

TRAFFIC REGULATION VIA CONTROLLED SPEED LIMIT*

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Abstract. We study an optimal control problem for traffic regulation via variable speed limit. The traffic flow dynamics is described with the Lighthill–Whitham–Richards model with Newell–Daganzo flux function. We aim at minimizing the L^2 quadratic error to a desired outflow, given an inflow on a single road. We first provide existence of a minimizer and compute analytically the cost functional variations due to needle-like variation in the control policy. Then, we compare three strategies: instantaneous policy; random exploration of control space; steepest descent using numerical expression of gradient. We show that the gradient technique is able to achieve a cost within 10% of the random exploration minimum with better computational performances.

Key words. traffic problems, optimal control problem, variable speed limit

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1. Introduction. In this paper, we study an optimal control problem for traffic flow on a single road using a variable speed limit. The first traffic flow models on a single road of infinite length using a nonlinear scalar hyperbolic partial differential equation (PDE) are due to Lighthill and Whitham [33] and, independently, Richards [35], who in the 1950s proposed a fluid dynamic model to describe traffic flow. Later on, the model was extended to networks [20] and started to be used to control and optimize traffic flow on roads. In the last decade, several authors studied optimization and control of conservation laws and several papers proposed different approaches to optimization of hyperbolic PDEs; see [5, 19, 21, 24, 31, 36, 37] and references therein. These techniques were then employed to optimize traffic flow through, for example, inflow regulation [12], ramp metering [34], and variable speed limit [22]. We focus on the last approach, where the control is given by the maximal speed allowed on the road. Notice that also the engineering literature presents a wealth of approaches [1, 2, 10, 11, 13, 15, 25, 26, 27, 28, 29, 30, 38], but mostly in the time discrete setting. In [1, 2] a dynamic feedback control law is employed to compute variable speed limits using a discrete macroscopic model. Instead, [25, 26, 27] use model predictive control to optimally coordinate variable speed limits for freeway traffic with the aim of suppressing shock waves.

In this paper, we address the speed limit problem on a single road. The control variable is the maximal allowed velocity, which may vary in time but we assume to

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be of bounded total variation, and we aim at tracking a given target outgoing flow. More precisely, the main goal is to minimize the quadratic difference between the achieved outflow and the given target outflow. Mathematically the problem is very hard, because of the delays in the effect of the control variable (speed limit). In fact, the link entering time (LET) $\tau(t)$, which represents the entering time of the car exiting the road at time t (see (7)), depends on the given inflow and the control policy on the whole time interval $[\tau(t), t]$. Moreover, the input-output map is defined in terms of LET, thus the achieved outflow at time t depends on the control variable on the whole interval $[\tau(t), t]$. Due to the complexity of the problem, in this article we restrict the problem to free flow conditions. Notice that this assumption is not too restrictive. Indeed, if the road is initially in free flow, then it will keep the free flow condition due to properties of the Lighthill–Whitham–Richards (LWR) model; see [9, Lemma 1].

After formulating the optimal control problem, we consider needle-like variations for the control policy as used in the classical Pontryagin maximum principle [8]. We are able to derive an analytical expression of the one-sided variation of the cost, corresponding to needle-like variations of the control policy, using fine properties of functions with bounded variation. In particular the one-sided variations depend on the sign of the control variation and involve integrals w.r.t. the distributional derivative of the solution as a measure; see (10). This allows us to prove Lipschitz continuity of the cost functional in the space of a bounded variation function and prove existence of a solution.

Afterwards, we define three different techniques to numerically solve this problem.

- Instantaneous policy. We design a closed-loop policy, which depends only on the instantaneous density at the road exit. More precisely, we choose the speed limit which gives the nearest outflow to the desired one.
- Random exploration (RE). It uses time discretization and random binary tree search of the control space to find the best maximal velocity profile.
- Gradient descent method (GDM). It consists in approximating numerically the gradient of the cost functional using (10) combined with a steepest descent method.

We compare the three approaches on two test cases: constant desired outflow and sinusoidal inflow; sinusoidal desired outflow and inflow. In both cases RE provides the best control policy, however, GDM performs within 10% of the best RE result with a computational cost of around 15% of RE. On the other hand, instantaneous policy performs poorly with respect to the RE, but with a very low computational cost. Notice that, in some cases, instantaneous policy may be the only practical policy, while GDM also represents a valid approach for real-time control, due to good performance and reasonable computational costs. Moreover, control policies provided by RE may have too large a total variation to be of practical use.

The paper is organized as follows: section 2 gives the description of the traffic flow model and of the optimal control problem. Moreover, the existence of a solution is proved. In section 3, the three different approaches to find control policies are described. Then in section 4, these techniques are implemented on two test cases. Final remarks and future work are discussed in section 5.

2. Mathematical model. In this section, we introduce a mathematical framework for the speed regulation problem. The traffic dynamics is based on the classical LWR model [33, 35], while the optimization problem will seek minimizers of quadratic distance to an assigned outflow.

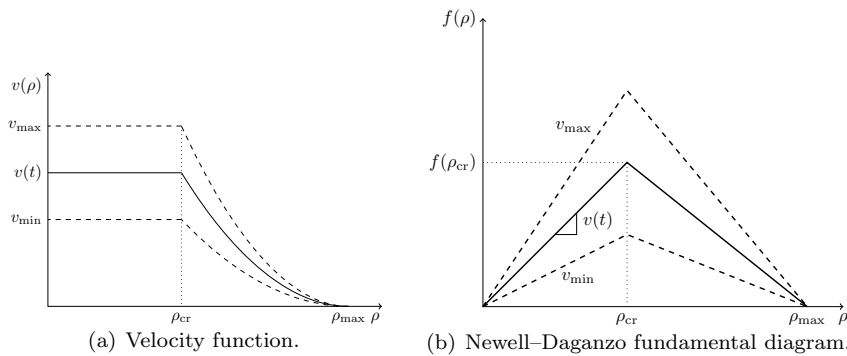


FIG. 1. Velocity and flow for different speed limits.

2.1. Traffic flow modeling. We consider the LWR model on a single road of length L to describe the traffic dynamics. The evolution in time of the car density ρ is described by a Cauchy problem for scalar conservation law with time-dependent maximal speed $v(t)$:

$$(1) \quad \begin{cases} \rho_t + f(\rho, v(t))_x = 0, & (t, x) \in \mathbb{R}^+ \times [0, L], \\ \rho(0, x) = \rho_0(x), & x \in [0, L], \end{cases}$$

where $\rho = \rho(t, x) \in [0, \rho_{\max}]$ with ρ_{\max} the maximal car density. In the transportation literature the graph of the flux function $\rho \rightarrow f(\rho)$ (in our case for a fixed $v(t)$) is commonly referred to as the fundamental diagram. Throughout the paper, we focus on the Newell–Daganzo-type [14] fundamental diagrams; see Figure 1(b). The speed takes value on a bounded interval $v(t) \in [v_{\min}, v_{\max}]$, $0 < v_{\min} \leq v_{\max}$, thus the flux function $f : [0, \rho_{\max}] \times [v_{\min}, v_{\max}] \rightarrow \mathbb{R}^+$ is given by

$$(2) \quad f(\rho, v(t)) = \begin{cases} \rho v(t) & \text{if } 0 \leq \rho \leq \rho_{\text{cr}}, \\ \frac{v(t)\rho_{\text{cr}}}{\rho_{\max} - \rho_{\text{cr}}}(\rho_{\max} - \rho) & \text{if } \rho_{\text{cr}} < \rho \leq \rho_{\max} \end{cases}$$

with $v(t)$ representing the maximal speed; see Figure 1(a). Notice that the flow is increasing up to a *critical density* ρ_{cr} and then decreasing. The interval $[0, \rho_{\text{cr}}]$ is referred to as the *free flow zone*, while $[\rho_{\text{cr}}, \rho_{\max}]$ is referred to as the *congested flow zone*.

The problem we consider is the following. Given an inflow $\text{In}(t)$, we want to track a fixed outflow $\text{Out}(t)$ on a time horizon $[0, T]$, $T > 0$, by acting on the time-dependent maximal velocity $v(t)$. A maximal velocity function $v : [0, T] \rightarrow [v_{\min}, v_{\max}]$ is called a *control policy*.

It is easy to see that a road in free flow can become congested only because of the outflow regulation with shocks moving backward; see [9, Lemma 2.3]. Since we assume Neumann boundary conditions at the road exit, the traffic will always remain in free flow, i.e., $\rho(t, x) \leq \rho_{\text{cr}}$ for every $(t, x) \in [0, T] \times [0, L]$. Given the inflow function $\text{In}(t)$, we consider the initial boundary value problem with assigned flow boundary condition $f_l \doteq f(\rho(t, 0^+))$ on the left in the sense of Bardos, Le Roux, and Nédélec

(see [6]) and Neumann boundary condition (flow $f_r \doteq f(\rho(t, 0^-))$) on the right:

$$(3) \quad \begin{cases} \rho_t + f(\rho, v(t))_x = 0, & (t, x) \in \mathbb{R}^+ \times [0, L], \\ \rho(0, x) = \rho_0(x), & x \in [0, L], \\ f_l(t) = \text{In}(t), \\ f_r(t) = \rho(t, L) v(t). \end{cases}$$

We denote by BV the space of scalar functions of bounded variations and by TV the total variation; see [7] for details. For any scalar BV function h we denote by $\xi(x^\pm)$ its right (respectively, left) limit at x . We further assume the following.

Hypothesis 2.1. There exists $0 < \rho_0^{\min} \leq \rho_0^{\max} \leq \rho_{cr}$ and $0 < f_{\min} \leq f_{\max}$ such that $\rho_0 \in \text{BV}([0, L], [\rho_0^{\min}, \rho_0^{\max}])$ and $\text{In} \in \text{BV}([0, T], [f_{\min}, f_{\max}])$.

Under this assumption, we have the following.

PROPOSITION 2.2. *Assume that Hypothesis 2.1 holds and*

$$v \in \text{BV}([0, T], [v_{\min}, v_{\max}]).$$

Then, there exists a unique entropy solution $\rho(t, x)$ to (3). Moreover, $\rho(t, x) \leq \rho_{cr}$ and, setting

$$(4) \quad \text{Out}(t) = \rho(t, L)v(t),$$

we have that $\text{Out}(\cdot) \in \text{BV}([0, T], \mathbb{R})$ and the following estimates hold:

$$(5) \quad \min \left\{ \rho_0^{\min}, \frac{f_{\min}}{v_{\max}} \right\} \leq \rho(t, x) \leq \max \left\{ \rho_0^{\max}, \frac{f_{\max}}{v_{\min}} \right\} \text{ for } x \in [0, L],$$

$$(6) \quad \min \left\{ \rho_0^{\min} v_{\min}, f_{\min} \frac{v_{\min}}{v_{\max}} \right\} \leq \text{Out}(t) \leq \max \left\{ \rho_0^{\max} v_{\max}, f_{\max} \frac{v_{\max}}{v_{\min}} \right\}.$$

Proof. Let $v^n \in \text{BV}([0, T], [v_{\min}, v_{\max}])$ be a sequence of piecewise constant functions converging to v in L^1 and satisfying $\text{TV}(v^n) \leq \text{TV}(v)$. For each v^n , by standard properties of initial boundary value problems for conservation laws [6, Theorem 2] and [16], there exists a unique BV entropy solution ρ^n to (3) with $\rho^n \in \text{Lip}([0, T], L^1)$. Notice that the left flow condition is equivalent to the boundary condition: $\rho_l(t) = \frac{\text{In}(t)}{v(t)}$. From [9, Lemma 2.3] and the Neumann boundary condition on the right, we get that $\rho^n(t, x) \leq \rho_{cr}$; thus, by the maximum principle it holds that

$$\rho^n(t, \cdot) \in \text{BV} \left(\mathbb{R}, \left[\min \left\{ \rho_0^{\min}, \frac{f_{\min}}{v_{\max}} \right\}, \max \left\{ \rho_0^{\max}, \frac{f_{\max}}{v_{\min}} \right\} \right] \right).$$

Let us now estimate the total variation of the solution ρ^n . Since it solves a scalar conservation laws, the total variation does not increase in time due to dynamics on $]0, L[$. Notice that changes in $v(\cdot)$ will not increase the total variation of ρ^n inside the road (i.e., on $]0, L[$). The total variation of ρ^n increases only because of new waves generated by changes in the inflow. Using the boundary condition $\rho_l(t) = \frac{\text{In}(t)}{v(t)}$, we can estimate the total variation in space of ρ^n caused by the time variation of In, respectively, time variation of v , by $\frac{\text{TV}(\text{In})}{v_{\min}}$, respectively, $\frac{f_{\max} \text{TV}(v)}{v_{\min}^2}$. Finally we get

$$\sup_t \text{TV}(\rho^n(t, \cdot)) \leq \text{TV}(\rho^n(0, \cdot)) + \frac{\text{TV}(\text{In})}{v_{\min}} + \frac{f_{\max} \text{TV}(v)}{v_{\min}^2}.$$

By Helly’s theorem (see [7, Theorem 2.4]) there exists a subsequence converging in $L^1([0, T] \times [0, L])$ to a limit ρ^* . By Lipschitz continuity of the flux and dominated con-

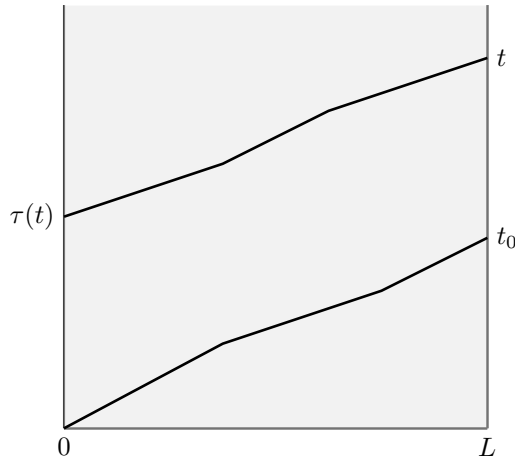


FIG. 2. Graphical representation of the LET function $\tau = \tau(t, v)$ defined in (7).

vergence we get that $f(\rho^n(t, x), v(t))$ converges in $L^1([0, T] \times [0, L])$ to $f(\rho^*(t, x), v(t))$. Passing to the limit in the weak formulation $\int_{\Omega} \rho^n \varphi_t + f(\rho^n, w) \varphi_x dt dx = 0$ (where $\Omega \subset\subset [0, T] \times [0, L]$ and $\varphi \in C_0^\infty$) we have that ρ^* is a weak entropic solution. We can pass to the limit also in the left boundary condition because this is equivalent to $\rho_l(t) = \frac{In(t)}{v(t)}$ and v is bounded from below. Finally ρ^* is a solution to (3). The standard Kruzhkov entropy condition [32] and [6, Theorem 2] ensure uniqueness of the solution. Since $Out(t) = \rho(t, L)v(t)$, we have that $Out(t)$ has bounded variation and satisfies Proposition 2.2. \square

To simplify notation, we further make the following assumptions.

Hypothesis 2.3. We assume Hypothesis 2.1 and the following:

$$\rho_0^{\min} \leq \frac{f_{\min}}{v_{\max}} \quad \text{and} \quad \rho_0^{\max} \geq \frac{f_{\max}}{v_{\min}}.$$

Given a control policy v , we can define an LET function $\tau = \tau(t, v)$ representing the entering time for a car exiting the road at time t . The function depends on the control policy v , but for simplicity we will write $\tau(t)$ when the policy is clear from the context. Notice that LET is defined only for a time greater than a given $t_0 > 0$, the exit time of the car entering the road at time $t = 0$; see Figure 2. Note that t_0 satisfies $\int_0^{t_0} v(s)ds = L$ and, for each $t \geq t_0$,

$$(7) \quad \int_{\tau(t)}^t v(s)ds = L.$$

Such $\tau(t)$ is unique, due to the hypothesis $v \geq v_{\min} > 0$. From the identity

$$\int_{\tau(t_1)}^{\tau(t_2)} v(s)ds = \int_{t_1}^{t_2} v(s)ds,$$

we get the following.

LEMMA 2.4. *Given a control policy v , the function τ is a Lipschitz continuous function with Lipschitz constant $\frac{v_{\max}}{v_{\min}}$.*

Recalling the definition of outflow of the solution given in (4), we get the following.

PROPOSITION 2.5. *The input-output flow map of the initial boundary value problem (3) is given by*

$$(8) \quad \text{Out}(t) = \text{In}(\tau(t)) \frac{v(t)}{v(\tau(t))}.$$

Proof. Thanks to Proposition 2.2, the solution ρ to the initial boundary value problem (3) satisfies $\rho(t, x) \leq \rho_{cr}$, thus ρ solves a conservation law linear in ρ . Indeed the Newell–Daganzo flow is linear in the free flow zone. Therefore, no shock is produced inside the domain $[0, L]$ and characteristics are defined for all times. In particular the value of ρ is constant along characteristics. The characteristic exiting the domain at time t enters the domain from the boundary at time $\tau(t)$. Therefore we get $\rho(t, L) = \rho(0, \tau(t)) = \frac{\text{In}(\tau(t))}{v(\tau(t))}$. From (4) we get the desired conclusion. \square

Remark 2.6. This map is highly nonlinear with respect to the control policy v due to the definition of τ . Hence, the classical techniques of linear control cannot be applied. Moreover, such a formulation clearly shows how delays enter the input-output flow map. The effect of the control v at time t on the outflow depends on the choice of v on the time interval $[\tau(t), t]$, because of the presence of the LET map in formula (8).

2.2. Optimal control problem. We are now ready to define formally the problem of outflow tracking.

Problem 2.7. Let Hypothesis 2.3 hold, fix $f^* \in \text{BV}([0, T], [f_{\min}, f_{\max}])$ and $K > 0$. Find the control policy $v \in \text{BV}([0, T], [v_{\min}, v_{\max}])$ with $\text{TV}(v) \leq K$, which minimizes the functional $J : \text{BV}([0, T], [v_{\min}, v_{\max}]) \rightarrow \mathbb{R}$ defined by

$$(9) \quad J(v) := \int_0^T (\text{Out}(t) - f^*(t))^2 dt,$$

where $\text{Out}(t)$ is given by (8).

We prove later on, in Proposition 2.15, that Problem 2.7 admits a solution.

Remark 2.8. We use the same positive extreme values f_{\min}, f_{\max} for both the inflow $\text{In}(\cdot)$ and the target outflow $f^*(\cdot)$ for simplicity of notation only.

Remark 2.9. In the simple case where all the parameters are constant in time, i.e., $\text{In}, \text{Out}, f^*, \rho_0$ do not depend on time, the problem has a a trivial solution which is $v = \frac{f^*}{\rho_0}$ realizing $J(v) = 0$.

2.3. Cost variation as function of control policy variation. In this section we estimate the variation of the cost $J(v)$ with respect to the perturbations of the control policy v . This computation will allow to prove continuous dependence of the solution from the control policy.

We first fix the notation for integrals of the BV function with respect to Radon measures.

DEFINITION 2.10. *Let ϕ be a BV function and μ a Radon measure. We define*

$$\int \phi(x^+) d\mu(x) := \int \phi(x) d\mu_c(x) + \sum_i m_i \phi(x_i^+),$$

where $\mu = \mu_c + \sum_i m_i \delta_{x_i}$ is the decomposition of μ into its continuous¹ and Dirac parts.

¹We recall that any Radon measure on \mathbb{R} can be decomposed into its continuous (AC + Cantor) and Dirac parts, as a consequence of the Lebesgue decomposition Theorem; see, e.g., [17].

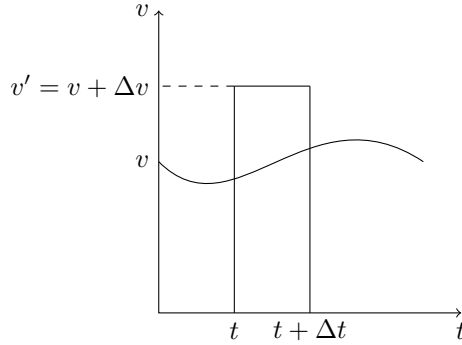


FIG. 3. Needle-like variation of the velocity v .

We now compute the variation in the cost J produced by needle-like variation in the control policy $v(\cdot)$, i.e., variation of the value of $v(\cdot)$ on small intervals of the type $[t, t + \Delta t]$ in the same spirit as the needle variations of the Pontryagin maximum principle [8]. The analytical expression of variations will allow us to implement a steepest-descent-type strategy to find the optimal speed limit.

DEFINITION 2.11. Consider $v \in \text{BV}([0, T], [v_{\min}, v_{\max}])$ and a time t such that $\tau^{-1}(0) = t_0 \leq t < \tau(T)$ and $v(t^+) < v_{\max}$. Let $\Delta v > 0$, $\Delta t > 0$ be sufficiently small such that $t + \Delta t \leq \tau(T)$ and $v(t^+) + \Delta v \leq v_{\max}$. We define a needle-like variation $v'(\cdot)$ of v , corresponding to t , Δt , and Δv by setting $v'(s) = v(s) + \Delta v$ if $s \in [t, t + \Delta t]$ and $v'(s) = v(s)$ otherwise; see Figure 3.

LEMMA 2.12. Consider $v \in \text{BV}([0, T], [v_{\min}, v_{\max}])$ and let v' be a needle-like variation of v . Then it holds that

$$\begin{aligned}
 & \lim_{\Delta v \rightarrow 0^+} \lim_{\Delta t \rightarrow 0^+} \frac{J(v') - J(v)}{\Delta v} \\
 & = 2\rho^2(t, L^-)v(t^+) - 2\rho(t, L^-)f^*(t^+) \\
 (10) \quad & - \int_{]0, L]} v((t + s(x))^+) d\rho_x^2(t) + 2 \int_{]0, L]} f^*((t + s(x))^+) d\rho_x(t) \\
 & + 2 \frac{\text{In}(t^-)}{v(t^+)} \left(f^*(t^+) - \frac{v(\tau^{-1}(t')^-)}{v(t^+)} \text{In}(t^-) \right),
 \end{aligned}$$

where integrals are defined according to Definition 2.10. For $\Delta v < 0$, the limit for $\Delta v \rightarrow 0^-$ satisfies the same formula with right limits replaced by left limits in the two integral terms in (10).

Remark 2.13. Notice that the condition $\tau^{-1}(0) = t_0 < t$ implies that the outflow $\text{Out}(s) \in [t, t + \Delta t]$, depends only on the inflow $\text{In}(\cdot)$ and not on the initial density ρ_0 . If such a condition is not satisfied, the perturbation given by Δv has a comparable effect on $\text{Out}(\cdot)$, but it needs to be estimated in two parts: one with respect to $\text{In}([0, t + \Delta t])$ and one with respect to $\rho_0(0, L - l)$ with l being such that

$$\int_0^t v(s) ds = l.$$

The condition $t + \Delta t \leq \tau(T)$ means that the perturbation Δv has influence on the whole outflow $\text{Out}(s)$ in the interval $[t, \tau^{-1}(t + \Delta t)]$. If this is not satisfied, then the

influence of the perturbation is stopped at $T < \tau^{-1}(t + \Delta t)$, hence, the variation $\text{Out}(s)$ is smaller.

Proof. Let $\tau(t)$ be defined according to (7) and an outflow $\text{Out}(t)$ according to (8). For simplicity we assume that $v(\cdot)$ has a constant value $\hat{v} := v(t^+)$ on $[t, t + \Delta t]$, the general case holding because of properties of BV functions.

We define $t' = t + \Delta t$ and s' to be the unique value satisfying

$$\int_0^{s'} v(t' + \sigma) d\sigma = L - (\hat{v} + \Delta v)\Delta t,$$

s'' to be the unique value satisfying

$$\int_0^{s''} v(t' + \sigma) d\sigma = L - \hat{v}\Delta t,$$

and $s''' = \tau^{-1}(t') - t'$, hence, $\int_0^{s'''} v(t' + \sigma) d\sigma = L$. Notice that $s' < s'' < s'''$. We also define the function

$$(11) \quad x(s) = L - \int_0^s v(t' + \sigma) d\sigma.$$

Remark that $x(s)$ is a decreasing function, with $x(0) = L$, $x(s') = (\hat{v} + \Delta v)\Delta t$, $x(s'') = \hat{v}\Delta t$, and $x(s''') = 0$. We denote with $\text{Out}'(s)$ the outflow, $\tau'(s)$ the LET (see (7)), and $\rho'(s, x)$ the density for the policy v' . Clearly, we have $\text{Out}'(s) = \text{Out}(s)$ for $s \in [0, t] \cup [\tau^{-1}(t'), T]$ and $\tau'(s) = \tau(s)$ for $s \in [t_0, t] \cup [\tau^{-1}(t'), T]$.

To compute the variation, we distinguish four time intervals: $I_1 = (t, t')$, $I_2 = (t', t' + s')$, $I_3 = (t' + s', t' + s'')$, and $I_4 = (t' + s'', \tau^{-1}(t'))$; see Figure 4. The variation of the cost in the first interval can be directly computed as a function of the velocity variation, while in the other intervals the delays in the outflow formula (8) will render the computation more involved. We denote with J_1, \dots, J_4 the contributions to $\lim_{\Delta t \rightarrow 0^+} (J(v') - J(v))/\Delta v$ in the four intervals and estimate them separately.

Case 1. $I_1 = (t, t')$. Let $s \in [0, t' - t] = [0, \Delta t]$, then $\text{Out}(t + s) = \rho(t, L - s\hat{v})\hat{v}$ and $\text{Out}'(t + s) = \rho(t, L - s(\hat{v} + \Delta v))(\hat{v} + \Delta v)$. We have

$$(12) \quad J_1 = \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_0^{\Delta t} (\text{Out}'(t + s) - f^*(t + s))^2 ds - \int_0^{\Delta t} (\text{Out}(t + s) - f^*(t + s))^2 ds \right]$$

$$(13) \quad = \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_0^{\Delta t} \text{Out}'^2(t + s) - \text{Out}^2(t + s) - 2f^*(t + s) (\text{Out}'(t + s) - \text{Out}(t + s)) ds \right].$$

Substituting the expressions for the outflows we get

$$\lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_0^{\Delta t} \rho^2(t, L - s(\hat{v} + \Delta v))(\hat{v} + \Delta v)^2 - \rho^2(t, L - s\hat{v})\hat{v}^2 ds - \int_0^{\Delta t} 2f^*(t + s) (\rho(t, L - s(\hat{v} + \Delta v))(\hat{v} + \Delta v) - \rho(t, L - s\hat{v})\hat{v}) ds \right].$$

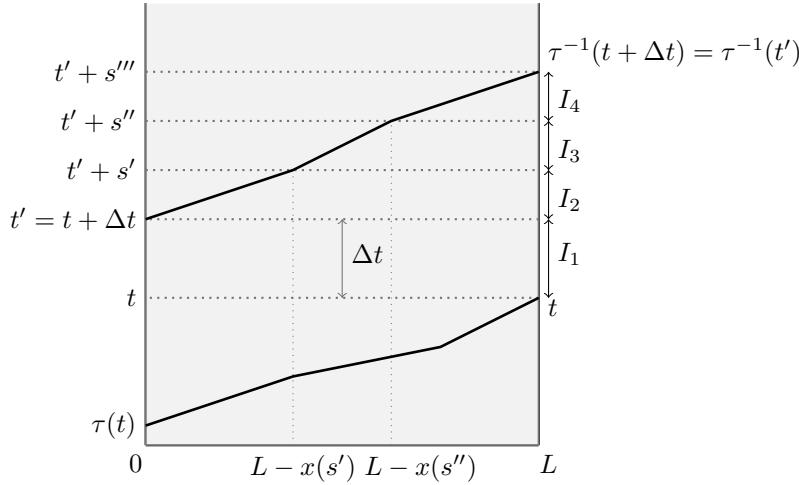


FIG. 4. Graphical representation for the notation used in subsection 2.3.

Dividing the first integral into two parts and making the change of variable $\sigma = s \frac{\hat{v} + \Delta v}{\hat{v}}$,

$$\lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_0^{\Delta t(1 + \frac{\Delta v}{\hat{v}})} \rho^2(t, L - \sigma \hat{v})(\hat{v} + \Delta v)^{\frac{2}{p}} \frac{\hat{v}}{\hat{v} + \Delta v} d\sigma - \int_0^{\Delta t} \rho^2(t, L - s\hat{v})\hat{v}^2 ds - \int_0^{\Delta t} 2f^*(t + s) \left(\hat{v}(\rho(t, L - s(\hat{v} + \Delta v)) - \rho(t, L - s\hat{v})) + \Delta v(\rho(t, L - s(\hat{v} + \Delta v))) \right) ds \right].$$

After simple algebraic manipulation we get

$$\lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_0^{\Delta t(1 + \frac{\Delta v}{\hat{v}})} \rho^2(t, L - s\hat{v})\Delta v \hat{v} ds + \int_{\Delta t}^{\Delta t(1 + \frac{\Delta v}{\hat{v}})} \rho^2(t, L - s\hat{v})\hat{v}^2 ds - \int_0^{\Delta t} 2f^*(t + s) \left(\hat{v}(\rho(t, L - s(\hat{v} + \Delta v)) - \rho(L - s\hat{v})) + \Delta v(\rho(t, L - s(\hat{v} + \Delta v))) \right) ds \right],$$

$$\lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_0^{\Delta t} \rho^2(t, L - s\hat{v})\Delta v \hat{v} ds + \int_{\Delta t}^{\Delta t(1 + \frac{\Delta v}{\hat{v}})} \rho^2(t, L - s\hat{v})(\hat{v}^2 + \Delta v \hat{v}) ds - \int_0^{\Delta t} 2f^*(t + s) \left(\hat{v}(\rho(t, L - s(\hat{v} + \Delta v)) - \rho(t, L - s\hat{v})) + \Delta v(\rho(t, L - s(\hat{v} + \Delta v))) \right) ds \right].$$

Taking the limit as $\Delta t \rightarrow 0^+$, we get

$$\rho^2(t, L^-)\hat{v}\Delta v + \rho^2(t, L^-)\hat{v}(\hat{v} + \Delta v) \frac{\Delta v}{\hat{v}} - 2f^*(t^+)[\hat{v}(\rho(t, L^-) - \rho(t, L^-))] - 2f^*(t^+)\Delta v \rho(t, L^-) = \rho^2(t, L^-)\hat{v}\Delta v + \rho^2(t, L^-)(\hat{v} + \Delta v)\Delta v - 2f^*(t^+)\Delta v \rho(t, L^-),$$

hence,

$$J_1 = 2\rho^2(t, L^-)\hat{v} + \rho^2(t, L^-)\Delta v - 2f^*(t^+)\rho(t, L^-),$$

thus

$$\lim_{\Delta v \rightarrow 0^+} J_1 = 2\rho^2(t, L^-)v(t^+) - 2f^*(t^+)\rho(t, L^-).$$

Case 2. $I_2 = (t', t' + s')$. If $s \in [0, s']$ then $\text{Out}(t' + s) = \rho(t', x(s))v(t' + s)$ and $\text{Out}'(t' + s) = \rho((t', x(s) - \Delta v \Delta t))v(t' + s)$. After decomposing J_2 as was done for J_1 in (12) and plugging in the expression of the outflows, we have

(14)

$$J_2 = \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_0^{s'} v^2(t' + s) \left(\rho^2(t', x(s) - \Delta v \Delta t) - \rho^2(t', x(s)) \right) ds - \int_0^{s'} 2f^*(t' + s)v(t' + s) \left(\rho(t', x(s) - \Delta v \Delta t) - \rho(t', x(s)) \right) ds \right].$$

Applying the change of variable $s \rightarrow x(s)$ (see (11)), it holds

$$J_2 = \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_{0^+}^L v(t' + s(x)) \left(\rho^2(t', x - \Delta v \Delta t) - \rho^2(t', x) \right) dx - \int_{0^+}^L 2f^*(t' + s(x)) \left(\rho(t', x - \Delta v \Delta t) - \rho(t', x) \right) dx \right].$$

Notice that this change of variable is justified by Lemma A.1 of the appendix. Using Lemma A.2 of the appendix, we get

$$\lim_{\Delta v \rightarrow 0^+} J_2 = - \int_{0^+}^L v((t' + s(x))^+) d\rho_x^2(t', x) + 2 \int_{0^+}^L f^*((t' + s(x))^+) d\rho_x(t', x).$$

Case 3. $I_3 = (t' + s', t' + s'')$. If $s \in [s', s'']$ then $\text{Out}(t' + s) = \rho(t', x(s))v(t' + s)$ and

$$\text{Out}'(t' + s) = v(t' + s) \frac{g(s)}{\hat{v} + \Delta v}, \quad g(s) = \ln \left(t' - \frac{x(s)}{\hat{v} + \Delta v} \right).$$

After decomposing J_3 as was done for J_1 in (12) and plugging in the expression of the outflows, we get

$$\lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_{s'}^{s''} v^2(t' + s) \frac{g^2(s)}{(\hat{v} + \Delta v)^2} - \rho^2(t', x(s))v^2(t' + s) - 2f^*(t' + s) \left(v(t' + s) \frac{g(s)}{\hat{v} + \Delta v} - \rho(t', x(s))v(t' + s) \right) \right] ds.$$

Observe that $\lim_{\Delta t \rightarrow 0^+} s' = \lim_{\Delta t \rightarrow 0^+} s'' = \tau^{-1}(t')^- - t'$ and $\int_{s'}^{s''} v(t' + \sigma) d\sigma = \Delta v \Delta t$, then

$$(15) \quad \Delta v J_3 = \frac{\Delta v}{v(\tau^{-1}(t')^-)} v^2(\tau^{-1}(t')^-) \text{In}^2(t'^-) \left[\left(\frac{1}{\hat{v} + \Delta v} \right)^2 - \left(\frac{1}{\hat{v}} \right)^2 \right] - \frac{\Delta v}{v(\tau^{-1}(t')^-)} 2f^*(\tau^{-1}(t')^-) v(\tau^{-1}(t')^-) \text{In}(t'^-) \left(\frac{1}{\hat{v} + \Delta v} - \frac{1}{\hat{v}} \right),$$

thus

$$\lim_{\Delta v \rightarrow 0^+} J_3 = 0.$$

Case 4. $I_4 = (t' + s'', t' + s''')$. If $s \in [s'', s''']$ then we compute

$$\text{Out}(t' + s) = \frac{h(s)}{\hat{v}} v(t' + s) \quad h(s) = \text{In} \left(t' - \frac{x(s)}{\hat{v}} \right),$$

and

$$\text{Out}'(t' + s) = v(t' + s) \frac{g(s)}{\hat{v} + \Delta v}, \quad g(s) = \text{In} \left(t' - \frac{x(s)}{\hat{v} + \Delta v} \right).$$

We decompose J_4 as was done with J_1 in (12), plug in the expression of the outflows, and use the equality $\int_{s''}^{s'''} v(t' + \sigma) d\sigma = \hat{v}$. Then, denoting $\tilde{v} = v(\tau^{-1}(t')^-)$, we have

$$\Delta v J_4 = \frac{\hat{v}}{\tilde{v}} \left[\tilde{v}^2 \text{In}^2(t'^-) \left[\left(\frac{1}{\hat{v} + \Delta v} \right)^2 - \left(\frac{1}{\hat{v}} \right)^2 \right] - 2f^*(\tau^{-1}(t')^-) \tilde{v} \text{In}(t'^-) \left[\frac{1}{\hat{v} + \Delta v} - \frac{1}{\hat{v}} \right] \right].$$

By passing to the limit, we get

$$\lim_{\Delta v \rightarrow 0^+} J_4 = 2f^*(\tau^{-1}(t')^-) \frac{\text{In}(t'^-)}{\hat{v}} - 2 \frac{\tilde{v}}{\hat{v}^2} \text{In}(t'^-)^2. \quad \square$$

Lemma 2.12 and Remark 2.13 allow us to prove the following.

PROPOSITION 2.14. *For every $K > 0$ and $C > 0$, the functional J is Lipschitz continuous on $\Omega := \{v \in \text{BV}([0, T], [v_{\min}, v_{\max}]) : \text{TV}(v) \leq K\}$ endowed with the norm $\|v\|_{L^1}$.*

Proof. Let $v, v' \in \Omega$. Then $v - v'$ is in $\text{BV}([0, T], [v_{\min}, v_{\max}])$ and can be approximated by piecewise constant functions. This means the $v - v'$ can be approximated in BV by needle-like variations as in Lemma 2.12. The right-hand side of (10) is uniformly bounded (since $v \in \Omega$ and $\rho \in \text{BV}$ with uniformly bounded variation). Therefore we conclude that $|J(v) - J(v')| \leq C \|v - v'\|_{L^1}$ for some $C > 0$. \square

This allows us to prove the following existence result.

PROPOSITION 2.15. *Problem 2.7 admits a solution.*

Proof. $\Omega = \{v \in \text{BV}([0, T], [v_{\min}, v_{\max}]) : \text{TV}(v) \leq K\} \cap \{v \in L^\infty([0, T], [v_{\min}, v_{\max}]) : \|v\|_\infty \leq C\}$ is compact in L^1 (see, e.g., [4]), and J is Lipschitz continuous on Ω , thus there exists a minimizer of Problem 2.7. \square

3. Control policies. In this section, we define three control policies for the time-dependent maximal speed v . The first, called the instantaneous policy, is defined by minimizing the instantaneous contribution for the cost $J(v)$ at each time. We will show that such a control policy does not provide a global minimizer due to delays in the control effect on the cost for Problem 2.7. In particular, due to the bound $v \in [v_{\min}, v_{\max}]$ the instantaneous minimization may induce a larger cost at subsequent times. Then, we introduce a second control policy, called the RE policy. Such a policy uses a random path along a binary tree, which corresponds to the upper and lower bounds for v , i.e., $v = v_{\max}$ and $v = v_{\min}$.

Finally, we introduce an effective strategy, which is one of the main results of the paper. More precisely, a third control policy is searched using a GDM. The classical GDM is based on computing the gradient w.r.t. the control space variable,

in finite or infinite-dimensional setting, and then using steepest descent. We use a different approach and replace the gradient with cost variations computed with respect to needle-like variations in the control policy. This is in line with the spirit of the Pontryagin maximum principle for optimal control problems. Therefore the key ingredient to define the third policy is the explicit computation of the gradient given in section 2.

3.1. Instantaneous policy.

DEFINITION 3.1. *Consider Problem 2.7. Define the instantaneous policy as follows:*

$$(16) \quad v(t) := P_{[v_{\min}, v_{\max}]} \left(f^*(t^-) \cdot \frac{v(\tau(t)^-)}{In(\tau(t)^-)} \right),$$

where the projection $P_{[v_{\min}, v_{\max}]} : \mathbb{R} \rightarrow \mathbb{R}$ is the function

$$(17) \quad P_{[a,b]}(x) := \begin{cases} a & \text{for } x < a, \\ x & \text{for } x \in [a, b], \\ b & \text{for } x > b. \end{cases}$$

Notice that this would be the optimal choice if f^* and In would be constant; see Remark 2.9. The instantaneous policy can also be written directly in terms of the input-output map defined in Proposition 2.5. As we will show later, the instantaneous policy is not optimal in general, i.e., it does not provide an optimal solution v for Problem 2.7. Clearly, it provides the solution in the case of v_{\min} sufficiently small and v_{\max} sufficiently big so that the projection operator reduces to the identity, i.e., $v(t) = P_{[v_{\min}, v_{\max}]} \left(\frac{f^*(t^-)}{\rho(L^-)} \right) = \frac{f^*(t^-)}{\rho(L^-)}$ for all times. Indeed, in this case the output $Out(t)$ coincides with $f^*(t)$, hence the cost $J(v)$ is zero.

3.2. RE policy. The RE policy is defined as follows.

DEFINITION 3.2. *Given the extreme values for the maximal speed, v_{\max} and v_{\min} , and a time step Δt , the RE policy draws sequences of velocities from the set $\{v_{\max}, v_{\min}\}$ corresponding to control policy values on the intervals $[i\Delta t, (i + 1)\Delta t]$.*

Notice that maximal speeds according to this algorithm can be generated for all times, independently of the corresponding solution, in contrast to the instantaneous policy which is based on the maximal speed at previous times. We will use numerical optimization to choose the best among the generated random policies, showing in particular that the instantaneous policy is not optimal in general.

3.3. Gradient method. We use needle-like variations and the analytical expression in (10) to numerically compute one-sided variations of the cost. We consider such variations as estimates of the gradient of the cost in L^1 . More precisely, we give the following definition.

DEFINITION 3.3. *The gradient policy is the result of a first-order optimization algorithm to find a local minimum to Problem 2.7 using the GDM and the expression in (10), stopping at a fixed precision tolerance.*

We will show that the gradient method gives very good results compared to the other policies taking into account the computational complexity.

4. Numerical simulations. In this section we show the numerical results obtained by implementing the policies described in section 3. The numerical algorithm for all the approaches is composed of two steps:

1. Numerical scheme for the conservation law (1). The density values are computed using the classical Godunov scheme, introduced in [23].
2. Numerical solution for the optimal control problem, i.e., computation of the maximal speed using the instantaneous control, RE policy and gradient descent.

Let Δx and Δt be the fixed space and time steps, and set $x_{j+\frac{1}{2}} = j\Delta x$, the cell interfaces such that the computational cell is given by $C_j = [x_{j-\frac{1}{2}}, x_{j+\frac{1}{2}}]$. The center of the cell is denoted by $x_j = (j - \frac{1}{2})\Delta x$ for $j \in \mathbb{Z}$ at each time step $t^n = n\Delta t$ for $n \in \mathbb{N}$. We fix \mathcal{J} the number of space points and T the finite time horizon. We now describe in detail the two steps.

4.1. Godunov scheme for hyperbolic PDEs. The Godunov scheme is a first order scheme, based on an exact solution to Riemann problems. Given $\rho(t, x)$, the cell average of ρ in the cell C_j at time t^n is defined as

$$(18) \quad \rho_j = \frac{1}{\Delta x} \int_{x_{j-\frac{1}{2}}}^{x_{j+\frac{1}{2}}} \rho(t^n, x) dx.$$

Then, the Godunov scheme consists of two main steps:

1. Solve the Riemann problem at each cell interface $x_{j+\frac{1}{2}}$ with initial data (ρ_j, ρ_{j+1}) .
2. Compute the cell averages at time t^{n+1} in each computational cell and obtain ρ_j .

Remark 4.1. Waves in two neighboring cells do not intersect before Δt if the following Courant–Friedrichs–Lewy condition holds:

$$(19) \quad \Delta t \max_{j \in \mathbb{Z}} |f'(\rho_j)| \leq \frac{1}{2} \min_{j \in \mathbb{Z}} \Delta x.$$

The Godunov scheme can be expressed in conservative form as

$$(20) \quad \rho_j^{n+1} = \rho_j^n - \frac{\Delta t}{\Delta x} \left(F(\rho_j^n, \rho_{j+1}^n, v^n) - F(\rho_{j-1}^n, \rho_j^n, v^n) \right),$$

where v^n is the maximal speed at time t^n . Additionally, $F(\rho_j^n, \rho_{j+1}^n, v^n)$ is the Godunov numerical flux that in general has the following expression:

$$(21) \quad F(\rho_j^n, \rho_{j+1}^n, v^n) = \begin{cases} \min_{z \in [\rho_j^n, \rho_{j+1}^n]} f(z, v^n) & \text{if } \rho_j^n \leq \rho_{j+1}^n, \\ \max_{z \in [\rho_{j+1}^n, \rho_j^n]} f(z, v^n) & \text{if } \rho_{j+1}^n \leq \rho_j^n. \end{cases}$$

For clarity, we included as an argument for the Godunov scheme, the maximal velocity so that the dependence of the scheme on the optimal control could be explicit.

4.2. Velocity policies. The next step in the algorithm consists of computing a control policy v that can be used in the Godunov scheme with the different approaches introduced in section 3. In particular, for the instantaneous policy approach we compute the velocity at each time step using the instantaneous outgoing flux. Instead, using the other two approaches, the RE and the GDM, we compute beforehand the value of the velocity at each time step and then use it to solve the conservation law with the Godunov scheme.

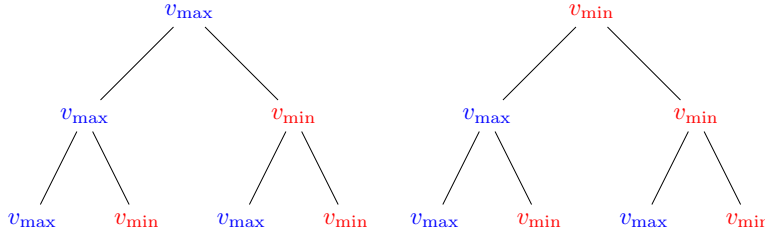


FIG. 5. The first branches of the binary tree used for sampling the velocity.

4.2.1. Instantaneous policy. We follow the control policy described in subsection 3.1 for the instantaneous control. At each time step, the velocity v^{n+1} is computed using the following formula:

$$(22) \quad v^{n+1} = v(t^{n+1}) = P_{[v_{\min}, v_{\max}]} \left(\frac{f^*(t^n)}{\rho_{\mathcal{J}}^n} \right).$$

4.2.2. RE policy. To compute for each time step the value of the velocity, we use a randomized path on a binary tree; see Figure 5. With such a technique, we obtain several sequences of possible velocities. For each sequence the velocities are used to compute the fluxes for the numerical simulations. We then choose the sequence that minimizes the cost.

Remark 4.2. Notice that the control policy RE may have a very large total variation, thus it might not respect the bounds on TV given in Problem 2.7. Therefore the found control policies may not be allowed as a solution of this problem. However, we implement this technique for comparison with the results and performances obtained by the GDM.

4.2.3. Gradient descent method. We first numerically compute one-sided variations of the cost using (10). Then, we use the classical GDM [3] to find the optimal control strategy and to compute the optimal velocity that fits the given outflow profile, as described in Algorithm 1.

Algorithm 1 Algorithm for the gradient descent and computation of the optimal control.

Input data: Initial and boundary condition for the PDE and initial velocity
 Fix a step tolerance ϵ and find a suitable step size α
while $|J_{i+1} - J_i| \leq \epsilon$ **do**
 Compute numerically cost variations ∇J_i
 Update the optimal velocity $v_{i+1} = v_i - \alpha \nabla J_i$
 Compute the new densities using the Godunov scheme
 Compute the new value of the cost functional
end while

Remark 4.3. One might be interested in solving the optimal control problem by applying an adjoint method, as is classical for finite-dimensional control systems. Unluckily, for the problem described here by a partial differential equation, adjoint equations are still unknown.

One might then discretize the dynamics, solve the finite-dimensional problem with an adjoint equation, and finally pass to the limit. While we showed in [18] that one can find minimizers by discretization for some specific mean-field equations, there is

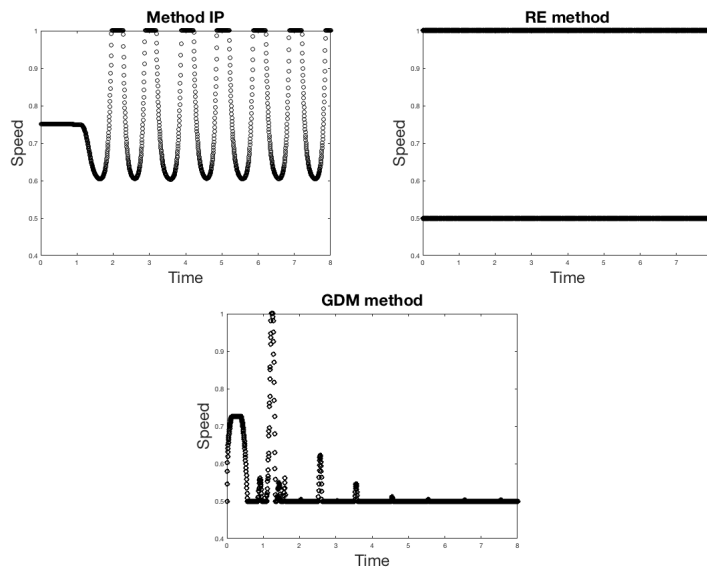


FIG. 6. Speed obtained by using the instantaneous policy (top, left), RE policy (top, right), and the GDM (bottom) for a target flux $f^* = 0.3$.

TABLE 1

Value of the cost functional and the average velocity for the different policies.

Method	Cost Functional	Average Speed
Fixed speed $v = v_{\max} = 1.0$	873.0786	1.0
Fixed speed $v = v_{\min} = 0.5$	785.2736	0.5
Instantaneous policy	850.3704	0.7867
Minimum of RE policy	723.6733	0.7597
Gradient method	735.0565	0.5241

no evidence that such a technique could work for the problem described here. In particular, there is no evidence that the sequence of minimizers of the discretized problem converge to the minimizer of the original one.

4.3. Simulations. We set the following parameters: $L = 1$, $\mathcal{J} = 100$, $T = 15.0$, $\rho_{cr} = 0.5$, $\rho_{\max} = 1$, $v_{\min} = 0.5$, $v_{\max} = 1.0$. Moreover, the input flux at the boundary of the domain is given by $In = \min(0.3 + 0.3 \sin(2\pi t^n), 0.5)$. We choose two different target fluxes $f^* = 0.3$ and $f^* = |(0.4 \sin(t\pi - 0.3))|$. The initial condition is a constant density $\rho(0, x) = 0.4$. We use oscillating inflows to represent variations in typical inflow of urban or highway networks at the 24 h time scale.

4.3.1. Test I: Constant outflow. In Figure 6, we show the time-varying speed obtained by using the instantaneous policy (left) and by using the GDM (bottom). In each case, we notice that due to the oscillating input signal the control policy is also oscillating. We are aware, however, that from a practical point of view, the solution where the speed changes at each time step might be unfeasible. Nonetheless, these policies can be seen as a periodic change of maximal speed for different time frames during the day when the time horizon is scaled to the day length.

In Table 1, we see the different results obtained for the cost functional computed at the final time for the different policies. For comparison, we also put the results of

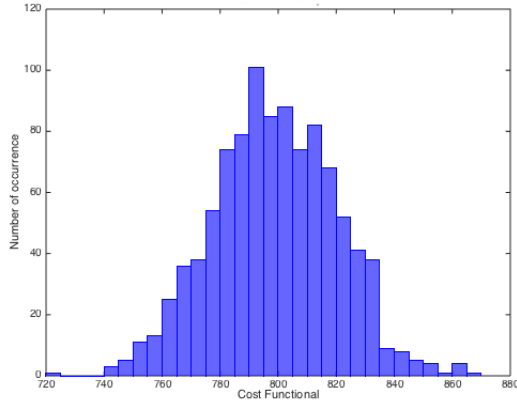


FIG. 7. Histogram of the distribution of the value of the cost functional for the RE policy. We run 1000 different simulations.

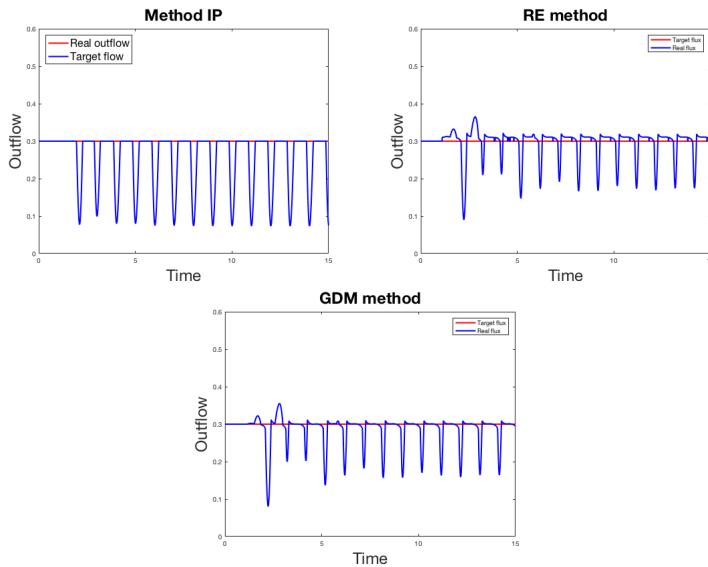


FIG. 8. Difference between the real outgoing flux and the target constant flux, computed with the instantaneous policy (top, left), the gradient method (top, right) and the RE policy (bottom).

the simulations with a constant speed equal to the minimum and maximal velocity bounds. The instantaneous policy is outperformed by the RE policy and by the gradient method. For the RE policy, in the table we put the minimal value of the cost functional computed by the algorithm. In Figure 7 we can see the distribution of the different values of the cost functional over 1000 simulations. Moreover, in Figure 8, we can see the differences between the actual outflow obtained and the target one for all methods.

We also compared the CPU time for the different simulations approaches (see Table 2). As expected, the RE policy is the least performing while the instantaneous policy is the fastest one. In addition, we computed the $TV(v)$ for each one of the policies obtaining the following results:

TABLE 2
CPU Time for the simulations performed with the different approaches.

Method	CPU Time (s)
Instantaneous policy	32.756
RE policy	7577.390
Gradient method	1034.567

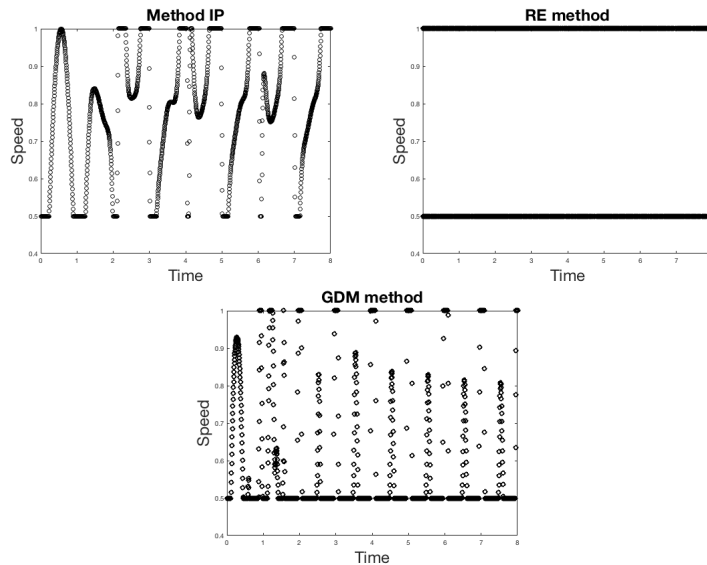


FIG. 9. Speed obtained by using the instantaneous policy (top, left), RE policy (top, right), and the GDM (bottom) and the gradient GDM (bottom) for a sinusoidal target flux.

- Instantaneous policy: $TV(v) = 12.6904$
- RE: $TV(v) = 753.5$
- GDM: $TV(v) = 70.81333$.

4.3.2. Test II: Sinusoidal outflow. In Figure 9, we show the optimal velocity obtained by using the instantaneous policy and by using the GDM with a sinusoidal outflow. We show in Figure 10 the histogram of the cost functional obtained for the RE policy and in Figure 11 we compare the real outgoing flux with the target one. In Table 3, different results obtained for the cost functional computed at the final time for the different policies are shown. Also in this case the instantaneous policy is outperformed by the other two. The CPU times give results similar to the previous test.

5. Conclusions. In this work, we studied an optimal control problem for traffic regulation on a single road via variable speed limit. The traffic flow is described by the LWR model equipped with the Newell–Daganzo flux function. The optimal control problem consists in tracking a given target outflow in free flow conditions. We proved the existence of a solution for the optimal control problem and provided explicit analytical formulas for cost variations corresponding to needle-like variations of the control policy. We proposed three different control policy designs: instantaneous depending only on the instantaneous downstream density, random simulations, and

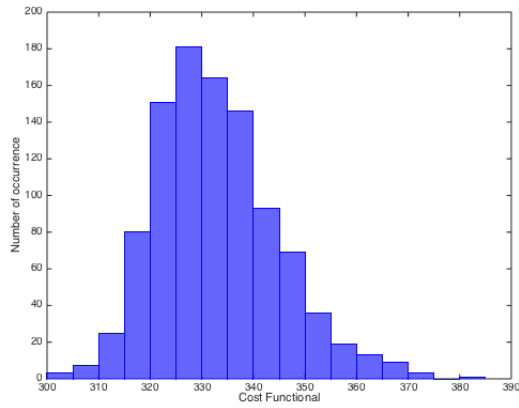


FIG. 10. Histogram of the distribution of the value of the cost functional for the RE policy. We run 1000 different simulations.

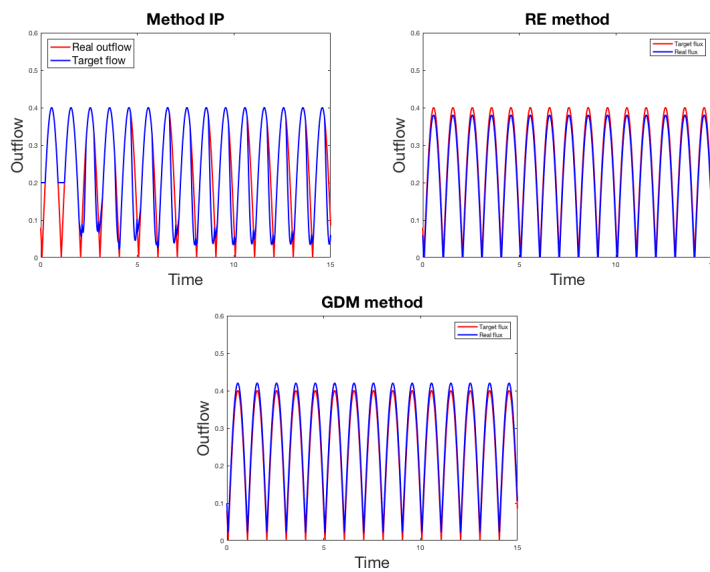


FIG. 11. Difference between the real outgoing flux and the target sinusoidal flux, computed with the instantaneous policy (top, left), the RE (top, right) and the gradient method (bottom).

TABLE 3
Value of the cost functional for the different policies.

Method	Cost functional	Average speed
Fixed speed $v = v_{\max} = 1.0$	$1.3979e + 03$	1.0
Fixed speed $v = v_{\min} = 0.5$	843.3395	0.5
Instantaneous policy	458.8874	0.7917
Minimum of RE policy	303.8327	0.7512
Gradient method	307.6889	0.6001

gradient descent. The latter, based on numerical simulations for the cost variation, represents the best compromise between performance, computational cost, and total variation of the control policy.

Future works will include the study of this problem in the case of congestion and the extension to second order traffic flow models.

Appendix A.

LEMMA A.1. *Let $\beta, T > 0$ and $\varphi \in \text{BV}([0, T], \mathbb{R}^+)$ be given.*

Define $L := \int_0^T \varphi(\sigma) d\sigma$ and the function $x : [0, T] \rightarrow [0, L]$ by $x(s) := L - \int_0^s \varphi(\sigma) d\sigma$, that is invertible. Define $\alpha \geq \beta$ and the function $\bar{t} : (0, \frac{L}{\alpha}] \rightarrow [0, L]$ such that $\bar{t}(\Delta t)$ is the unique solution of $\int_0^{\bar{t}(\Delta t)} \varphi(\sigma) d\sigma = L - \alpha \Delta t$.

It then holds

$$(23) \quad \begin{aligned} & \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_0^{\bar{t}(\Delta t)} \varphi^2(s) \left(\psi(x(s) - \beta \Delta t) - \psi(x(s)) \right) ds \right] \\ &= \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_{0^+}^L \varphi(s(x)) \left(\psi(x - \beta \Delta t) - \psi(x) \right) dx \right]. \end{aligned}$$

Proof. The change of variable $s \rightarrow x(s)$ inside the integral gives

$$(24) \quad \begin{aligned} & \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \left[\int_0^{\bar{t}(\Delta t)} \varphi^2(s) \left(\psi(x(s) - \beta \Delta t) - \psi(x(s)) \right) ds \right] \\ &= \lim_{\Delta t \rightarrow 0^+} -\frac{1}{\Delta t} \int_L^{\alpha \Delta t} \varphi(s(x)) \left(\psi(x - \beta \Delta t) - \psi(x) \right) dx, \end{aligned}$$

$$(25) \quad \begin{aligned} & \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \int_{0^+}^L \varphi(s(x)) \left(\psi(x - \beta \Delta t) - \psi(x) \right) dx \\ & - \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \int_{0^+}^{\alpha \Delta t} \varphi(s(x)) \left(\psi(x(s) - \beta \Delta t) - \psi(x(s)) \right) dx, \end{aligned}$$

where $s(x)$ is uniquely determined by the invertibility of the function $x(s)$. Observe that we need to specify the 0^+ extremum in the integral, since the limit will provide Dirac terms inside the integral. We want to now prove that the last addendum tends to zero. Denote by ψ_x the distributional derivative of ψ , which is a measure, and decompose it as in the continuous (AC + Cantor) and Dirac part. By integrating ψ_x , we write $\psi = \tilde{\psi} + \sum_i m_i \chi_{[x_i, L]}$ with $\tilde{\psi}$ a continuous function, $m_i > 0$, $\sum_i m_i < +\infty$, and $x_i \in [0, L]$. Hence, by the mean value theorem applied to $\tilde{\psi}$, we have

$$(26) \quad \begin{aligned} & \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \int_{0^+}^{\alpha \Delta t} \varphi(s(x)) \left| \tilde{\psi}(x(s) - \beta \Delta t) - \tilde{\psi}(x(s)) \right| dx \\ & \leq \lim_{\Delta t \rightarrow 0^+} \|\varphi\|_\infty \alpha \left| \tilde{\psi}(\tilde{x} - \beta \Delta t) - \tilde{\psi}(\tilde{x}) \right| = 0, \end{aligned}$$

where $\tilde{x} \in (0, \alpha \Delta t)$ is a point (depending on Δt) and the limit is zero as a consequence of the continuity of $\tilde{\psi}$. The remaining term in (25) is then

$$\begin{aligned} & \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \int_{0^+}^{\alpha \Delta t} \varphi(s(x)) \sum_{x_i \in (0, \alpha \Delta t]} m_i (\chi_{[x_i - \beta \Delta t, L]} - \chi_{[x_i, L]}) dx \\ &= \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \sum_{x_i \in (0, \alpha \Delta t]} \varphi(s(x_i)^-) m_i \beta \Delta t \leq \lim_{\Delta t \rightarrow 0^+} \beta \|\varphi\|_\infty \sum_{x_i \in (0, \alpha \Delta t]} m_i. \end{aligned}$$

Since ψ is in BV the quantity $\sum_{x_i \in (0, \alpha \Delta t]} m_i$ tends to zero as Δt tends to zero, thus we conclude. \square

LEMMA A.2. Let $\varphi, \psi \in \text{BV}([a - \varepsilon, b + \varepsilon], \mathbb{R})$, then

$$(27) \quad \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \int_a^b \varphi(x) (\psi(x - C\Delta t) - \psi(x)) dx = -C \int_a^b \varphi(x^+) d\psi_x(x),$$

where the integral in the right-hand side is defined in Definition 2.10.

Proof. We decompose the measure ψ_x as $\psi_x = \ell d\lambda + \sum_i m_i \delta_{x_i}$, where λ is the Lebesgue measure, ℓ the Radon–Nikodym derivative of ψ_x w.r.t. λ , $m_i > 0$, and $\sum_i m_i < +\infty$. We approximate ψ by piecewise continuous functions ψ^n defined as the integrals of $\psi_x^n = \ell d\lambda + \sum_{i \leq N(n)} m_i \delta_{x_i}$, where $N(n)$ is chosen such that $\sum_{i > N(n)} m_i < \frac{1}{n}$.

Define $I(n) = \cup_{i=1}^{N(n)} [x_i, x_i + C\Delta t]$ and by I_c its complement in $[a, b]$. Notice that for $x \in [x_i, x_i + C\Delta t]$ we have $\psi^n(x - C\Delta t) - \psi^n(x) = -m_i - \int_{x-C\Delta t}^x \ell d\lambda$ while on I_c there are no jumps so $\psi^n(x - C\Delta t) - \psi^n(x) = -\int_{x-C\Delta t}^x \ell d\lambda$. We thus can write

$$(28) \quad \begin{aligned} & \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \int_a^b \varphi(x) (\psi^n(x - C\Delta t) - \psi^n(x)) dx \\ &= \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \sum_{i=1}^{N(n)} \int_{x_i}^{x_i + C\Delta t} \varphi(x) (\psi^n(x - C\Delta t) - \psi^n(x)) dx \\ & \quad + \int_{I_c} \varphi(x) (\psi^n(x - C\Delta t) - \psi^n(x)) dx \\ &= \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \sum_{i=1}^{N(n)} (-m_i) \int_{x_i}^{x_i + C\Delta t} \varphi(x) dx - \frac{1}{\Delta t} \int_a^b \varphi(x) \int_{x-C\Delta t}^x \ell d\lambda dx. \end{aligned}$$

Since φ is in BV we can write

$$\begin{aligned} & \lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \int_a^b \varphi(x) (\psi^n(x - C\Delta t) - \psi^n(x)) dx \\ &= -\sum_{i=1}^{N(n)} m_i \varphi(x_i^+) - \int_a^b \varphi(x) d(\ell \lambda) \\ &= -\int_a^b \varphi(x^+) d\left(\sum_{i=1}^{N(n)} m_i \delta_{x_i} + \ell \lambda\right) = -\int_a^b \varphi(x^+) d\psi_x^n \end{aligned}$$

Now, the following estimates hold:

$$\begin{aligned} & \left| \frac{1}{\Delta t} \int_a^b \varphi(x) (\psi^n(x - C\Delta t) - \psi^n(x)) dx - \frac{1}{\Delta t} \int_a^b \varphi(x) (\psi(x - C\Delta t) - \psi(x)) dx \right| \\ &= \left| \frac{1}{\Delta t} \int_a^b \varphi(x) (\psi^n(x - C\Delta t) - \psi(x - C\Delta t)) - (\psi^n(x) - \psi(x)) dx \right|. \end{aligned}$$

We can write $\psi^n(x - C\Delta t) = \psi(a) + \int_a^{x-C\Delta t} d\psi_x^n$ and $\psi(x - C\Delta t) = \psi(a) + \int_a^{x-C\Delta t} d\psi_x$, which gives us

$$= \left| \frac{1}{\Delta t} \int_a^b \varphi(x) \left(\int_a^{x-C\Delta t} dr_n - \int_a^x dr_n \right) dx \right|,$$

where $r_n = \psi - \psi^n$. Taking the limit for $\Delta t \rightarrow 0^+$,

$$\begin{aligned} & \left| \frac{1}{\Delta t} \int_a^b \varphi(x) (\psi^n(x - C\Delta t) - \psi^n(x)) dx - \frac{1}{\Delta t} \int_a^b \varphi(x) (\psi(x - C\Delta t) - \psi(x)) dx \right| \\ & \leq \left| \frac{1}{\Delta t} \int_a^b \varphi(x) \left(- \int_{x-C\Delta t}^x dr_n \right) dx \right| \\ & \leq \|\varphi\|_\infty \frac{1}{\Delta t} \left| \int_a^b \int_{x-C\Delta t}^x dr_n dx \right| \leq \|\varphi\|_\infty \frac{1}{n}. \end{aligned}$$

The last inequality holds true because

$$\int_{x-C\Delta t}^x dr_n = \sum_i m_i \int_{x-C\Delta t}^x d\delta_{x_i} = \sum_i m_i \chi_{[x_i, x_i + C\Delta t]}.$$

Thus we get

$$\lim_{\Delta t \rightarrow 0^+} \frac{1}{\Delta t} \int_a^b \varphi(\psi(x - C\Delta t) - \psi(x)) dx = \mathcal{O}\left(\frac{1}{n}\right) + \int_a^b \varphi(x^+) d\psi_x^n.$$

Let us now estimate the quantity

$$\left| \int_a^b \varphi(x^+) d\psi_x^n - \int_a^b \varphi(x^+) d\psi_x \right|.$$

Recalling that $\psi^n(x - C\Delta t) = \psi(a) + \int_a^{x-C\Delta t} d\psi_x^n$ and $\psi(x - C\Delta t) = \psi(a) + \int_a^{x-C\Delta t} d\psi_x$ we get

$$\left| \int_a^b \varphi(x^+) d \left(\sum_{i \geq N(n)} m_i \delta_{x_i} \right) \right| \leq \|\varphi\|_\infty \frac{1}{n}.$$

Passing to the limit in n we conclude. \square

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