\beta|$  of Svd-Vgt is ~2.1, indicating an approximately uniform spatial and energetic distribution of traps [27]-[29]. The slope  $|\beta|$  of Svd-Vgt is ~2.5 after the RT annealing, suggesting a less uniform density of generated traps in space and energy. On the other hand, "ON"-biased devices are characterized by constant noise with  $|\beta|$  equal to 2, indicating uniform and constant density of traps. Room temperature annealing in "ON"-biased devices induces a slight increase in  $|\beta|$ , which is equal to 2.3 after 27 h of room temperature annealing.

#### IV. UNPASSIVATED DEVICES

#### A. TID sensitivity

This section analyzes the TID response of unpassivated devices that are otherwise similar to those in Figs. 3-7. The DC characteristics in the linear regime ( $V_{ds} = 0.1$  V) of unpassivated

GaN-based HEMTs are shown in Fig. 8 when the devices are irradiated and annealed in the "CUT-OFF" and "ON"-bias conditions. The highest shift is visible in the "CUT-OFF" condition, where  $V_{th}$  shifts to negative values by about ~0.6 V and the leakage current increases by two orders of magnitude, from  $2 \times 10^{-6}$  A to  $2 \times 10^{-4}$  A. Slight performance recovery is visible after 27 h of room temperature annealing, similarly to passivated devices. The "ON"-biased devices are characterized by negative  $V_{th}$  shifts, about -270 mV after 100 Mrad(SiO<sub>2</sub>), which are smaller than those of "CUT-OFF"-biased devices.

The influence of irradiation bias on TID sensitivity is shown in Fig. 9, which summarizes the degradation of: (a) maximum drain current  $I_{on}$ , (b) threshold voltage  $V_{th}$ , and (c) maximum transconductance  $g_{m-MAX}$ . The dotted lines refer to electrical stress-induced degradation without X-ray exposure; continuous lines are obtained with X-ray exposure. The  $I_{on}$  variation of irradiated GaN HEMTs of Fig. 9(a) is mostly dominated by the negative shift of  $V_{th}$ . The highest shift is visible in "CUT-OFF" and "OFF" biases, while the bias conditions with the smallest degradation are the "GND" and "ON" conditions. The clear separation of dotted and continuous lines indicates that the degradation induced during the exposure is mainly related to TID.

In contrast to the passivated HEMTs, the  $V_{th}$  values of unpassivated devices irradiated in "GND" and "ON" conditions



Fig. 7. 1/f noise magnitudes at f = 10 Hz vs.  $V_{gs}$ - $V_{th}$  at  $V_{ds} = 0.5$  V for GaNbased HEMTs with irradiated and annealed in (a) the "CUT-OFF"-bias condition and (b) "ON"-bias condition.



Fig. 8.  $I_d$ - $V_{gs}$  curves of unpassivated GaN-based HEMTs in the saturation regime ( $V_{ds} = 5$  V). The devices were irradiated up to 100 Mrad(SiO<sub>2</sub>) and then annealed at room temperature for 27 h in (a) the "CUT-OFF"-bias and (b) the "ON"-bias.



Fig. 9. Degradation of (a) maximum drain current  $\Delta I_{an-lin}$ , (b) threshold voltage  $\Delta V_{lh}$ , and (c) maximum transconductance  $\Delta g_{m-MAX}$  as a function of dose in unpassivated GaN-based HEMTs. Dotted lines refer to electrical stress-induced degradation, where devices were tested without X-ray exposure; continuous lines refer to test results with X-ray exposure. Irradiations are performed up to 100 Mrad(SiO<sub>2</sub>) and then devices were annealed at room temperature for 27 h in different bias conditions.

degrade with a similarly decreasing monotonic trend. On the other hand, similarly to passivated devices, the "CUT-OFF" and "OFF"-biased transistors exhibit a rebound of the  $V_{th}$  and  $g_m$  values around 10 Mrad(SiO<sub>2</sub>). At doses < 10 Mrad(SiO<sub>2</sub>),  $V_{th}$  shifts to negative values and  $g_m$  increases. At doses > 10 Mrad(SiO<sub>2</sub>),  $V_{th}$  shifts toward more positive values and  $g_m$  decreases.

Fig. 10 shows  $\Delta V_{th}$  as a function of the time for devices that were irradiated in the OFF-bias condition and then annealed at room temperature for up to 24 h in the same bias condition. In the passivated devices,  $V_{th}$  recovers by 34 mV in the first 5 h and by 40 mV after 24 h. In unpassivated devices,  $V_{th}$  recovers by 79 mV in the first 5 h and by 103 mV after 24 h. The plot shows that most annealing-induced shifts occur in the first 5 h with the highest shifts in unpassivated devices. The recovery then saturates, becoming approximately stable for annealing times over 15 h. The additional annealing that occurs in the unpassivated devices is most likely due to enhanced hydrogen diffusion and passivation reactions in these devices [21], [23], as discussed in Section V.

Low-frequency noise measurements for the "CUT-OFF"biased HEMTs show typical 1/f low-frequency noise, as shown in Fig. 11(a). The noise magnitude was unchanged up to 1 Mrad(SiO<sub>2</sub>) and increases by almost one order of magnitude after 100 Mrad(SiO<sub>2</sub>), indicating activation of new border traps. Fig. 11(b) plots the low-frequency noise magnitude at 10 Hz as a function of  $V_{gt}$  in the HEMTs irradiated in "CUT-OFF"-bias condition. The devices show significant increases of the lowfrequency noise levels at 100 Mrad(SiO<sub>2</sub>), corresponding to the  $V_{th}$  increase and  $g_m$  decrease visible in Fig. 11. In both pristine and irradiated devices, the slope  $|\beta|$  of  $S_{id}$ - $V_{gt}$  is ~2.1 indicating an approximately uniform spatial and energetic distribution of traps [27]-[29] before and during the irradiation. During room temperature annealing, the value of  $|\beta|$  is 2.4, indicating a slightly non-uniform redistribution of the traps.



Fig. 10. Change in threshold voltage  $\Delta V_{th}$  vs. time in passivated and unpassivated GaN-based HEMTs. The  $\Delta V_{th}$  is measured during room temperature annealing of devices that were irradiated to 100 Mrad(SiO<sub>2</sub>). The annealing is performed at  $V_g = -7$  V, i.e., in the OFF-bias condition.



Fig. 11. (a) Low-frequency noise magnitudes for unpassivated GaN HEMTs irradiated in the "CUT-OFF"-bias condition. The noise was measured at  $V_{ds} = 0.1$  V and  $V_{gt} = 0.5$  V at room temperature. (b) 1/f noise magnitudes at f = 10 Hz vs.  $V_{gs}$ - $V_{th}$  at  $V_{ds} = 0.1$  V for the "CUT-OFF" irradiated HEMT.

## B. TID mechanisms

These results suggest two main TID-related mechanisms:

-  $I^{st}$  mechanism. This is characterized by negative  $V_{th}$  shifts,  $g_m$  increases, and unchanged noise. In unpassivated devices, this response is visible under all bias conditions, with enhancement at high gate biases. It is likely that this mechanism results from the TID-assisted passivation of acceptor-like defects via hole capture [16], [32].

-  $2^{nd}$  mechanism. This is characterized by positive  $V_{th}$  shifts,  $g_m$  degradation, and increase of the low-frequency noise magnitude. It is visible only during the irradiation at high gate biases, i.e., "CUT-OFF" and "OFF" at doses >10 Mrad(SiO<sub>2</sub>). It is more likely that this mechanism is related to activation of acceptor-like defects via dehydrogenation of defects, as often observed in proton-irradiated GaN-based HEMTs at higher fluences [15], [16], [18], [29].

#### C. Leakage current

Fig. 12 plots the off-state leakage current  $I_{off}$  flowing through the drain terminal when  $V_{gs} = -7$  V and  $V_{ds} = 5$  V in unpassivated HEMTs. In general, the value of  $I_{off}$  increases by about one order of magnitude after devices are irradiated to 100 Mrad(SiO<sub>2</sub>), with negligible contributions of electrical stress (dotted curves). Only GaN-based HEMTs in the "CUT-OFF"bias condition (green curves) exhibit these large Ioff increases of about two orders of magnitude. This high  $I_{off}$  degradation in "CUT-OFF" biased HEMTs is induced by electrical stress, which is enhanced when the gate and drain are simultaneously biased at opposite voltages. The high electric field induced by high gate-to-drain voltage may lead to percolation-based transport through defect and/or impurity centers in the AlGaN layer [20], [29], [35]-[37]. Particularly at higher voltages, these stress conditions may also lead to impact ionization of carriers, leading to positive charge trapping in the passivation layer of these devices [37], [38].



Fig. 12. Increase of the drain leakage current  $I_{off}$  at  $V_{ds} = 5$  V as a function of cumulative dose for GaN HEMTs irradiated and annealed in different bias conditions.

### V. DISCUSSION

Fig. 13 shows the  $\Delta V_{th}$  and gate leakage  $I_g$  of passivated and unpassivated HEMTs irradiated and annealed under different bias conditions. The "CUT-OFF" and "OFF"- biased HEMTs



Fig. 13. Degradation of (a) threshold voltage  $\Delta V_{th}$  and (b) gate leakage current  $I_g/I_{g0}$  for passivated and unpassivated GaN-based HEMTs. Solid lines refer to passivated devices, while dotted lines refer to unpassivated devices. Irradiations are performed up to 100 Mrad(SiO<sub>2</sub>) and then devices were annealed at room temperature for 27 h under similar bias conditions to those applied during irradiation.

have similar TID responses; only "CUT-OFF"-biased devices are shown for clarity. The trends of curves in Fig. 13(a) among passivated and unpassivated devices are generally similar, except for passivated "ON"-biased devices, for which the degradation is dominated by electrical stress. TID-induced effects are enhanced when bias is applied to the gate, i.e., at  $V_g$  = -7 V, corresponding to the OFF condition. In "CUT-OFF" passivated and unpassivated devices, TID effects are caused by the two mechanisms described in section IV. The 1<sup>st</sup> mechanism occurs at doses <10 Mrad(SiO<sub>2</sub>) with negative  $V_{th}$  shifts, while the 2<sup>nd</sup> mechanism dominates at doses > 10 Mrad(SiO<sub>2</sub>) with positive  $V_{th}$  shifts. "GND" and "ON" biased devices exhibit only the 1<sup>st</sup> mechanism, inducing negative  $V_{th}$  shifts.

Observed shifts in Fig. 13(a) are smaller for passivated devices than unpassivated devices. After 100 Mrad(SiO<sub>2</sub>) in the "CUT-OFF" bias condition,  $V_{th}$  values for the passivated HEMTs shifts by -0.34 V vs. -0.68 V for unpassivated devices. The higher TID sensitivity of unpassivated HEMTs compared to passivated devices highlights the key role of contaminant absorption (e.g., oxygen, moisture) through the surface layers [21], [23]. SiN<sub>x</sub> passivation inhibits moisture absorption, limiting the formation of acceptor-like defects [21]. Hence, the

composition and thickness of passivation layers is an important factor in determining the radiation tolerance and long-term reliability of GaN-based HEMTs.

Fig. 13(b) shows the gate current  $I_g$  normalized by its preirradiation value of  $I_{g0}$  for GaN-based HEMTs irradiated under different bias conditions. In general, the highest gate-to-drain leakage currents are visible in unpassivated devices. After 100 Mrad(SiO<sub>2</sub>), the value of  $I_g/I_{g0}$  of unpassivated HEMTs increases by roughly one order of magnitude for all cases except CUT-OFF" devices. These show increases of two orders of magnitude, consistent with the stress-induced increase visible in *I*<sub>off</sub> in Fig. 12. In passivated devices, the increase of the gate leakage is lower than one order of magnitude, regardless of bias applied during irradiation. Since the leakage depends only weakly on gate bias, the leakage in the passivated devices is dominated most likely by charge trapping in the SiN layer [35], [36], while unpassivated devices are most likely dominated by surface trap buildup at the top of the AlGaN [37], [38]. Both the traps in SiN and the surface traps are most likely charged positively after stress, based on the behavior of the device of Fig. 12, and consistent with the electric fields. The comparative responses between the two device types in Fig. 13(b) suggest that the surface trap density in the unpassivated devices exceeds the SiN charged trap density [23].

#### VI. CONCLUSIONS

AlGaN/GaN HEMTs irradiated at ultra-high doses show significant degradation due to TID and electrical stress, with magnitudes depending on irradiation bias. In general, ultra-high doses induces negative  $V_{th}$  shifts with magnitudes that are higher than the ones retrieved at lower doses of previous X-rays and gamma studies. The HEMTs irradiated with negative gate bias (OFF-state) exhibit the most negative threshold voltage shifts. At doses <10 Mrad(SiO<sub>2</sub>), TID effects are related to the passivation of pre-existing acceptor-like defects via hole capture, which induces negative threshold voltage shifts and improvement of transconductance. At doses >10 Mrad(SiO<sub>2</sub>), dehydrogenation of defect and impurity complexes leads to the creation of acceptor-like defects. These degrade the transconductance, shift the threshold voltage positively, and increase low-frequency noise. Slight performance recovery is visible after 27 h of room temperature annealing, most likely due to the formation of a significant density of stable defects.

Irradiation results on passivated and unpassivated HEMTs show that passivation layers may strongly affect oxygen and moisture absorption. The enhanced degradation of unpassivated devices in this study reinforces the key role that oxygen impurities and hydrogen play in the radiation response and long-term reliability of GaN-based HEMTs.

Considering potential system applications, AlGaN/GaN HEMTs have much greater tolerance to ultra-high doses than Si-based CMOS technologies [1], [2], [9], [12], [15]. In the worst-case condition, AlGaN HEMTs show <10%  $\Delta I_{on}$  variation after 100 Mrad(SiO<sub>2</sub>), which is less than ~38% of 31 nm MOSFETs and ~20% of gate-all-around Si nano-wire FETs, both tested at ultra-high doses [1], [12]. Hence, the long-term reliability of the AlGaN/GaN HEMTs is likely to be a more limiting factor than their radiation response [15], [18], [20].

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