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CICLO XXIII

**Characterization of Electronic  
Circuits with the SIRAD IEEM:  
Developments and First Results**

**Direttore della Scuola :** Ch.mo Prof. Attilio Stella

**Supervisore:** Ch.mo Prof. Dario Bisello

**Correlatore:** Ch.mo Prof. Jeffery Wyss

**Dottorando:** Luca Silvestrin

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# Introduction

When an energetic ion strikes a microelectronic device it induces current transients that may lead to a variety of undesirable Single Event Effects (SEE). An important part of the activity of the SIRAD heavy ion facility at the 15 MV Tandem accelerator of the INFN Laboratories of Legnaro (Italy) concerns SEE studies of microelectronic devices destined for radiation hostile environments.

An axial Ion Electron Emission Microscope (IEEM) is working at the SIRAD irradiation facility. It is devised to provide a micrometric sensitivity map of Single Event Effects of an electronic device. The IEEM system reconstructs the positions of individual random ion impacts over a circular area of 180  $\mu\text{m}$  diameter by imaging the ion-induced secondary electrons emitted from the target surface. A fast Data Acquisition system (DAQ) is used to reconstruct the X and Y coordinates and the temporal information of every ion impact. Any signal induced by the SEE in a generic DUT can be used to tag the IEEM reconstructed event. This information is then used to display a map of the regions of the DUT surface which are sensitive to the impinging ions.

In this thesis we introduce the subject of the effects of ionizing radiation on microelectronics circuits and systems. We then describe in detail the IEEM system, especially how it was modified and improved during the period of our work.

We present the results of an extensive study of the IEEM resolution and image distortions, performed using high statistics acquisitions obtained with a 241 MeV  $^{79}\text{Br}$  ion beam by means of a fast SDRAM-based ion induced single event detection system, specifically designed for this purpose.

We also describe a new feature implemented in the DAQ system which enables the IEEM to perform Time Resolved Ion Beam Induced Charge Collection (TRIBICC) studies, and show preliminary results obtained studying a MOSFET power transistor.

We also studied a digital microelectronic circuit (SOI-Imager Shift Register) in two steps: we measured the SEU cross-section with our broad-beam facility at SIRAD, and then used the IEEM to acquire a SEU sensitivity map.

At present the resolution of the IEEM at SIRAD is not close to the theoretical one. In this thesis we also describe an extensive set of studies we performed to investigate the origin of the resolution degradation.

The *conclusions* follow and close this work.

# Introduzione

Quando uno ione energetico colpisce un dispositivo microelettronico, induce impulsi di corrente che possono generare diversi Single Event Effect (SEE) indesiderati. Una parte importante dell'attività della facility di irraggiamento a ioni pesanti SIRAD, presso il tandem da 15 MV dei Laboratori Nazionali di Legnaro (Italia) dell'INFN, riguarda studi di SEE su dispositivi microelettronici destinati ad ambienti ostili per il livello delle radiazioni.

Presso la facility di irraggiamento SIRAD, e' in funzione un Ion Electron Emission Microscope (IEEM). Esso e' concepito per generare mappe di sensibilità a Single Event Effect di un dispositivo elettronico, con risoluzione micrometrica: il sistema IEEM ricostruisce le posizioni degli impatti di singoli ioni distribuiti casualmente entro un'area di 180  $\mu\text{m}$  di diametro, acquisendo gli elettroni secondari emessi dalla superficie del bersaglio colpita dallo ione. Un sistema di acquisizione veloce (DAQ) è utilizzato per ricostruire le coordinate X ed Y e l'informazione temporale di ogni impatto. Ogni segnale indotto da un SEE in un generico dispositivo sotto test può essere utilizzato per marcare gli eventi ricostruiti dal sistema. Queste informazioni sono in seguito utilizzate per generare una mappa delle aree della superficie del dispositivo che sono sensibili all'impatto ionico.

In questa tesi introduciamo l'argomento degli effetti della radiazione ionizzante sui sistemi e i dispositivi microelettronici e in seguito descriviamo in dettaglio il sistema IEEM, soffermandoci in particolare sulle modifiche e le migliorie introdotte durante questo periodo di lavoro.

Descriviamo un detector di singoli impatti ionici, basato su una SDRAM, con il quale abbiamo ottenuto acquisizioni ad alta statistica usando un fascio di ioni  $^{79}\text{Br}$  da 241 MeV. Questi dati ci hanno consentito uno studio approfondito della risoluzione dell'IEEM e della distorsione dell'immagine generata.

Descriviamo inoltre una nuova caratteristica implementata nel nostro sistema di acquisizione, che consente all'IEEM di effettuare analisi di Time Resolved Ion Beam

Induced Charge Collection (TRIBICC), e illustriamo i risultati preliminari ottenuti studiando un transistor MOSFET di potenza.

Abbiamo infine studiato un circuito microelettronico digitale (SOI-Imager Shift Register) in due fasi: dapprima e' stata misurata la sezione d'urto a SEU con la nostra facility di irraggiamento a fascio non focalizzato, e in seguito l'IEEM e' stato utilizzato per acquisire una mappa di sensibilità a SEU.

Infine, verificato che allo stato attuale la risoluzione dell'IEEM presso SIRAD non e' vicina al valore teorico, in questo lavoro di tesi descriviamo la serie di studi approfonditi condotti al fine di indagare l'origine della degradazione della risoluzione.

# 1 Radiation effects on electronic devices

The effects of ionizing particles in electronic components are due to the formation of trails of electron-hole pairs in the semiconductor material along the particle track. Under the effect of internal or applied electric fields, these charge carriers generate currents in the external circuit as they move and are collected by electrodes. The consequences of localized uncontrolled charge injections due, directly or indirectly, to a single energetic particle have been categorized as Single Event Effects (SEE); they form a large assortment of anomalies in the operations of many types of devices.

In this chapter I will introduce the subject of radiation effects on electronic devices and will focus on the physical processes involved in the production of SEE.

## ***1.1 Charge deposition***

### **1.1.1 Introduction**

There are two primary methods by which charge is released along the path of an ionizing particle: *direct ionization*, due to the coulomb interaction of a charged incident particle with the electrons of the material, and *indirect ionization* when the incident particle interacts (coulomb, nuclear) with the lattice silicon nuclei of the material to produce secondary ionizing particles (recoils, protons, alphas and other nuclear fragments).

### **1.1.2 Direct charge deposition**

When an energetic charged particle passes through a semiconductor material, it frees electron-hole pairs along its path as it loses kinetic energy. When all of its energy is lost, the particle comes to rest in the semiconductor; the total path length

traveled is referred to as the particle's *range*. A frequently used quantity is the rate of energy loss by ionization of the particle, the *linear energy transfer* (LET):

$$(2.1) \quad LET = \frac{1}{\rho} \cdot \frac{dE}{dx}$$

with  $\rho$  the density of the material and  $x$  is the distance along the path of the particle. The LET is frequently expressed in MeV-cm<sup>2</sup>/mg. In these units the energy loss per unit path length (MeV/cm) is normalized by the density of the target material (mg/cm<sup>3</sup>), so that the rate of energy loss can be roughly quoted independently of the target material.

It is easy to relate the LET of a particle to the charge deposition per unit path length, if one knows the average amount of energy that is needed to create an electron-hole pair. Consider silicon: the density is 2328 mg/cm<sup>3</sup> and approximately 3.6 eV energy deposition is needed to release one electron-hole pair [1], hence a LET of 97 MeV-cm<sup>2</sup>/mg corresponds to a linear charge deposition of 1 pC/μm. This conversion factor of about 100 between LET and linear charge deposition in silicon is handy and should be kept in mind. A useful rule of thumb for silicon is that the maximum LET of an ion, expressed in MeV-cm<sup>2</sup>/mg, is roughly equal to its atomic number  $Z$  [2].

The LET is a function of the velocity  $v$  of an ion and can be express as:

$$(2.2) \quad LET(Z, v) = Q^2 \times LET(Z = 1, v) = \eta^2 \times Z^2 \times LET(Z = 1, v),$$

where  $LET(Z = 1, v)$  is the Linear Energy Transfer of a proton with the same velocity  $v$ , and  $\eta$  accounts for the velocity dependence of the effective charge  $Q = \eta \times Z$  of the ion inside the impacted material. The  $LET(Z = 1, v)$  of a proton is given by the Bethe-Boch equation and scales like  $v^{-2}$ . The fractional charge  $\eta$ , function of the atomic number  $Z$  of the species and the ion velocity  $v$ , can be estimated, within a few percent, using the parametric form:



$$(2.3) \quad \eta = 1 - A \times \exp\left(-B \frac{v}{v_{\text{Bethe}}}\right),$$

with  $A = 1$  and  $B \approx 0.95$  [3]. If  $v \gg v_{\text{Bethe}}$  the ion is unable to retain electrons and the charge is the naked nuclear charge  $Z$ . As the ion progresses through the material, it loses energy and slows. When  $v \approx v_{\text{Bethe}}$  the ion picks up electrons and the effective charge decreases further as the slowing ion captures more.

The dependence of the LET as a function of the depth reached by the ion slowing inside a target material is of fundamental interest for understanding the interaction of a given particle with a device.

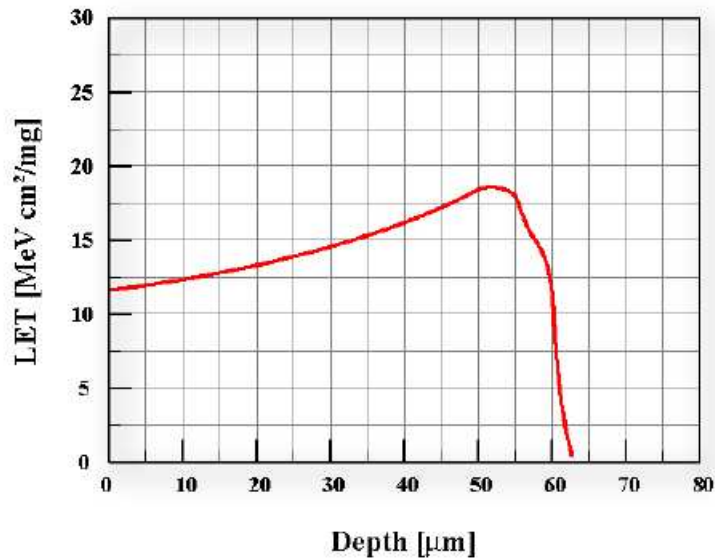


Figure 1.1 LET vs ion depth curve for 210MeV  $^{35}\text{Cl}$  ion in silicon.

Figure. 1.1 shows the average LET as a function of ion depth for a 210 MeV  $^{35}\text{Cl}$  ion traveling through silicon. A peak in the charge deposition occurs at  $\sim 50 \mu\text{m}$  below the silicon surface as the particle nears its range. The rate of ionization then drops as the ion slows and captures more and more electrons, going to zero when the particle becomes a completely neutral atom. The peak in charge deposition is referred to as *Bragg peak*.

### 1.1.3 Indirect charge deposition

Protons and neutrons<sup>1</sup> can both produce significant SEE rates due to indirect mechanism.

As a high energy proton or neutron enters the semiconductor lattice, it may undergo an inelastic collision with a silicon nucleus. This may result in the emission of alpha ( $\alpha$ ) and a recoiling daughter nucleus (e.g. if the Si emits one  $\alpha$ -particle, the recoiling nucleus is Mg), or a spallation reaction, in which the target nucleus is broken into two recoiling fragments (e.g. Si breaks into C and O ions). These heavy reaction products deposit large quantities of energy along their paths by direct ionization, and hence they may induce a SEE. The inelastic collision by-products typically have low energies and do not travel far from the site of the inelastic collision of the primary particle. They also tend to be forwarded scattered in the direction of the primary particle. As a consequence SEE sensitivity is a function of the angle of incidence of the proton or neutron. Low energy neutrons may also indirectly create ionizing secondary particles when they interact with the boron used as a p-type dopant for junction formation in ICs; the isotope  $^{10}\text{B}$  is unstable and neutron capture induces the nucleus to fission into lithium and alpha.

## 1.2 Charge collection

### 1.2.1 Introduction

The basic properties of charge collection following a particle strike have been investigated using several theoretical and experimental methods. The physics of charge collection have been studied through the use of two and three dimensional numerical simulations [4][5] or by measuring induced charge collection transients with ion microbeams and lasers. Ion microbeam and lasers have also been used to map integrated charge collection as a function of both time and position [6] in ICs.

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<sup>1</sup> Pions and kaons are hadronic particles which are produced in large numbers in High Energy Physics experiments at accelerators. Since their effects are very similar to those of protons, they will not be discussed here.

## 1.2.2 Physics of charge transport

There are essentially three mechanisms that act on the charge carriers deposited by an ionizing particle:

- carriers can move by *drift* in response to applied or built-in fields in the device;
- carriers can move by *diffusion* under the influence of carrier concentration gradients within the device;
- carriers can be annihilated by *recombination* through direct or indirect processes.

These three mechanisms are of course not unique to the particle strike problem and are in fact the governing processes of charge transport in semiconductor under most operating conditions.

When an energetic particle hits a microelectronic device, the most sensitive regions are reversed biased p/n junctions. In the high field present in the depletion region of a reversed-biased junction, the charge carriers drift and are efficiently collected by the electrodes. According to Gunn's theorem, the drifting carriers induce a current on electrodes of the device. The induced current appears on an given electrode delayed only by the time necessary to the electrical field to propagate at the speed of light the information about the new charge distribution, and not when the carriers actually reach the electrode. For all practical purposes the signals on all electrodes appear simultaneously and the induced current will appear on an electrode even if the carriers do not really reach them, as when recombine or get trapped, etc.

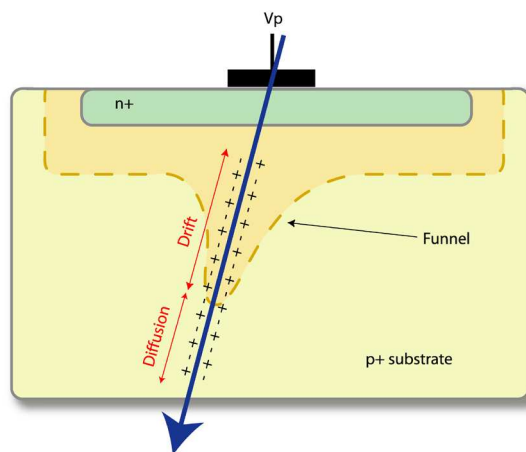
The amount of induced current in the  $i$ -th electrode is:

$$(2.4) \quad I_i = -q\vec{v} \cdot \frac{\partial \vec{E}}{\partial V_i},$$

where  $q$  is the amount of moving charge, **Errore. Non si possono creare oggetti dalla modifica di codici di campo.** is the drift velocity, **Errore. Non si possono creare oggetti dalla modifica di codici di campo.** is the electrical field at the position of the charge,  $V_i$  is the voltage of the  $i$ -th electrode and the derivative is

evaluated keeping the potential constant on all other electrodes. The voltage swing induced by this unwanted current flow can change the logic state of the device, depending on the amount of the induced charge and on the intrinsic properties of the circuit to which the device is connected.

Carriers that are produced outside the sensitive depletion region, where the electrical field is not present, either recombine or diffuse and do not induce a transient current. The carriers that manage to diffuse into the depletion region do induce transient currents as they drift and get collected. It is then clear that the transient induced current will generally have a fast component, due to the prompt drift of carriers created by a direct particle hit in the sensitive region, and a slow component, due to the diffusion of carriers created outside the sensitive region that slowly move into the sensitive region.<sup>2</sup>



**Figure 1.2** Funneling of the junction field to the charge deposited by an ionizing particle.

As a matter of fact, things are a bit more complicated and interesting. Along the path of a heavily ionizing particle the dense non-equilibrium distribution of electron-hole pairs induces a funnel-shaped distortion of the potential that extends the electric field away from the junction and deep into the substrate (Figure. 1.2). This funneling effect enhances charge collection by drift: charge deposited some distance from the junction can be collected through the efficient drift process. The prompt (drift)

<sup>2</sup> It should be noted that a particle hit *near* a depletion region can also result in a significant transient current as carriers diffuse into the depletion region.

collection phase typically follows for tens of picoseconds and as the funnel collapses, diffusion then dominates until all excess carriers have been collected, recombined or diffused away from the junction area. The current transient typically lasts 200 picoseconds with the bulk of the charge collection occurring within 2-3 microns of the junction region for modern submicron CMOS technologies.

### 1.3 Cumulative effects

#### 1.3.1 Introduction

Energetic particles incident in a solid lose their kinetic energy not only by producing electron-hole pairs, but also by displacing atoms as they travel through a given material. Neutrons are particularly good at damaging a silicon lattice. If the energy of the neutron is sufficient, the primary knock-on atom can also displace other atoms in the lattice (~500 for one 1 MeV neutron). For ions the non-ionizing energy loss (NIEL) is particularly important near the end of range, when the ion is slow and elastic coulomb collisions with nuclei become important and dominate the total rate of energy loss (Figure. 1.3).

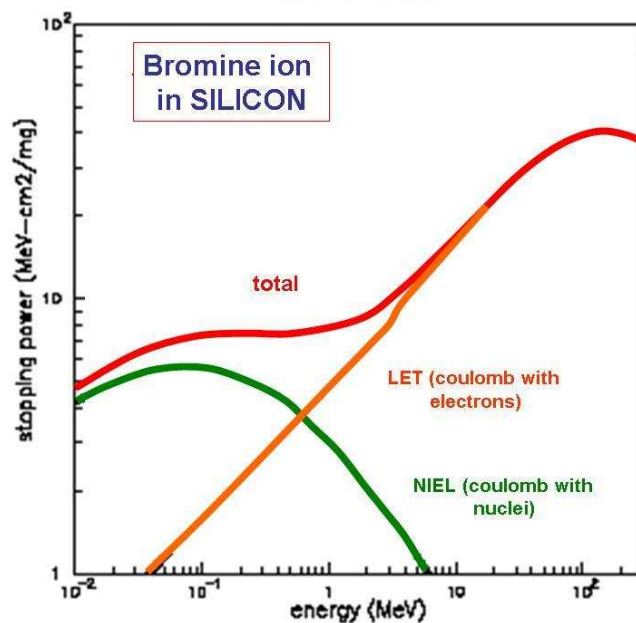


Figure 1.3 Mean LET and NIEL of a bromine ion in silicon as a function of kinetic energy.

In a material like silicon, the accumulation of lattice defects, from the non-ionizing energy loss of a great number of incident particles, will directly affect the minority carrier lifetime and mobility, and this lead to modifications of the electrical characteristics of components (e.g. degradation of electrical parameters; increased leakage current). The effects of non-ionizing energy loss are categorized as *Displacement Damage Dose (DDD)* effects.

When an insulator is exposed to ionizing radiation fixed and charged regions are induced and the material does not return to its initial state. The homogeneous accumulation of charge in oxide layers and Si-SiO<sub>2</sub> interfaces in silicon devices exposed to ionizing radiation is at the origin of the parametric degradation of irradiated devices. These effects are called *Total Ionizing Dose (TID)* effects.

### 1.3.2 Displacement Damage

Defect production:

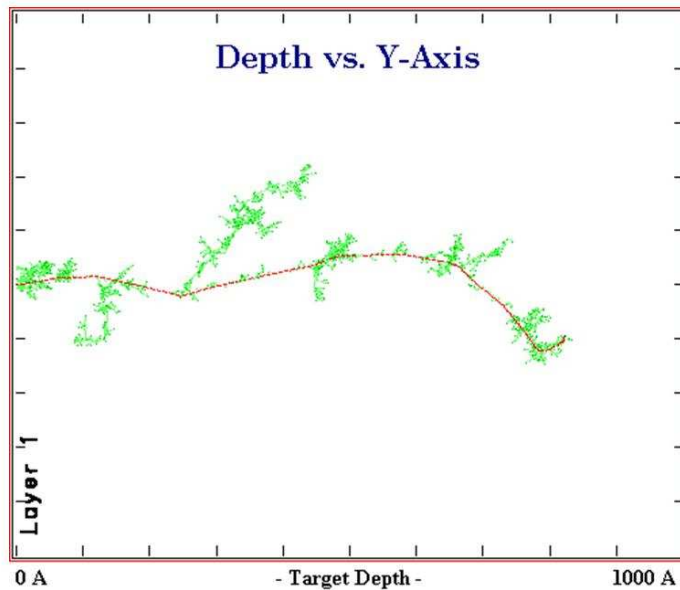
The non-ionizing energy loss produces displaced atoms<sup>3</sup>. The primary lattice defects initially created are vacancies and interstitials. A vacancy is the absence of an atom from its normal lattice position. If the displaced atom moves into a non-lattice position, the resulting defect is called an interstitial. The combination of a vacancy and an adjacent interstitial is known as a close pair or Frenkel pair. As regards the density of defects produced by radiation, at one extreme radiation-induced defects may be relatively far apart and are referred to as point defects or isolated defects. For example, incident electrons and photons with energy of the order of 1 MeV produce such defects. At the other extreme, defects may be produced relatively close together and form a local region of disorder (defect cluster or disordered region), such as those ones produced by incident neutrons with energy of the order of 1 MeV, or by a heavy ions near the end of their range. The mechanism involved is the initial transfer of a significant amount of energy from the particle to a single Si atom. The dislodged primary knock-on atom then displaces many other Si atoms locally, thereby creating a disordered region called a cluster. This may occur several times if the primary knock-on is energetic enough (Figure. 1.4). In general, incident energetic particles produce a mixture of isolated and clustered defects.

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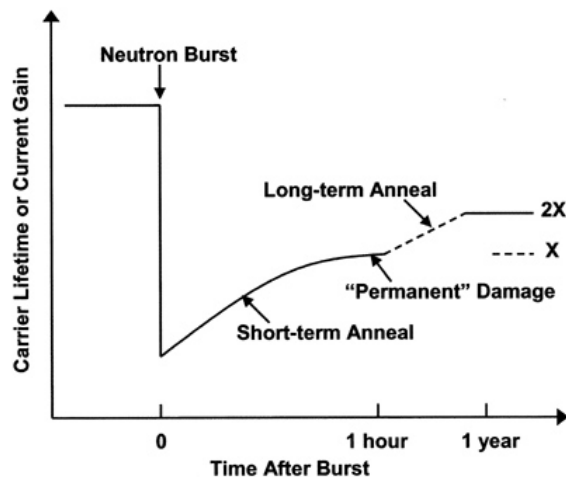
<sup>3</sup> To knock out an atom in Si requires 25 eV.

Defect reordering:

Once defects are formed by incident radiation, they will reorder to form more stable configurations. For example, the vacancy in silicon is an unstable defect and it is quite mobile at room temperature. After vacancies are introduced, they move through the lattice and form stable defects such as divacancies (two adjacent vacancies) and vacancy–impurity complexes. Defect reordering is usually called *annealing* and typically implies that the amount of damage and its effectiveness are reduced (Figure. 1.5). Defect reordering is temperature dependent (thermal annealing) and dependent on the present excess carrier concentration (injection annealing). Furthermore, the reordering of defects with time or increased temperature to more stable configurations can also result in more effective defects, where in this case the process is often referred in the literature as reverse annealing, in contrast to the more typical process of forward beneficial annealing.



**Figure 1.4** A defect cascade created by a 50 keV primary knock-on silicon ion in silicon. The primary ion is in red; displaced ions in green. Clusters and super-clusters of displaced ions are evident (SRIM 2003).



**Figure 1.5** Conceptual illustration of a short term and long term annealing at room temperature of displacement damage in bulk silicon and silicon devices [7]

DDD effects:

The discussion on defect reordering clarifies that the effectiveness of radiation-induced displacement damage depends on the conditions of the irradiation and on the time passed after irradiation. More generally, damage effectiveness depends on many factors, including particle type, particle energy, irradiation temperature, measurement temperature, time after irradiation, thermal history after irradiation, injection level, material type (n- type or p-type) and impurity type and concentration. The primary effect of displacement damage that leads to the degradation of material and of device properties is the introduction of new energy levels in the band gap, associated with defects (a new energy level arise from a disturbance of lattice periodicity). These defect states, or centers, have a major impact on the electrical and optical behavior of semiconductor materials.

Radiation-induced levels in the band-gap can give rise to several processes. Let us focus, for instance, on the *thermal generation* of electron-hole pairs through a level near midgap. This process can be viewed as the thermal excitation of a bound valence-band electron to the defect center and the subsequent excitation of that electron to the conduction band, thereby generating a free electron-hole pair. Only those center near the midgap make a significant contribution to carrier generation<sup>4</sup>.

<sup>4</sup> An exponential decrease in generation rate occurs as the energy-level position is moved from midgap.



Thus, thermal generation of electron-hole pairs (which is the mechanism for leakage current increases in silicon devices) through radiation-induced defects centers near midgap is important in device depletion regions.

Another type of effect is the *recombination of electron-hole pairs*, a process in which a free carrier of one sign is first captured at the defect center, followed by the capture of a carrier of the opposite sign. Recombination removes electron-holes pairs as opposed to the generation process. The mean time a minority carrier spends in its band before recombining is referred to as the recombination lifetime. Radiation-induced recombination centers cause the lifetime to decrease: this is the dominant mechanism for gain degradation due to displacement damage in bipolar transistors.

A third effect is the temporary *trapping of carriers* at a typically shallow level. In this process a carrier is captured at a defect center and is later emitted to its band, with no recombination event taking place. In general, trapping of both majority and minority carriers can occur (at separate levels). Radiation-induced traps are responsible for increasing the transfer inefficiency in charge-coupled devices.

A complete review of the literature on the effects of radiation-induced displacement damage in semiconductors materials and devices can be found in [7].

### 1.3.3 Total ionization effects

When an MOS transistor is exposed to high-energy ionizing irradiation, electron-hole pairs are created uniformly along the track of the incident particle throughout the oxide<sup>5</sup>. Electron-hole pair generation in the oxide leads to almost all TID effects: in fact, the generated carriers induce the buildup of charge, which can lead to the device degradation. The effect of the ionization on MOS devices depends upon the way that this charge is transported and trapped at the Si-SiO<sub>2</sub> interface. The net effect of ionizing radiation on MOS device oxides depends upon the oxide thickness, the field applied to the oxide during and after exposure, as well as trapping and recombination within the oxide. The manufacturing processing techniques strongly affect the latter factor.

After pair creation, in general, some of electrons will recombine with holes (depending on the material, the kind of radiation and the applied field, which acts

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<sup>5</sup> In oxide (SiO<sub>2</sub>), the electron-hole pair creation energy is ~ 17 eV.

separating the pairs). Following the initial creation process, the radiation-generated electrons and holes are transported under the applied electric field. Most of the electrons will drift in picoseconds toward the gate, where they are collected, while holes, far less mobile in Si than electrons<sup>6</sup>, linger where they have been generated. After this, the holes undergo a “hopping” transport over the Si/SiO<sub>2</sub> interface, through localized states in oxide. As the holes approach the interface, some fraction (strongly depending on the process) of the holes will be trapped, forming a positive oxide trap charge. Most of the holes are trapped within 7 nm of Si/SiO<sub>2</sub> interface and generally anneal with time.

In addition to hole trapping and annealing at the Si/SiO<sub>2</sub> interface, there is build up of radiation-induced *interface traps*. Hydrogen ions (protons) are likely to be released as holes “hop” through the oxide or as they are trapped near the Si/SiO<sub>2</sub> interface. The protons can drift to the Si/SiO<sub>2</sub> interface where they may react to form interface traps. In addition to oxide-trapped charge and interface-trap charge buildup in gate oxides, charge buildup will also occur in other oxides including field oxides and silicon-on-insulator (SOI) buried oxides.

Semi-permanent TID effects in MOS devices and circuits caused by the buildup of space charge in the SiO<sub>2</sub> layer fall into several categories, such as voltage offsets, or shifts, induced parasitic leakage currents and mobility degradation.

In general, the effect of radiation-generated charge  $\Delta\rho$  on the *threshold voltage shift*  $\Delta V_{th}$  of a transistor is given by:

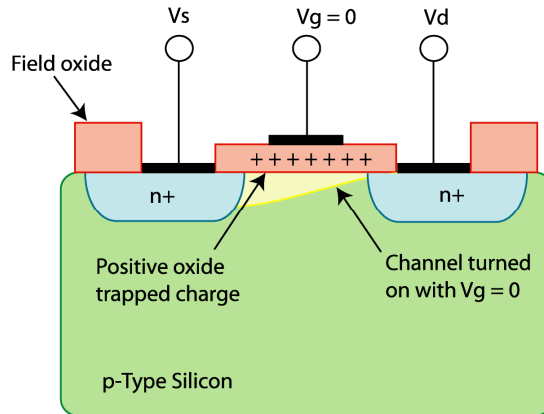
$$(2.5) \quad \Delta V_{th} = (-1/C_{ox}) \int_0^{t_{ox}} \Delta\rho(x)(x/t_{ox}) dx,$$

where  $t_{ox}$  is the oxide thickness,  $C_{ox}$  is the oxide capacitance and  $x$  is measured from the gate-SiO<sub>2</sub> interface. From equation (1.6) it can be seen that positive charge (trapped holes) will cause a negative shift in the threshold voltage of a device, while negative charge will cause a positive shift in the threshold voltage. In general, the initial response of an MOS transistor to radiation is a negative shift in the threshold voltage, due to buildup of trapped holes. For a sufficiently large amount of trapped positive charge, the n-channel device may be turned on even for a zero applied gate

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<sup>6</sup> In Silicon:  $\mu_{\text{electrons}} \leq 0.14 \text{ m}^2/\text{V}\cdot\text{s}$ ,  $\mu_{\text{holes}} \leq 0.05 \text{ m}^2/\text{V}\cdot\text{s}$ .

bias. In this case the device is said to have gone into “depletion mode”. When strongly into depletion, the n-channel device ceases to function because it cannot be switched from the ON to the OFF state: it is always ON (Figure. 1.6)!



**Figure 1.6** Schematic cross section of an MOS transistor illustrating charge buildup in the gate oxide

Charge gathered in the thick field oxide will also turn on a parasitic leakage path at the edges of the gate metal, where current can flow from source to drain outside the channel region. The irradiation-induced shift of the gate-oxide curve is small due to the thin thickness of gate oxide layer. On the contrary, while the contribution of the field oxide leakage current is negligible before irradiation, after irradiation it becomes the major effect. This is due to the larger thickness of the field oxide respect to the gate one, this resulting in a larger voltage shift per unit dose. The combination of two effects makes the *leakage current* raise several orders of magnitude after irradiation, which is often enough to cause functional failure of the devices.

Figure 1.7 shows the voltage threshold shift effect for a typical commercial process. Hardened devices will exhibit much lower threshold shifts primarily because of recombination in the oxide. Present commercial CMOS technologies will usually fail at levels between 10 and 50 krad(Si). To set the scale, the total dose that can be accumulated during 10 years in space may range from a minimum of a few krad(Si) and may reach up to 100 krad(Si).<sup>7</sup> The total dose that will accumulated in 10 years

<sup>7</sup> In  $\text{SiO}_2$  the number density of electron-hole pairs per unit dose is  $n = 7.6 \times 10^{12}$  e-h/cm<sup>3</sup>-rad; in Si  $n = 3.7 \times 10^{13}$  e-h/cm<sup>3</sup>-rad.

by the frontend electronics of the silicon CMS tracker at LHC will range from 100krad(Si) to 50 Mrad(Si).

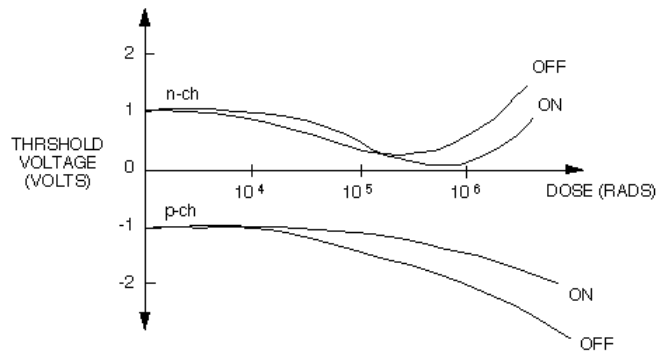


Figure 1.7 Voltage shift due to irradiation.

## 2 Single Event Effects

Single Event Effects (SEE), as the name suggests, are due to the interaction of a single particle with a semiconductor device. In this chapter I will discuss SEE and describe the various types of effects that can be induced by a single particle strike.

### 2.1 Introduction

#### 2.1.1 Brief history of SEEs

The first confirmed report of cosmic-ray-induced Single Event Upsets (SEU, discussed later) in space was presented at the NSREC<sup>8</sup> in 1975 by Binder *et al.*[8]. In this paper, four upsets in 17 years of satellite operation were observed in bipolar J–K flip–flops operating in a communications satellite. The authors used scanning electron microscope (SEM) exposures to determine the sensitive transistors and, using a diffusion model, calculated a predicted upset rate within a factor of two of the observed rate. Due to the small number of observed errors, the importance of SEU was not fully recognized until 1978–1979, when significant numbers of SEU-related papers were presented at the NSREC.

The occurrence of soft errors in terrestrial microelectronics manifested itself shortly after the first observations of SEU in space [9]. This watershed paper from authors at Intel found a significant error rate in DRAMs as integration density increased to 16 to 64K. The primary cause of soft errors at ground level was quickly diagnosed as due to alpha particle contaminants in the package materials. Radioactive contaminants in the water used by the factory were contaminating the ceramic packages of devices.

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<sup>8</sup> NSREC: Nuclear and Space Radiation Effect Conference.

In the late 1970s, evidence continued to mount that cosmic-ray-induced upsets were indeed responsible for errors observed in satellite memory subsystems, and the first models for predicting system error rates were formulated [10]. By this time satellite memory systems had increased in size and on-orbit error rates of one per day could not be ignored.

Even though the first papers attributed memory upsets to direct ionization by heavy ions, by 1979 two groups reported at the NSREC on errors caused by proton and neutron indirect ionization effects [11] [12]. This was a very important discovery, because of the much higher abundance of protons relative to heavy ions in the natural space environment: not only would SEE be caused by galactic cosmic rays, but also by protons trapped in the Earth's radiation belts and by solar event protons. The paper by Guenzer *et al.*[12] was the first to use the term "single-event upset", and this term was immediately adopted by the community to describe upsets caused by both direct and indirect ionization. The year 1979 also brought the first report of single-event latchup (SEL, described later), an important discovery given the potentially destructive nature of the failure mode.

In the early 1980s, research on SEU continued to increase and methods for hardening ICs to SEU were widely developed and used throughout this decade [13] [14]. There were also few studies on another emerging and potentially troubling single-event issue: errors due to single events in combinational or imbedded logic.

The 1990s saw two major developments that continued to increase the importance of SEEs. One was the dramatic decrease in the number of manufacturers offering radiation-hardened digital ICs. This (among other factors, such as the increased functionality and performances they could provide) led to the increased usage of commercial electronics in spacecraft systems. However, their relative sensitivity to SEE presented significant challenges to maintaining system reliability. The second development was the continued advance in fabrication technologies toward smaller IC feature sizes and the higher speeds and more complex circuitry that scaling enables. These advances typically increase sensitivity to SEE, even to the point of errors occurring in a benign desktop terrestrial environment, and may also lead to new failure mechanisms. These two developments led to an interesting convergence of mission from two historically disparate communities: space and military vendors

driven toward commercial (non radiation hardened) circuits and commercial vendors driven toward a very real concern about SEE in the everyday consumer environment.

As we enter the 21<sup>st</sup> century, concern about sensitivity to SEU is expected to continue, both in memories and core logic. Upsets in terrestrial electronics are a serious reliability concern for commercial manufacturers. At the same time, feasibility of traditional SEU-hardening techniques is becoming questionable, especially because of fewer dedicated rad-hard foundries implementing them. Circuit design that are inherently radiation resistant (Hardening By Design, HBD) are receiving considerable attention [15] [16].

### **2.1.2 Classification of SEE**

In Chapter 1 we have seen how an ion strike releases charge along its path through a semiconductor and how this charge can be collected by p/n junctions, but what really matters is determining whether the event actually causes an error in circuit operation. In the following sections we will study how charge collection interacts with the circuit type and design to create a single-event effect. Here we report the major types of single event phenomena, which can be classified into several categories:

- Single event upset (soft error that can be reset)
- Single event latchup (soft or hard errors)
- Single event burnout (hard failures)
- Single event gate rupture (hard failures)

## **2.2 Single Event Upset**

### **2.2.1 Introduction**

Single event upset, or SEU, is the most common type of single event effect. SEU is caused by the deposition of charge in a device by a single particle, that is sufficient to change the logic state of a single bit (from one binary state to another). Whether or

not the charge deposited through direct ionization is sufficient to cause an upset of course depends on the type of device and circuit that has been struck, as well as the strike location and particle trajectory. Direct ionization is the primary charge deposition mechanism for upsets caused by heavy ions (ions with atomic number  $Z \geq 2$ , i.e. He and above). Lighter particles, such as protons, do not usually produce enough charge by direct ionization to cause upset in memory circuits, but researches have suggested that single event effects due to direct ionization by protons may occur in new and more susceptible ICs [17] [18].

Single bit upsets are sometimes called *soft errors* because a reset or a rewriting of the device results in normal device behavior thereafter. An SEU may occur in analog, digital, or optical components; it may also have effects in surrounding interface circuitry to which they are connected, but this strongly depends on the nature of the interconnections. Some memory devices are also susceptible to Multiple Bit Upset (MBU), in which more than one bit is upset. This can be caused by a single ion traveling essentially parallel to the die surface, depositing energy in the sensitive volume of a consecutive line of memory cells, or striking the die close to normal, depositing enough energy in two or three adjacent cells to upset them. A severe SEU is the Single-Event Functional Interrupt (SEFI) in which an SEU in the control circuitry of the device places it into a test mode, halt, or undefined state. The SEFI halts normal operations, and requires a power reset to recover.

In the next paragraphs the focus will primarily be on memory circuits, as this will be the main field of application of the equipment described in this thesis.

### **2.2.2 Single Event Upset in DRAM**

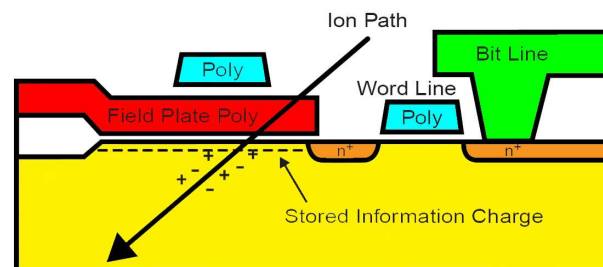
SEUs in terrestrial electronics were first observed in DRAMs [9] [19]. This kind of memories have historically been quite susceptible to soft errors because they rely on passive storage of charge to represent information: there is no inherent refreshing of this charge packet (e.g., charge resupply through a load device) and no active regenerative feedback. Their charge state is readily modified by funnel-assisted drift or diffusion following an energetic particle strike; they hence allow any disturbance, no matter how small, of the stored information to persist, until corrected by external circuitry.



What is so often referred to as a bit flip, the transition from one stable binary state to the other, is not required in DRAMs for an SEU to occur. A degradation of the stored signal to a level outside the noise margin of the supporting circuitry is sufficient to lead to erroneous interpretation and a resultant error. DRAMs have therefore received less use in space systems as engineers have preferred SRAM technologies. As the need for very large amounts of on-board memory is increasing, the use of DRAM technologies in space systems is becoming more common.

DRAMs are prone to SEU due to three primary mechanisms: storage cell errors, bit-line errors and a combination of the two.

Figure 2.1 illustrates the mechanism for *storage cell errors* in a field plate capacitor DRAM [20]. In this kind of DRAM a stored “0” is represented by electrons occupying a potential well under the field plate, while a stored “1” corresponds to electrons being depleted under the plate. Following a particle strike, electrons can be collected at the reverse-biased field plate. In the case of a stored “0”, this just reinforces the original state, but a stored “1” can look like a stored “0” after electron collection.



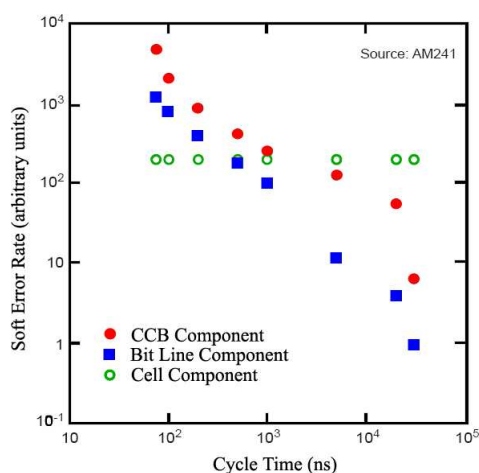
**Figure 2.1** Illustration of storage cell SEU in a field-plate DRAM. Collections of electron at the reverse-biased field plate reinforces a stored “0”, but can lead to an upset of a stored “1”.

Upsets can also occur in DRAMs due to bit-line strikes. When the bit lines are in a floating voltage state (e.g. during a read cycle), DRAMs are sensitive to the collection of charge into diffusion regions that are electrically connected to the bit access lines.<sup>9</sup> The *bit-line error* is the reduction of the sensing signal due to a charge imbalance introduced of the precharged bit lines. Because they can only occur during

<sup>9</sup> This collection could arise from any of the access-transistor drains along the floating bit-line or from a direct strike to the sense amplifier circuitry itself.

a read cycle, bit-line errors have a direct dependency on the read access frequency, with an increasing error rate as the access frequency increases.

A new failure mode for DRAMs was demonstrated when it was found that charge collection at both the storage cell and bit line, that was insufficient to individually cause an upset, could cause an error in combination [21]. This new failure mode, dubbed the *Combined Cell-Bit line (CCB)* error, was shown to dominate the storage cell and bit-line error rates for very short cycle times. The three components of soft errors in a 512K DRAM are shown in Figure. 2.2 as a function of the cycle time. Note the independence of storage-cell errors on cycle time, and the domination of CCB errors for short cycle times.



**Figure 2.2** Components of soft-error rate in DRAM [21]. The storage cell component is not dependent on the cycle time, while soft errors involving the bit lines increase dramatically as the cycle time decreases.

### 2.2.3 Single Event Upset in SRAM

The upset process in SRAMs is quite different from DRAMs, due to the active feedback in the cross-coupled inverter pair that forms a typical SRAM memory cell, as illustrated in Figure. 2.3. When an energetic particle hits a sensitive location in a SRAM (typically the reverse-biased drain junction of a transistor biased in the “off” state, T1 in figure), charge collected by the junction induces a transient current in the struck transistor. As this current flows through the struck transistor, the restoring transistor (“on” p-channel transistor, T2 in figure) sources current in an attempt to

balance the particle-induced current. The current flowing through the restoring transistor, due to the finite transistor channel conductance, induces a voltage drop at its drain (point A in Figure. 2.3). This voltage transient (in response to the single-event current transient) is actually the mechanism that can cause upset in SRAM cells. In fact, T2 drain is also connected to the gates of transistors T3 and T4. If the induced current is sufficient to lower the voltage of restoring transistor drain below a threshold voltage, the logical states of T3 and T4 will be inverted. This will consequently force the voltage of point B to go to  $V_D$  (it was at zero before the hit), so switching T1 and T2 and changing the state of the cell as a result. Competition between the feedback process and the recovery process governs the SEU response of SRAM cells. In fact, if the recovery current sourced by the restoring transistor is faster than the feedback one, the circuit will not flip, although the induced transient current is obviously still present.

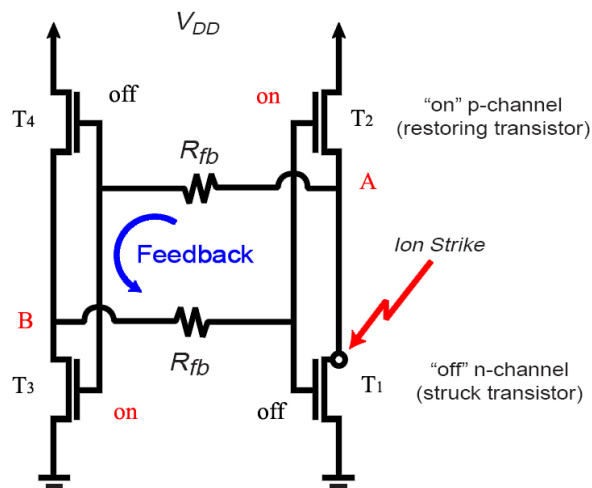
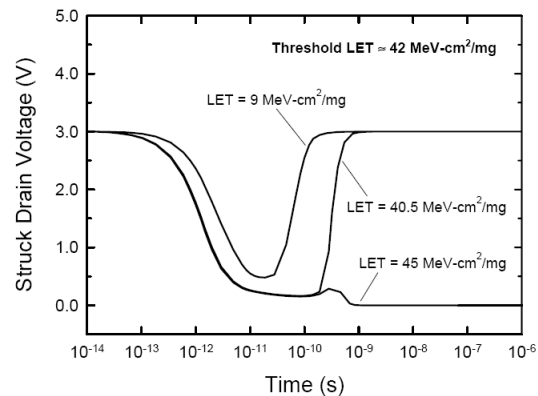


Figure 2.3 Schematic layout of a CMOS SRAM cell.

Interestingly, even incident particles with LET far below the upset threshold are often sufficiently ionizing to induce a momentary voltage “flip” at the struck node of an SRAM (Figure. 2.4). Whether an observable SEU occurs depends on what happens faster: the feedback of the voltage transient through the opposite inverter, or the recovery of the struck node voltage as the single-event current dies out. It must be noted that drift (including funneling effects) is responsible for the rapid initial flip of the cell, while long-term charge collection by diffusion prolongs the recovery process; both mechanisms are critical to the upset process.



**Figure 2.4** SRAM struck drain voltage transient for ion strikes with LET well below, just below and just above the SEU threshold.

The recovery time of an SRAM cell to a particle strike depends on many factors, such as the particle LET, the strike location, etc. From a technology standpoint, the recovery time depends on the restoring transistor current drive and minority carrier lifetimes in the substrate [22] [23]. A higher restoring current leads to a fast recovery time, as do decreased minority carrier lifetimes<sup>10</sup>. The cell feedback time is simply the time required for the disturbed node voltage to feed back through the cross-coupled inverters and latch the struck device in its disturbed state. This time is related to the cell write time and in its simplest form can be thought of as the RC delay in the inverter pair. This RC time constant is thus a critical parameter for determining SEU sensitivity in SRAMs: the smaller the RC delay, the faster the cell can respond to voltage transients (including write pulses) and the more susceptible the SRAM is to SEUs. Obviously this has implications for the sensitivity of future, higher speed technologies.

## 2.2.4 Single Event Upset in SOI devices

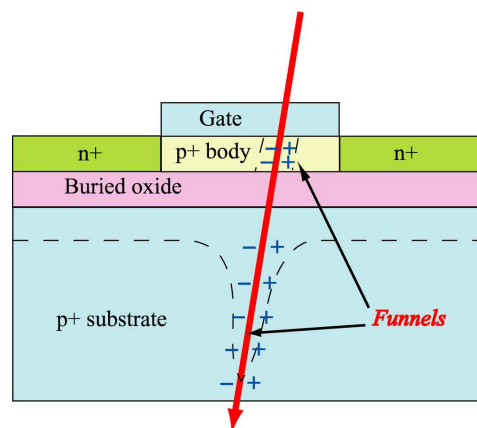
Due to their intrinsic structure, Silicon On Insulator (SOI) devices were regarded to be much less sensitive to upsets than conventional bulk silicon circuits. In a bulk Si transistor the charge generated by an ion strike is fully collected from the substrate

<sup>10</sup> This is because a higher restoring current is more quickly able to re-establish the struck node voltage, while decreased substrate minority carrier lifetimes reduce the diffusion current at the struck node.

region, regardless whether the gate or the drain has been hit. In a SOI transistor, instead, (see Figure. 2.5) the volume area sensible to charge collection is made smaller by the buried oxide that prevents charge deposited in the substrate to be efficiently collected. However, it has been shown how it is possible to have charge collection from below the buried oxide in SOI technologies that use a very thin buried (on the order of 200 nm) oxide layer [24].

For these technologies it has been measured that the saturated cross section ( $\sim 8 \mu\text{m}^2/\text{bit}$ ) was closer to the sum of the active gate and drain areas ( $6.1 \mu\text{m}^2/\text{bit}$ ) rather than to the gate area alone ( $0.64 \mu\text{m}^2/\text{bit}$ ). This indicates that, contrary to the earlier beliefs, charge collection could also occur from the substrate below the buried oxide, at least in some SOI technologies.

From past studies, it is known that charge collection occurs only when the substrate is biased in depletion or inversion mode, and the mechanism for charge collection at top electrode was assumed to be due to a capacitive discharge or to a displacement current. Recent studies and simulations [25] with dedicated microscopy experiments performed at microbeam facilities, led to a deeper understanding of this kind of phenomenon.



**Figure 2.5** Charge collection behavior in SOI transistor

### 2.2.5 Single Event Upset in logic circuits

Although we have concentrated on SEU in memory circuits, they can also occur in other digital circuits, prime examples being microprocessors and digital signal processors. Errors in logic circuits are very sensitive to critical timing windows and logic paths, and may never propagate to the output pins. Therefore, in core logic, the

concepts of “faults” and “errors” are distinct from memory circuits and require precise definition.

In a logic circuit, charge collection due to a single-event strike on a particular node will generate a low-to-high or high-to-low voltage transition or a transient noise pulse. If this pulse is larger than the input noise margin of a subsequent gate, it will compete with the legitimate digital pulses propagating through the circuit. The ability of the noise pulse to propagate depends not only on its magnitude, but also on several more factors. First, the existence of active combinational paths from the struck nodes to latches<sup>11</sup>; second, the arrival time of the erroneous signal at the latches; third, the erroneous pulse time profile at the latch input<sup>12</sup>. If all three of the above conditions are properly met, then the SE-generated noise pulse will be captured by the latch as erroneous information. We define this as the generation of a *soft fault* (SF).

SFs may also be generated by direct single-event strikes to the latch nodes, where the latch information is corrupted via a bit flip. In this case the effect is analogous to SEUs in memory circuits and can be modeled in a similar way.

Once a SF has been identified, or a SF probability has been calculated, one knows the vulnerability of a circuit to single events and/or critical paths which may contribute a weak link for single-event tolerance. However, actual upset rates, which refer to the observable operation of a particular circuit located in a particular hostile radiation environment, cannot be immediately deduced from knowledge of SFs. Internal SFs may not be observable at the interface pins of a circuit (or the I/O ports of a subcircuit). For example, the particular latch effected by the soft fault may be part of a “don’t care” state of the finite state machine; the change of state has no effect on subsequent operation of the circuit. Or, the erroneous latch data may be part of a data register that is scrubbed in a subsequent clock cycle. Thus, no observable error actually occurs. However, if the soft fault eventually propagates to one or more of the I/O ports of the circuit, then an externally observed error exists; we define this and only this event as an *error event*. It is clear that one soft fault may cause

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<sup>11</sup> The active combinational paths depend on the dynamic state of the logic as determined by the particular code vectors executed at that time (the present “state” of the logic).

<sup>12</sup> The pulse must arrive within the setup and hold (S/H) time of the latch element to be stored by the latch element. The clocking characteristics of the latch and the previous state of the latch contribute to this mechanism.

erroneous information at many I/O ports and that this erroneous information may appear during many clock cycles.

### **2.2.6 Single Event Upset in analog circuits**

SEU can occur in almost any integrated circuit. For example, SEU is not constrained to digital circuits, but also occur in analog circuit as well.

Upsets in photodiodes used in optocoupler applications have been observed and correlated to direct ionization by protons. Single-Event current Transients (SET) resulting from proton direct ionization are capable of causing upsets in these photodiodes because they are by design very large and operate at very high data rates. A recent analysis suggests that a combination of direct ionization and recoils are responsible for the anomalous angular dependence of proton upsets in optocouplers. Charge-coupled devices (CCDs) can also be sensitive to direct ionization by protons because of their large collection depths [26].

Errors are observed in many analog circuit types, including operational amplifiers, comparators, analog-to-digital converters (ADCs). Upsets in ADCs are interesting because analog errors are observed as corruptions in digital output codes.

## **2.3 Other kinds of SEE**

### **2.3.1 Single Event Latchup (SEL)**

Circuits are made by combining adjacent p-type and n-type materials into transistors. Paths other than those chosen to form the desired transistor can sometimes result in so-called parasitic transistors, which, under normal conditions, cannot be activated. A latchup is the inadvertent creation of a low-impedance path between the power supply rails of an electronic component, triggering the above mentioned parasitic structure, which then acts as a short circuit, disrupting proper functioning of the part and possibly even leading to its destruction due to overcurrent. A power cycle is required to correct this situation.

The parasitic structure is usually an equivalent of a thyristor (or Silicon Controlled Rectifier, SRC), a PNPN structure which acts as a PNP and an NPN transistor

stacked next to each other (Figure. 2.6). During a latchup, when one of the transistors is conducting, the other one begins conducting too.

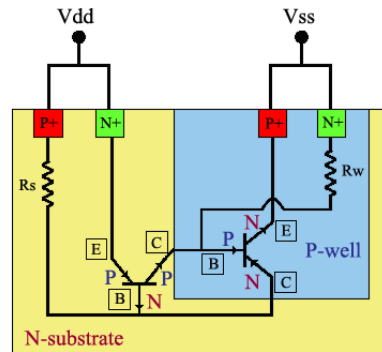


Figure 2.6 Lateral section of a p/n/p/n structure with two parasitic BJTs

They both keep each other in saturation for as long as the structure is forward-biased and some current flows through it (it usually means until a power-down). The SCR parasitic structure is formed as a part of the totem-pole PMOS and NMOS transistor pair on the output drivers of the gates.

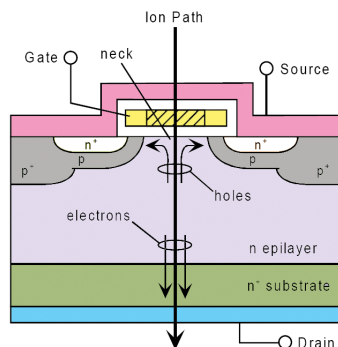
### 2.3.2 Single Event Gate Rupture (SEGR)

Dielectric breakdown can occur when the electric field across an insulating material exceeds some threshold value. When initiated by an energetic particle strike to the gate region of an MOS device, this phenomenon is referred to as a Single-Event Gate Rupture (SEGR).

Single-event gate rupture has been studied most extensively for power devices such as double-diffused power MOSFETs (DMOS), so we will use this device or describing the SEGR mechanism.

As shown in Figure. 2.7, current flow in the DMOS structure is vertical rather than lateral as in a standard MOSFET. Application of a positive bias to the gate in this n-channel DMOSFET inverts the p-body region to form a channel between the n-source at the top of the structure and the drain (substrate) contact at the bottom of the structure. To handle large currents, the full structure usually contains hundreds or thousands of these cells connected in parallel.





**Figure 2.7 Structure of a vertical power MOSFET and current flow paths following a heavy ion strike.**

The thick lightly-doped epitaxial region allows the power MOSFET to sustain high voltages without breakdown. When an ion strikes the neck region through the gate oxide, SEGR can occur as charge is transported near the Si/SiO<sub>2</sub> interface. As charge from the ion strike accumulates underneath the gate region (and depending on the gate bias), the electric field in the gate insulator can temporarily increase to above the critical field for breakdown, causing a localized dielectric failure (i.e., an SEGR). The SEGR response in vertical power MOSFETs has two components [27]. The “capacitor response” describes the interaction of the ion directly with the gate dielectric, inducing an oxide breakdown at a lower field than would occur in the absence of the ion strike. If a drain bias is applied when the ion strike occurs, part of the drain voltage may be transferred through the epitaxial layer to the gate interface [28]. This part of the response is referred to as the “substrate response.” Increasing the gate voltage increases susceptibility to SEGR through the capacitor response by increasing the pre-existing electric field in the oxide. Increasing the drain voltage also increases the susceptibility to SEGR because part of this voltage can be coupled to the interface through the substrate response.

SEGR effects have been studied for some time in power devices, but a topic that has recently received a considerable amount of interest is SEGR in logic and memory ICs. As gate oxide thicknesses decrease, SEGR could become a problem in ICs because they will likely be operated at somewhat higher electric fields.

### 2.3.3 Single Event Burnout (SEB)

Single Event Burnout (SEB) due to heavy ions, neutrons and protons has been observed both in power MOSFET and in bipolar transistor. SEB is a destructive failure mechanism that comes about due to a parasitic bipolar transistor structure inherent to some devices. Looking at the power MOSFET structure in Figure.2.7, a parasitic bipolar transistor is formed by the n-source (emitter), p-body (base) and n-epitaxial (collector) regions. Following an ion strike, currents flowing in the p-body can forward bias the emitter-base junction of the parasitic BJT due to the finite conductivity of the p-body region. The parasitic BJT is now operating in the forward active regime, and if the drain-to-source voltage is higher than the breakdown voltage ( $BV_{CEO}$ ) of the parasitic BJT, avalanche multiplication of the BJT collector current can occur. If this positive feedback (regenerative) current is not limited, it can lead to junction heating and the eventual burnout of the device [29].

### 2.3.4 Single Event Snapback (SES)

Single Event Snapback is a stable, regenerative condition similar to latchup caused by a drain-to-source breakdown in normal n-MOS transistors. Like latchup, the resulting condition is a high current state that can lead the device to failure (Figure 2.8)

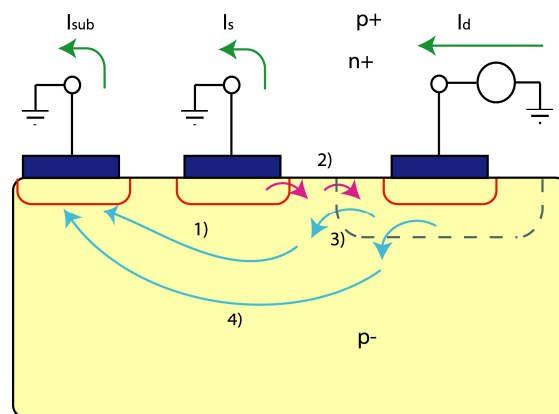


Figure 2.8 Snap back mechanism in n-MOS structure

Unlike latchup, a p-n-p-n four layer structure is not necessary to have a snap back. Snap back is initiated by avalanche breakdown of the drain junction by current injection into the n-MOS transistor body, or by excess body current after an high

dose rate radiation pulse or an heavy ion strike. After an ion hit, excess current near the drain junction results in avalanche multiplication and injection of holes that flow in the body region to the body contact (1) and cause the potential at the source-body junction to increase. If an avalanche condition is sustained long enough due to a sufficiently large current pulse, the source-substrate junction becomes forward biased turning on the parasitic npn bipolar transistor and injecting electrons into the substrate (2). As these feed into the drain, additional avalanche multiplication occurs (3), causing an increased substrate current and completing the regenerative feedback mechanism (4). Snap back cannot be triggered unless an external circuit provides sufficient current; for this reason, it is usual observed onto I/O stages of ICs equipped with large current drive pull up transistors. It is not observed in p-channel devices because the ionization rate for holes is much lower than for electrons, and regenerative feedback is consequently much lower.

## **2.4      *The SIRAD Single Events irradiation facility***

### **2.4.1      Introduction**

The SIRAD heavy ion irradiation facility, located at the 15 MV Tandem-XTU accelerator at the INFN National Laboratory of Legnaro (Italy) is dedicated to radiation damage studies in silicon detectors and devices. An important part of the experimental program is the study of ion induced SEE in microelectronic devices and systems. Devices under test are exposed to a broad beam (few cm<sup>2</sup>) and global characterizations are routinely performed. A wide selection of swift ion species, from Li to Au, is available to test most modern technology electronic devices for high energy physics and space applications. The IEEM discussed in this work was non-invasively installed to extend SEE capabilities of the SIRAD beam-line to include the ability to reconstruct the impact points of individual ions with high resolution. In this section we will give a detailed description of SIRAD facility.

## 2.4.2 The Tandem XTU accelerator

The Tandem-XTU accelerator is an electrostatic Van de Graaff type (Figure 2.9): two stripper stations are used in order to achieve high ion energies.



**Figure 2.9** The 15MV Tandem XTU at the INFN Legnaro National Laboratories.

Table 2.1 reports typical ion species and energies available at SIRAD. Normally, the extracted beam is continuous but pulsed beams are also possible. The maximum operating voltage is 15 MV and available ions range from  $^1\text{H}$  (30 MeV) to  $^{197}\text{Au}$  (1.4 MeV/a.m.u.). The energy, expressed in MeV, of the ions at the exit of the Tandem with two strippers is:

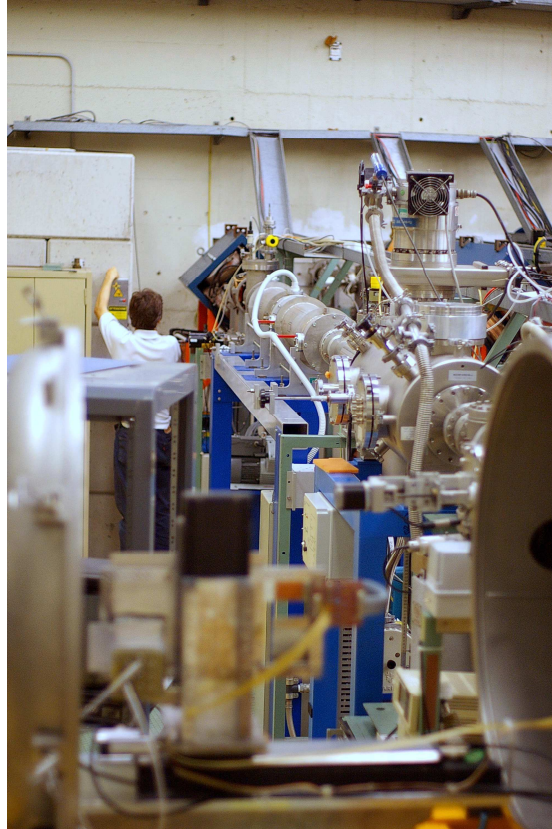
$$(2.1) \quad E = E_{inj} + V_0 \cdot (1 + q_1 \cdot f + q_2 \cdot (1 - f))$$

where  $E_{inj} = 0.18$  MeV is the energy of the negative charged ion injected from the source into the Tandem,  $V_0 = 11 \div 15$  MV is the Tandem operating voltage,  $f = 0.25$ , and  $q_1$  is the positive charge of the ion expressed in units of the electron charge after the first stripper foil located at the terminal. The charge  $q_2 > q_1$  is the ion charge after the second stripper foil located downstream of the first one. The second stripper foil can be excluded, in which case the energy of the ions is

The beam at the Tandem output is not monochromatic due to the realization of different  $q_1$  and  $q_2$  ion charge states. Magnetic momentum analysis selects ions of a certain energy and the switching magnet then sends the monochromatic beam into the various experimental beam lines. The Tandem-XTU accelerator services 3

experimental halls and 10 beam lines: the SIRAD beam line is the  $+70^\circ$  in the heavily shielded hall 1 ( Figure 2.10)

$$(2.2) \quad E = E_{inj} + V_0 \cdot (1 + q_1)$$



**Figure 2.10** Picture of the SIRAD irradiation facility at INFN Laboratori Nazionali di Legnaro. The large global irradiation chamber in foreground is open. The IEEM chamber is downstream and not visible.

### 2.4.3 The SIRAD irradiation facility

Bulk damage and SEE studies are routinely addressed at the SIRAD irradiation facility of the INFN National Laboratory of Legnaro (Padova, Italy) by Universities and Industrial groups, involved in the study of the radiation hardness of semiconductor devices and electronic systems for high energy physics and space applications [60].

The characteristics of the typical ion beams available at the SIRAD irradiation facility are reported in Table 4.1: the energy values refer to the most probable  $q_1$  and  $q_2$  charge state, obtained with two stripper stations and with the Tandem operating at

14 MV; the surface ion LET<sub>0</sub> and range reported are for silicon (calculated by SRIM).

Ion	Energy (MeV)	q <sub>1</sub>	q <sub>2</sub>	LET <sub>0</sub> (MeV × cm <sup>2</sup> /μg)	Range (μm)
<sup>1</sup> H	28	1	1	0.02	4390
<sup>7</sup> Li	56	3	3	0.37	378
<sup>11</sup> B	80	4	5	1.01	195
<sup>12</sup> C	94	5	6	1.49	171
<sup>16</sup> O	108	6	7	2.84	109
<sup>19</sup> F	122	7	8	3.87	99.3
<sup>28</sup> Si	157	8	11	8.59	61.5
<sup>32</sup> S	171	9	12	10.1	54.4
<sup>35</sup> Cl	171	9	12	12.5	49.1
<sup>48</sup> Ti	196	10	14	19.8	39.3
<sup>51</sup> V	196	10	14	21.4	37.1
<sup>58</sup> Ni	220	11	16	28.4	33.7
<sup>63</sup> Cu	220	11	16	30.5	33.0
<sup>74</sup> Ge	231	11	17	35.1	31.8
<sup>79</sup> Br	241	11	18	38.6	31.3
<sup>107</sup> Ag	266	12	20	54.7	27.6
<sup>127</sup> I	276	12	21	61.8	27.9
<sup>197</sup> Au <sup>2</sup>	275	13	26	81.7	23.4

**Table 2.1** Characteristics of the typical ion beams available at the SIRAD irradiation facility with the Tandem operating at 14 MV. The values of the LET<sub>0</sub> and the range are for silicon.

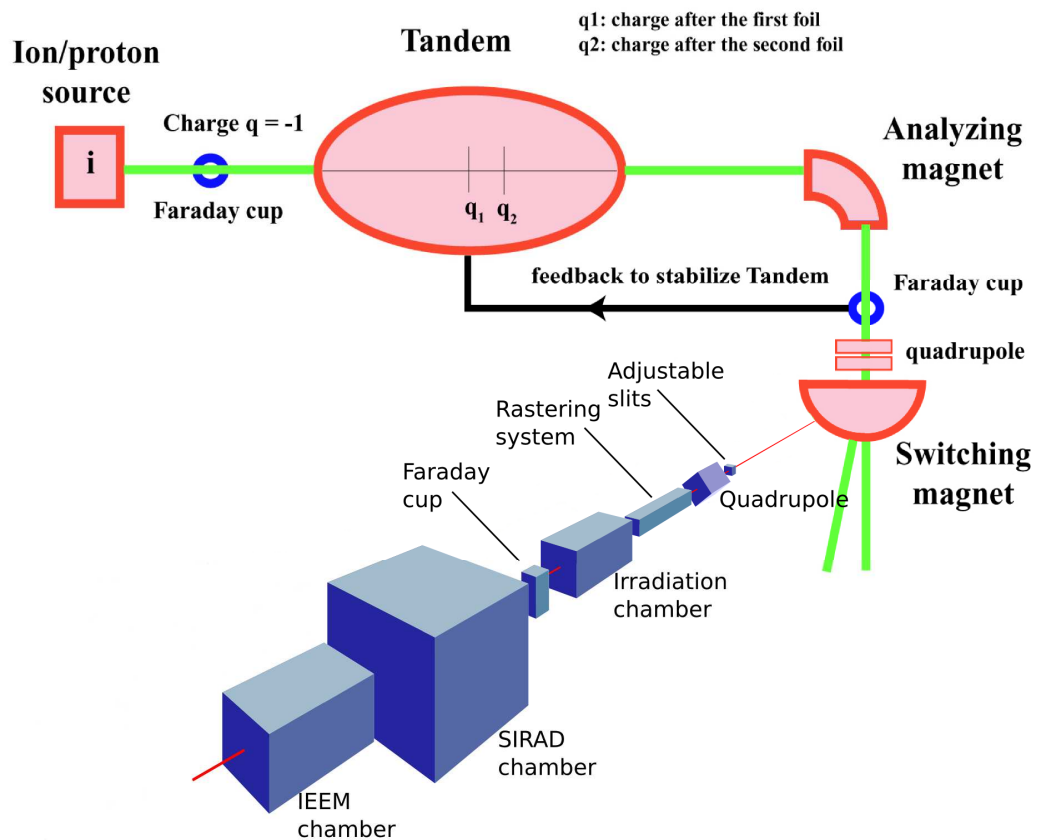
At present when using <sup>197</sup>Au beams in SIRAD the operating voltage is typically lowered to 11.6 MV due to a temporary limitation in the maximum current in the power supply of the switching magnet that deviates the beam into the line at 70°. <sup>13</sup> The ion species reported in Table 4.1 have been selected in order to minimize the time required for the ion source change during SEE tests. When possible two multi-sources (the first including O, Si, Ni and Ag; the second including F, Cl, Br, and I) are used to decrease the time for beam setting.

The essential elements of the SIRAD line, shown in Figure 2.11, are:

- a system of adjustable horizontal and vertical slits;

<sup>13</sup> We plan to remove all limitations of this type by stripping further electrons from the ions just before the analyzing magnet.

- a quadrupole doublet for focusing the beam down to millimetric spots;
- an electric rastering system for irradiating extended targets;
- an irradiation chamber with a vertical sample-holder, available both for diagnostic and irradiation purpose;
- a chamber with an extractable Faraday cup (FC70);
- an irradiation chamber including a battery of small Faraday cups and a battery of silicon PIN diodes with pulse counting electronics.



**Figure 2.11 Schematic drawing of the SIRAD irradiation facility. The IEEM chamber is downstream of the large global irradiation chamber (SIRAD chamber). A smaller chamber upstream is used for beam diagnostics.**

The typical spot size diameter of a focused beam is 3-4 mm and beam diagnostics is performed by an extractable Faraday Cup positioned in a diagnostic chamber located ~ 1 m upstream of the target plane. Visual inspection of the beam profile may be performed on a quartz window positioned at the end of the irradiation chamber.

An image intensifier is sometimes used to see the beam spot on the quartz for tenuous beam current.

In order to irradiate a large target with a focused proton or ion beam, a rastering system is used. The system, produced by IBA (Louvain-la-Neuve, Belgium), is made of vertical and horizontal deflection plates 1 m long, with 5 cm gaps, and with linearly ramped voltages ( $V_{\max} = \pm 15$  kV) at slightly different frequencies ( $\nu_x = 625$  Hz,  $\nu_y = 612$  Hz). The rastering system permits a uniform irradiation (better than 5%) over a fiducial area of  $5 \times 5$  cm<sup>2</sup> on the target plane. On-line monitoring of the beam current and uniformity on the target is provided by a square battery of  $3 \times 3$  small Faraday cups, located behind the target plane (sample holder). This configuration is suitable for radiation tests at beam currents higher than 100 pA/cm<sup>2</sup> and is currently used for proton induced bulk damage studies in silicon.

The very low ion fluxes ( $10^2$ - $10^5$  ions/(cm<sup>2</sup>·s)) necessary for global SEE studies in electronic devices and systems are obtained by closing machine collimators to achieve low beam currents (< 1 nA) and by defocusing the beam on the target plane by adjusting the SIRAD quadrupole doublet (see Figure 2.11). The doublet is positioned before the rastering system, which is normally not used in SEE experiments (it is used instead for high current bulk damage studies or intense ion beam irradiation). The ion fluxes for SEE tests are well below the sensitivity of the Faraday cups and the beam spot cannot be seen with the quartz system. To setup the beam, measure the ion flux, uniformity and the quality of the beam (monochromaticity) we use an array of silicon PIN diodes as particles counters in the target plane. During irradiation the device under test is surrounded by 4 diodes and the beam characteristics are monitored.

The same beam-set up procedure is used when the IEEM is used. A single PIN diode inside the IEEM chamber is used to measure the ion flux and the beam quality.



## 3 SEE studies

### 3.1 SEEs modeling

#### 3.1.1 Introduction

Modeling Single Event Effect rates in a microelectronic device involves a combination of:

- assumptions about the physics of the device;
- detailed knowledge of the radiation environment;
- real experimental.

The device physics that underlies SEE involves charge generation along the path of a primary or secondary ionizing particle, charge transport and collection on circuit nodes and the final response of the circuit to the charge transient. Both the total collected charge and the rate of charge collection can be important to triggering a single event effect. Models that predict SEE rates typically use test data obtained at accelerator irradiation facilities to extract information about the device sensitivity. The typical information sought for are the cross section  $\sigma$  and the critical charge ( $Q_C$ ), as a function of LET or the energy of the incident particles. The experimentally measured cross section for a device can be expressed as the ratio between the number of SEE counted for a certain fluence of particles of a given LET or energy:

$$(3.1) \quad \sigma = \frac{\text{counts}}{\text{fluence}} [cm^2].$$

Once the cross section versus the particle LET or energy has been measured, there are established techniques for using the data to predict SEE rates in a given radiation

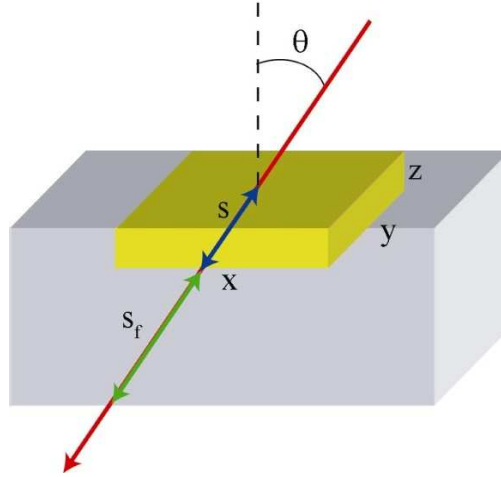
environment. The rate prediction methods do a fairly good job of predicting what is actually observed in a radiation hostile environment, such as onboard a spacecraft.

As a first approximation the occurrence of SEEs is driven by the quantity of deposited energy. This allows one to reduce all particle types and energy distributions present in the radiation environment to their LET and to calculate the deposited energy by integrating the LET along the trajectories throughout the sensitive volume. With this simplification, the problem is to define the size of the sensitive volume, calculate the rate of particle hits and the consequent energy depositions, and determine the fraction of total particle hits that cause SEEs. The SEE rate is the product of the sensitive area on the chip by the flux of particles in the environment that can cause the considered event. The problem is complicated by the angular dependence since the amount of energy deposited in the sensitive volume depends on chord length, which in turn depends on angle of incidence of the striking particle.

This model was first proposed by Pickel and Blandford in 1978 [30] and was later implemented in several simulation codes. This method models the sensitive volume as a right rectangular parallelepiped (RRP) with lateral dimensions  $x$  and  $y$  and thickness  $z$  (Figure 3.1). The ion path through the RRP is  $s$  and is determined by thickness,  $z$ , and the angle of incidence,  $\theta$ , between the  $xy$  plane. Charge is also allowed to be collected along a funneling distance,  $s_f$ , that adds to  $s$  for the charge calculation.

The energy deposited in the sensitive volume from an ion interaction with LET,  $L$ , is

$$(3.2) \quad E \approx (s + s_f)L.$$



**Figure 3.1** Schematic of the RPP model parameters

This energy is converted to ionization charge and it is assumed that all the charge generated within the charge collection length  $s+s_f$  is collected by the sensitive volume circuit node. This model is also based on the following assumptions: ion plasma track structure can be ignored, ion LET is constant along a chord  $s$  through the sensitive volume, charge collection by diffusion from ion strikes external to the RPP can be ignored and there is a sharp threshold for upset, i.e. ions with a LET below threshold will not cause SEEs, ions with a LET above the threshold will always give SEEs.

To get a SEE rate  $R(E_c)$  prediction, the model integrates the LET distribution and the expected ion flux over the chord-length modulated by an analytic differential distribution  $f(S)$  function relation:

$$(3.3) \quad R(E_c) = A_p \int_0^{(x^2+y^2+z^2)^{1/2}} \Phi[L_t(s, E_c)] f(s) ds.$$

where the integration goes from zero to the maximum path-length through the RPP,  $A_p$  is the average projected area of the RPP,  $\Phi(L)$  is the integral flux,  $E_c$  is the threshold energy for generating  $Q_c$  and  $L_t(s, E_c)$  is the minimum average LET depending on chord length through

$$(3.4) \quad L_t(s, E_c) = \frac{E_c}{s + s_f}.$$

As already mentioned above, the RPP model assumes a step function for cross section versus LET value. However, most devices show a gradual rise from threshold to saturation, rather than a step function. This behavior is due to the superposition of composite response of multiple types of sensitive volumes, with different thresholds and with distribution of their parameters. To solve this issue, it has been proposed [31] to divide the cross-section curve into several steps in order to more accurately represent it. The generally accepted approach is to integrate in energy and weigh with the normalized experimental cross-section data

$$(3.5) \quad R = \int_{E_c}^{E_{sat}} R(E) f(E) dE.$$

where the integration range is from the measured threshold,  $E_c$ , to the measured value at saturation,  $E_{sat}$ , and  $f(E)$  is the cross-section versus LET curve converted to a probability density, described by the four parameter Weibull distribution:

$$(3.6) \quad f(E) = 1 - \exp\left[-\left(\frac{E - E_c}{W}\right)^S\right].$$

where  $E_C$  is the threshold energy, while  $W$  and  $S$  are two shape parameters used to fit the curve to the experimental data. The  $f(E)$  function represents the rate at which an energy of  $E$  is deposited in the sensitive volume. It can be regarded as the probability density for an event caused by deposition of an energy quantity equal or greater than  $E$ . This approach is commonly called the integral RPP (IRPP).

### 3.1.2 Prediction for proton-induced SEU

Only the most sensitive devices (such as high density DRAMs and CCDs) are sensitive to SEU from the direct ionization of a proton because the proton LET is so low. However, protons can cause SEU through nuclear reactions<sup>14</sup>, which result in

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<sup>14</sup> With nuclear reactions we mean both coulomb plus strong interactions with nuclei.

recoiling ions that can deposit enough energy in the sensitive volume to cause upsets even in less sensitive devices such as SRAMs.

To get reliable proton induced SEE predictions the key step is to determine the energy spectra of the ion recoils as a function of the material and the incoming proton energy; the knowledge of the energy distribution of the recoil products will then allow to estimate SEE rates following the heavy ion model. The model shown here [32] has been derived by observing how proton SEU cross-section data (as a function of proton energy) follow a relationship resembling the proton nuclear cross section in silicon. The Bendel parameter,  $A$ , was introduced on a semi-empirical basis; the original formulation had both a threshold and a limiting cross section but the single parameter  $A$  was adequate to describe the data available at the time. As more data became available, it became clear that the response of some modern smaller feature size devices was better modeled with the use of both parameters. An improved two-parameter Bendel model was suggested by two groups at about the same time, and this is the form that currently has the widest acceptance [33] [34]. The two-parameter model is expressed as

$$(3.7) \quad \sigma_p = \left(\frac{B}{A}\right)^{14} \left[1 - \exp(-0.18Y^{0.5})\right]^4.$$

where  $\sigma_p$  is a cross section in units of  $10^{12}$  upsets per proton/cm<sup>2</sup> per bit,  $A$  and  $B$  are empirically determined constants unique to a device and

$$(3.8) \quad Y = \sqrt{\frac{18}{A}}(E - A).$$

with  $E$  as proton energy in units of MeV.

The parameter  $A$  is related to the apparent upset energy threshold, while the ratio  $(B/A)^{14}$  is associated with the saturation cross section observed at high energies. The one-parameter model has  $B$  fixed at a value of 24. The advantage of the two-parameter model is that it allows better fitting of the experimental data in the high energy regions, particularly for small geometry devices, while preserving the apparent low energy proton upset threshold. Also for protons, a closer fit matching can be obtained by the superimposition of Weibull's distribution curves with

different fixed parameters. The important thing to notice here is that, in contrast with heavy ions case, the proton upset rate depends on the probability of a nuclear interaction to happen within the whole device size, and not only during the path of the proton in the device active volume.

## **3.2 Test with accelerators**

### **3.2.1 Introduction**

The final goal of this thesis is to describe a new tool to measure the SEE sensitivity of electronic devices to ionizing radiation. In this chapter we will give a review of the traditional methods employed to perform this kind of measurement, underlining the strong and the weak aspects of currently adopted techniques.

### **3.2.2 Laboratory accelerator based measurements**

The essential part of any SEE qualification process is actually performing test measurements: electronic devices undergo radiation tests to check their behavior under controlled conditions that well reproduce the environment where they are expected to work in. Simulation tools derived from first principles are certainly useful in providing some indication of SEE device sensitivity of a particular type of device, but reliable predictions of actual performances may not be made without real data, possibly collected with the very same type of device.

The radiation environment in space is widely varied in composition, energy, orbital position, time, and it is largely omni-directional. To validate a component or device for use in the space environment, irradiation facilities at particle accelerators are routinely used to test the SEE sensitivity of electronic components in controlled and repeatable conditions. A broad variety of ion species, with adequate energies, are required to perform reliable tests.

The energy of a certain type of particle delivered by an accelerator sets the LET (*Linear Energy Transfer*) and the range; i.e. the depth the particle will travel inside the target. Of course the LET of a particle varies with energy and hence it changes along the particle trajectory as the particle slows. As already mentioned, the LET is

the main reference parameter in SEE testing and one assumes that different particles with the same LET will affect the circuit the same way. The range is clearly important because the impinging particle must be able to reach the active volume of the device and therein deposit an adequate amount of energy. By knowing the range (initial energy) of the particle one can evaluate the LET at the depth of the active volume. Using ions with different ranges allow one to get information about the circuit active depth; i.e. the depth beyond which further energy deposition does not affect more the device behavior.

Clearly range and surface LET are critical parameters for competitive SEE testing. An ideal SEE facility should provide a wide range of energetic ion species. In practice a facility will be limited if heavy ions, the most useful in establishing the plateau (saturation) SEE cross-section, do not have enough energy to penetrate to the electronically active layers.

Ion	Energy (MeV)	LET (MeV × cm <sup>2</sup> /mg)	Range (μm)
<sup>1</sup> H <sup>1+</sup>	28	0.02	4390
<sup>7</sup> Li <sup>3+</sup>	56	0.37	378
<sup>11</sup> Be <sup>5+</sup>	80	1.01	195
<sup>12</sup> C <sup>6+</sup>	94	1.49	171
<sup>16</sup> O <sup>7+</sup>	108	2.84	109
<sup>19</sup> F <sup>8+</sup>	122	3.87	99.3
<sup>28</sup> Si <sup>11+</sup>	157	8.59	61.5
<sup>35</sup> Cl <sup>12+</sup>	171	12.5	49.1
<sup>48</sup> Ti <sup>14+</sup>	196	19.8	39.3
<sup>58</sup> Ni <sup>16+</sup>	220	28.4	33.7
<sup>63</sup> Cu <sup>16+</sup>	220	30.5	33.0
<sup>79</sup> Br <sup>18+</sup>	241	38.6	31.3
<sup>107</sup> Ag <sup>20+</sup>	266	54.7	27.6
<sup>127</sup> I <sup>21+</sup>	276	61.8	27.9
<sup>197</sup> Au <sup>26+</sup>	275	81.7	23.4

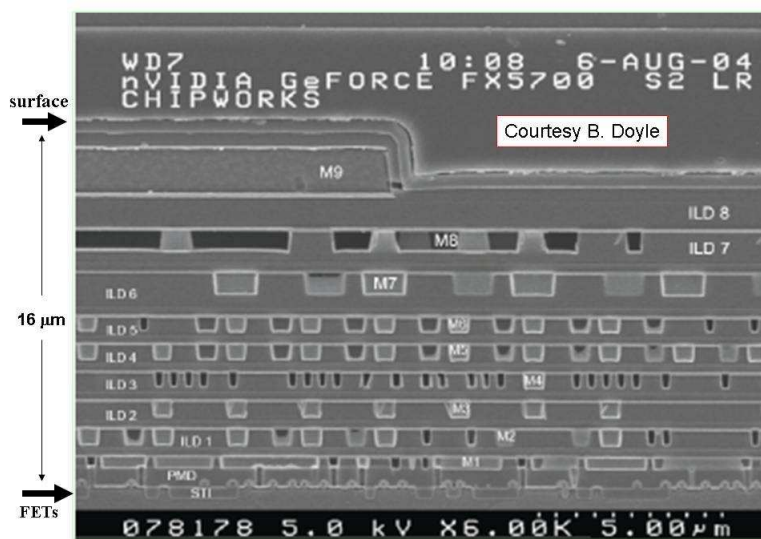
**Table 3.1 Typical Ion surface LET and range in silicon for some of the ion species available at the Legnaro Tandem accelerator.**

Tandem accelerators are used for SEE testing because they offer a wide selection of heavy ion species, they are robust and easy to use. The energy resolution, after momentum analysis, is very good ( $\Delta E/E$  better than  $10^{-4}$ ). In Table 3.1 are listed some of typical ions species available at the 15 MV Tandem of the Legnaro

Laboratories. The LET values reported are the surface LET value at the beam energy; i.e. the values as the ion enters a piece of silicon before losing energy.

Tandems are however somewhat limited in energy. Indeed the active volumes of the latest generation microelectronic devices are buried below several metallization layers and to test them requires ions with greater ranges (Figure 3.2).

SEE tests are of course performed with more energetic types of accelerators (cyclotrons, linacs, booster systems). These are less mono-chromatic, but as ion LET and range depend weakly on energy this is not a problem.<sup>15</sup>



**Figure 3.2** A cross-section of a modern device showing the thick metallization layers (courtesy B. Doyle). The active volumes (FETs) are 16 $\mu$ m below the surface.

### 3.2.3 Cross-section measurement

The occurrence of SEE in a device depends on the total amount of charge collected by an active volume and this depends on the total ion path length in the active part of the device. The SEE sensitivity is assumed to be completely described by the geometry of the sensitive volume and the critical charge  $Q_c$  associated with the particular type of single event effect. The critical charge is the amount of charge

<sup>15</sup> However the issue of high quality energy resolution beams is of capital importance if there is the need for micro-focusing the beam down to micron size, a well-established technique to perform microscopic SEE testing.



that must be collected in an active volume of the device to cause an event and depends primarily on the circuit characteristics.

In SEE testing one wants to determine the device sensitivity as a function of the amount of charge deposited. The path length and hence the charge deposited in a thin layer depends on the angle of incidence of the particle and hence it is possible to measure the SEE sensitivity over a range of charge deposition by simply varying the angle of the beam. However, the results need to be normalized to the effects of the beam at normal incidence. This idea leads to the concept of effective LET:

$$(3.9) \quad LET(eff) = \frac{LET(0^\circ)}{\cos(\vartheta)}$$

Device sensitivity measurements are then expressed as a function of effective LET. This technique works if the particle reaches depth of the active volume; i.e.  $range > depth/\cos(\vartheta)$ .

The goal of a sensitivity test is to measure the SEE cross section as a function of the effective LET. The experimental SEE cross section is given by:

$$(3.10) \quad \sigma_{SEE}(effective\ LET) = \frac{SEE\ count}{effective\ fluence} [cm^2] = \frac{SEE\ count}{fluence \times \cos \vartheta} [cm^2]$$

where the *effective fluence* is the particle fluence of the beam (respect to a unit surface normal to the beam) multiplied by the cosine of the incidence angle of the beam on the tilted target.

The results of a SEE measurement usually takes the form of a saturation-like curve with an onset at some threshold LET which then goes to an asymptotic value at higher LET values. The threshold LET determines the critical charge, the asymptotic cross section gives the area of the sensitive volume. This information, combined with the thickness of the sensitive volume, is sufficient to calculate the SEE rates of many types of devices in any given radiation environment.

A typical test consists of a series of exposures with well-defined beams (energy and fluence) over a range of LETs (or effective LETs) to allow a determination of the cross-section curve. During each exposure, the device is placed under bias, either active or passive. The SEE of interest are recognized and counted by the control

electronics driving the device during irradiation, while the particle fluence is obtained from beam dosimetry.

For phenomena regarding memory elements, like SEU, the cross section can also be given per bit by simply dividing the global SEU cross section by the number of irradiated bits per unit area:

$$(3.11) \quad \sigma_{SEE}(\text{effective LET}) = \frac{\sigma_{SEE}(\text{effective LET})}{\text{bit into device}} \left[ \frac{\text{cm}^2}{\text{bit}} \right].$$

SEUs in static RAMs best exemplify many aspects of SEU testing. Each RAM cell is, to first order, identical, and from an SEE perspective, the device is easily seen to be an array of sensitive volumes. Tests are usually performed by loading a pattern in the memory array, exposing the device to a known fluence of charged particles at a particular LET. The exposure is stopped and then the array is interrogated to count the number of flipped bits, and the cross section is calculated. Since each sensitive volume is identical, the per-bit cross section is simply the measured cross section normalized to the number of bits in the memory array. A complete experiment uses many LET values to obtain a full cross section curve of the SEE of interest.

The SEE cross section often depends on other factors, such as electrical bias or temperature, and deviates from a strict dependence on effective LET. In reality, the cross section is not a step function, but a Weibull curve (Figure 3.3) that increases with a finite slope in the threshold region, followed by a knee region, and a gradual approach to the asymptotic cross section. These deviations can be due to statistical variations in the sensitive volume geometry or in the critical charge for a volume and are significant for calculating event rates. Another source of deviation in the shape of the cross section occurs when the unit cell has more than one sensitive volume, or when several different types of cells are present, each with their own characteristic sensitive volume. In such a case one may observe a stair-shape curve which is the superposition of a many Weibull curves each with different threshold and plateau LET values (Figure 3.4).

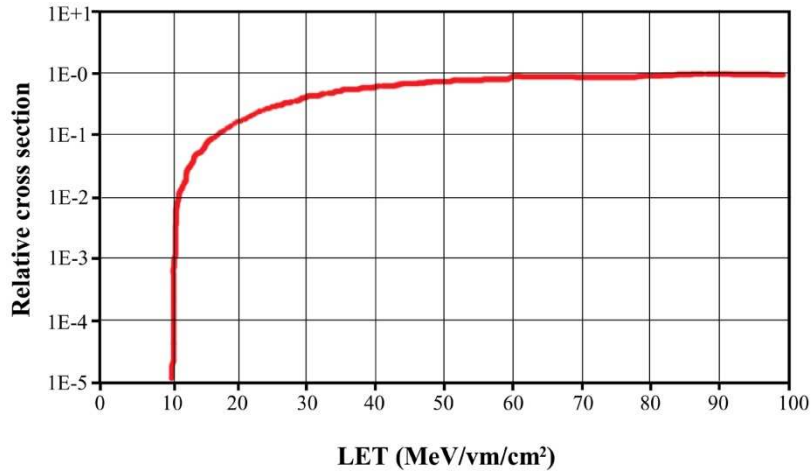


Figure 3.3 Representative heavy ion cross section curve with cross section expressed as a function of effective LET. This curve has Weibull parameters:  $L_0= 10\text{MeV/mg/cm}^2$ ,  $W=30\text{ MeV/mg/cm}^2$ , shape parameter = 1.6.

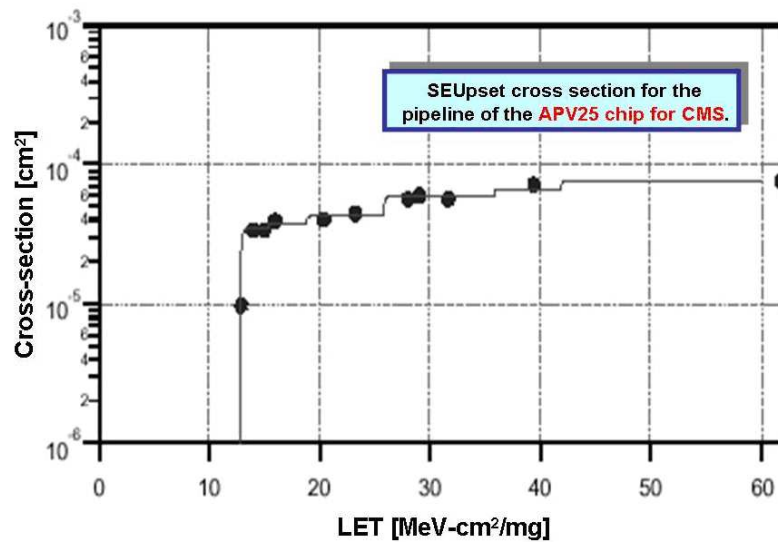


Figure 3.4 The SEU cross-section experimental data and multiple-Weibull fit of the pipeline of the APV25 frontend chip for the CMS detector at LHC. [35]

### 3.2.4 Proton SEE testing

Energetic protons generally do not deposit enough energy in a sensitive volume to directly cause SEEs. However, approximately one in  $10^4$  to  $10^6$  protons undergo reactions with nuclei of the Si atoms in the device and produce energetic residual range nuclei (recoils or fragments). If produced in or near a sensitive volume, the

residual nuclei can deposit enough energy to cause an SEE. The residuals are short-range ions that will deposit most or all their energy within the sensitive volume.

Proton testing proceeds much like heavy ion testing in that the sample is exercised while exposed to a beam for a given fluence. Events are counted in each exposure, and the event cross section is calculated by dividing the number of events by the fluence for the exposure (recall that the effective fluence is used for heavy ion testing). This procedure is repeated over a range of proton energies to fully characterize the cross section as a function of energy. Three issues, however, make proton testing significantly different from heavy ion testing. First, and foremost, samples experience significant total ionizing dose damage when exposed to proton beams (to obtain useful statistics in proton testing one must compensate the very small probability of indirectly causing a SEE by irradiating up to relatively high proton fluences, several orders of magnitude higher than those used with heavy ion testing), and the event cross section can be different as damage accumulates. Care must be taken to plan experiments so that the device characteristics are not unduly altered during the measurements. Second, since the nuclear interaction probability does not depend on the beam incident angle and the reaction products deposit nearly all their energy in the sensitive volume, the cross section is assumed to only depends on the proton energy. As a result, for proton testing, there is no equivalent concept to the effective LET used in heavy ion testing. Finally, the physical layout of proton exposure facilities and safety concerns for human experimenters adds considerable complication to experiment and equipment design.

### **3.3      *Radiation Effect Microscopy (REM)***

#### **3.3.1      Introduction**

In previous paragraphs, an overview of device characterization with respect to SEE sensitivity was given, and the concept of global cross section was introduced. This type of tests provides fundamental data regarding the reliability of electronic circuits in radiation environments: the knowledge of the cross section curve versus LET allows one to predict how a device will be affected from a random exposure to ionizing radiation. As the whole device, or a macroscopic portion of it, is exposed to

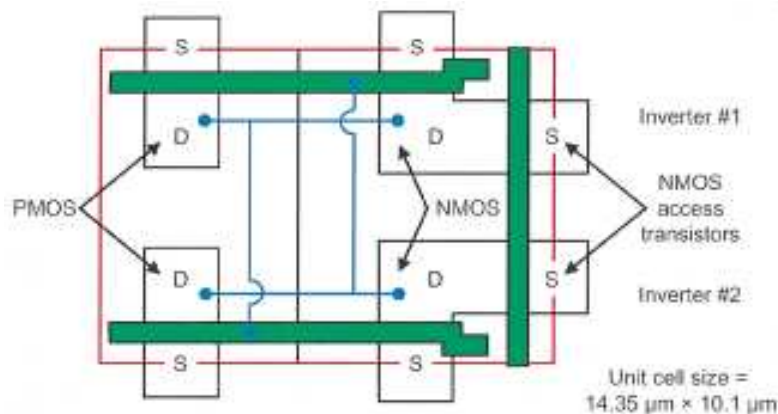
a broad beam, this method cannot indicate the specific reason for radiation sensitivity. To do so would require knowing the location of the ion impacts. Device simulations can be used very effectively to pin point the sensitive parts of a device; e.g. determine which parts of a device are sensitive to SEE (e.g. which transistor in a latch; which logic element in an IC; etc. etc.). But experimental data is ultimately desirable, if only because data is necessary to validate any simulation.

Radiation Effects Microscopy (REM) provides a way to correlate device response (occurrence of an SEE; anomalous *Ion Beam Induced Charge Collection* (IBICC)) to the impact points of incoming particles. REM experiments are usually performed with a microprobe system that systematically scans the device under test with a low-intensity highly focused ion microbeam.

### 3.3.2 A REM example

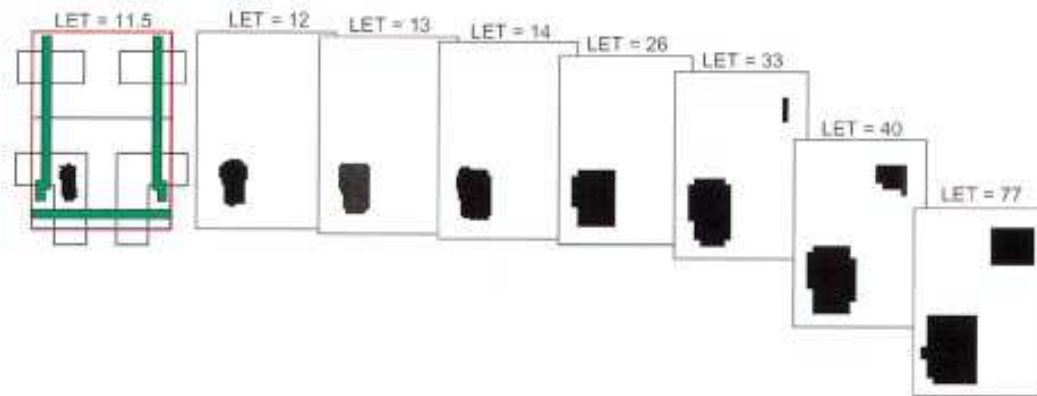
A famous example of REM has been performed by SANDIA laboratories [36], where predictions resulting from simulations with DA VINCI code and experimental results were compared.

Two CMOS6r SRAM ICs were studied in this work, a 16 K SRAM test chip known as the TA788, and a 256 K SRAM standard evaluation circuit (SEC) known as the SA3953 (Figure 3.5).



**Figure 3.5** Layout of 256 K 6-transistor SRAM unit cell (D = drain and S = source). The red box indicates the boundaries of the unit cell, the green regions are the gate polysilicon lines, and the blue lines show the interconnections within the unit cell.

The simulations were performed for energetic ion strikes incident every  $0.5\mu\text{m}$  throughout the unit cell to give a map of the SEU-sensitive area of the SRAM unit cell. By repeating these simulations for several ion/energy combinations, the evolution of the sensitive area as a function of ion LET has been generated, as shown in Figure 3.6.



**Figure 3.6** Evolution of the soft-error sensitive area (black regions) of a 256 K SRAM unit cell as a function of increasing ion LET

As one can see from the picture, different parts of the circuit start begin to be sensitive at higher LET values, and only a few components are the cause of the radiation sensitivity of the cell. In a global irradiation experiment such a behavior would give rise to a double step Weibull cross-section curve.

The simulation results are impressive. However they require enormous computing time, even on a parallel supercomputer, and cannot represent a definitive verdict about the radiation hardness of a circuit, as they rely on the many assumptions necessary to implement a computable physical model.

To perform a direct validation of a such a rich simulation it is necessary to use an experimental system that is capable of registering both the effect and the position of impinging ions with a spatial resolution compatible with the feature size of the device under test. To provide validation of the Da Vinci simulations at the level of individual memory cells (Figure 3.7), REM experiments were performed at the heavy ion microprobe facility on the EN tandem Van de Graaff at Sandia.

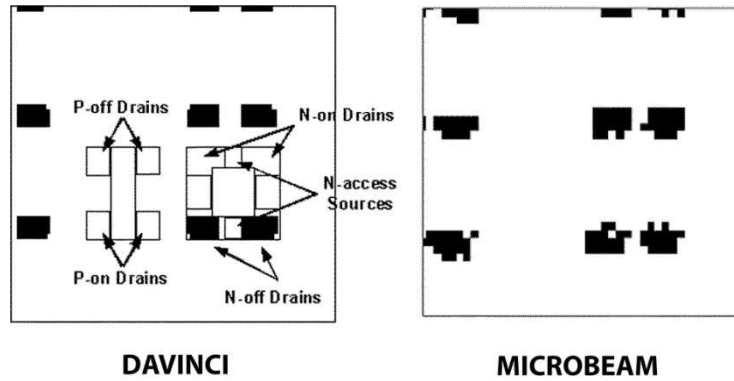


Figure 3.7 SEU image of several unit cells in a TA788 16 K SRAM obtained with 35 MeV chlorine ions using a heavy ion microprobe and equivalent simulated SEU map for 35MeV chlorine ions.

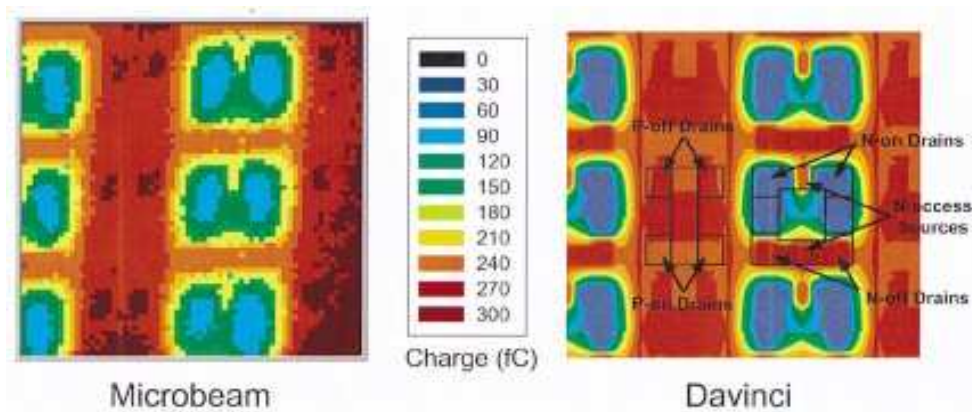


Figure 3.8 Left: calibrated IBICC image of several unit cells in a TA788 16 K bulk SRAM obtained with 20 MeV carbon ions using a focused ion microbeam. Right: equivalent simulated charge-collection map for 20-MeV carbon ions. The color scales for both maps are the same and indicate total charge collection measured at the power supply.

In addition to the soft-error sensitive region for a given ion/energy combination, the simulations give the transient currents in the SRAM cell as a function of ion strike location. By integrating the current over time it is possible to compute the total charge collection as a function of ion strike location in an externally accessible contact. Comparing the simulated charge-collection images to experimentally measured calibrated IBICC images obtained from the heavy ion microprobe, is helpful to further validate the accuracy of the simulations. Figure 3.8 shows a 20-MeV carbon-ion calibrated IBICC image of several unit cells of the TA788 16 K

SRAM, along with the simulated charge collection. 20-MeV carbon ions have an LET of 6 MeV-cm /mg, below the upset threshold.

The simulated and measured IBICC images generally agree to within about 20–30%. The validation experiments shown here indicate that mixed-level device/circuit simulation tools such as Da Vinci are well suited to SEU modeling of bulk CMOS SRAMs.

## **3.4 Microbeam techniques**

### **3.4.1 Introduction**

A microbeam allows one to precisely probe SEE sensitive areas of a device. In addition the amount of ion beam induced charge collected at specific locations on the integrated circuit can be measured and the depth of charge collection of the device can be calculated. These microprobe techniques, when coupled together, give a detailed picture of the mechanisms responsible for SEE that is impossible to obtain by other means. Microbeam techniques are also essential for transient charge collection measurements to ensure that signal arises from only the region of interest. When coupled with modern simulation tools, a complete picture of SEE emerges.

In the following paragraph we will discuss the main ways to implement microbeam techniques.

### **3.4.2 Microbeam apparatus**

The first approach consists in placing a diaphragm with a pin-hole aperture between the sample and a heavy-ion source (such as an accelerator) and collimating the ion beam to a diameter of a few micrometers. The test sample, and in some cases the aperture, is positioned on an  $x$ - $y$  stage to move the microbeam to a specific region of the device. Aperture sizes that can be used range from tens of  $\mu\text{m}$  down to about 2.5  $\mu\text{m}$ . Micro-collimator systems based on glass tube micro-capillaries have also been used with radioactive alpha sources, such as a polonium tipped wire.



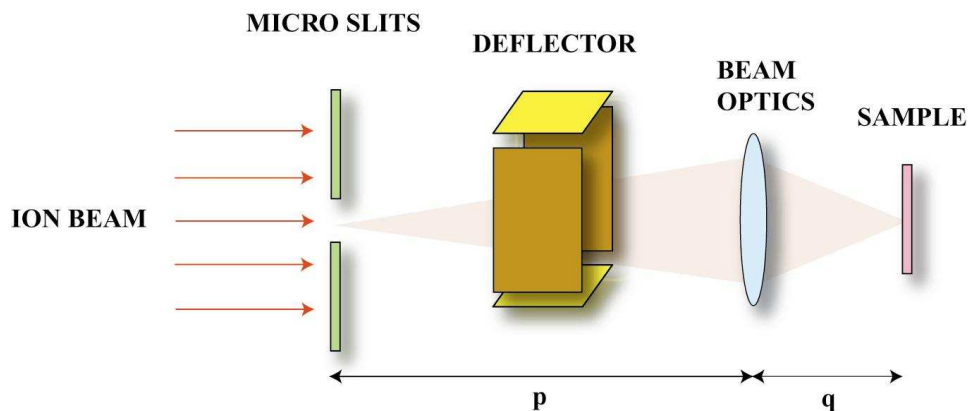
A significant fraction of beam particles interact with the edge material of the aperture and produce a wide spatial and energy distribution of background particles (beam halo) that will affect the analysis. This limits the achievable spot size of micro-collimator systems to about 2  $\mu\text{m}$  (as distance of the aperture and the sample is on the order of 0.5 cm). The beam halo increases with increasing atomic number and energy. Secondly a micro-collimator system cannot be scanned rapidly. In addition the beam current falls rapidly with the diameter of the aperture. This is problem if high statistics experiments are to be performed on low sensitivity devices. All these limit the effectiveness of the micro-collimator technique for studying feature sizes smaller than a micron.

The second technique performs magnetic micro-focusing of the beam, and the scanning of the regions of interest on the device is achieved either by a electrostatic or magnetic means. A schematic of a magnetically focused system is shown in Figure 3.9. The beam optics is represented by a lens. In practice a microbeam facility will include: pre-slits, a magnetic beam switch, microslits, antiscattering slits, a beam scanning (rastering) system, a magnetic beam deflector, a lens diaphragm, the lens (a system of magnetic quadrupoles, usually a triplet), an optical microscope, and finally the sample stage. The optical microscope helps to aim the beam onto the target. In addition one might include an ion impact detection system to certify the arrival of an ion on the targeted position. This can be done by detecting the secondary electrons emitted from the target surface when impacted by the ion. Finally the vibrations must be reduced to acceptable levels. Vibrating pumps (turbo and cryopumps) are coupled to the microscope chamber via soft bellows and vibration free pumps (ion pumps) are used along the beamline between the microslits and the lens. In some facilities the microprobe is isolated from vibrations from the floor by air springs.

To date, various microbeam facilities exist with different performances (e.g. beam spot sizes, ions species and energies). For SEE studies the most important facilities are:

- the heavy ion microbeam of GSI (Darmstadt, Germany). The linear accelerator UNILAC delivers ions from C to Ur with energies between 1.4 MeV/nucleon to 11.4 MeV/nucleon. It has been operational since 1987 and beam spot sizes of 0.5  $\mu\text{m}$  are routinely achieved [37] [38];

- the more recent microbeam at the SNAKE facility (Munich, Germany). The accelerator is a 14 MV tandem and delivers ions, from 20 MeV protons to 200 MeV Au. Beam spots of 0.5  $\mu\text{m}$  have been achieved [39] [40];
- The microbeam at TIARA (Takasaki, Japan). The accelerator is the JAERI AVF cyclotron accelerates heavy ions (up to Ur) with energies up to 27.5 MeV/nucleon. The energy spread of the accelerator has been greatly reduced recently allowing the microbeam to achieve spot sizes  $\cong 0.8 \mu\text{m}$  [41].



**Figure 3.9** A schematic of a magnetically focused scanned microbeam system.

As shown in Figure 3.9, the beam spot on the target plane is the transmitted image of the aperture slit. The electrostatic/magnetic lenses of the beam-optics produces a demagnified image of the slit on the focal plane. For a simple lens, the magnification ratio is given, to first order, by the ratio  $q/p$ . The demagnification of the beam size performed by the lens allows one to work with a large slit aperture, giving a higher beam current and a sharper energy distribution of the focused particles. By means of electrostatic deflection, it is easy to rapidly scan the focused beam across the sample.

Charged particles are accelerated, steered and focused using a combination of electrostatic and magnetic fields. The deflection of a beam passing through a uniform magnetic field  $B$  of length  $l$  ( $Bl$  in Tesla metres) is

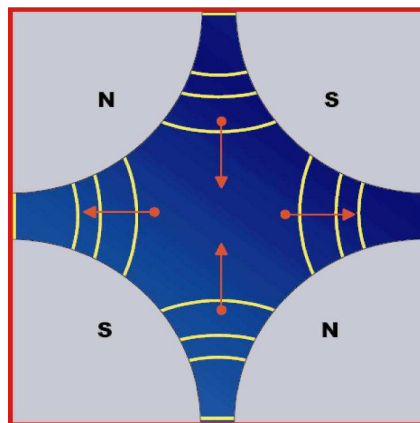
$$(3.12) \quad \sin \theta = \frac{3.48Bl}{\sqrt{(EA/Q^2)}}.$$

while the deflection of a beam passing through a uniform electrostatic field  $V/d$  ( $\text{Vm}^{-1}$ ) of length  $l$  metres is

$$(3.13) \quad \tan \theta = \frac{5 \cdot 10^{-7} VQl}{d \cdot E}.$$

where  $A$  is the particle mass,  $Q$  is its charge and energy  $E$  is expressed in MeV. The much higher effectiveness of magnetic bending in curving high energetic particles makes it the most used way to bend ion beams.

The usual way to focus MeV ions is through quadrupole lenses (Figure 3.10).



**Figure 3.10** Quadrupole lens schematic. Beam direction is toward the page.

A magnetic quadrupole consists in four poles arranged symmetrically about the beam axis generating a hyperbolic field profile normal to particle motion axis. In the illustrated configuration the field is normal respect to the beam axis, so ensuring strong force applied toward the axis, a fundamental condition to allow beam focusing. Note that this kind of lens focuses the beam along one axis while it defocuses the beam along the orthogonal one: this means that to focus the beam in both axis at least two carefully matched quadrupoles are needed (doublet configuration). To get submicron beam focusing (high demagnification ratio), at present both triplet (“Oxford”) and quadruplet (“Russian”) multi lens system are used (Figure 3.11).

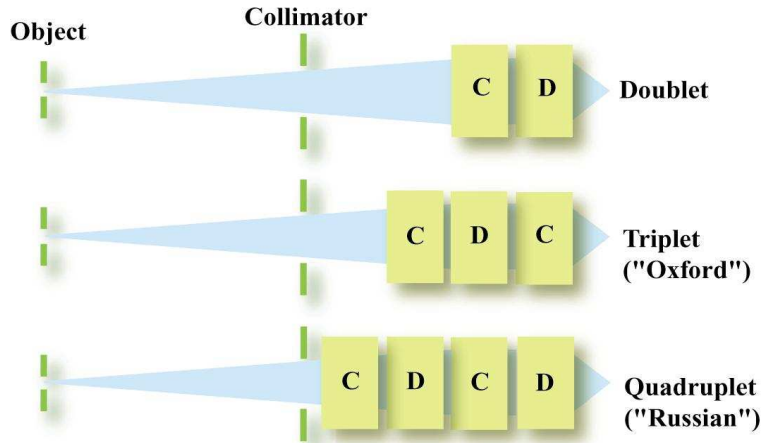
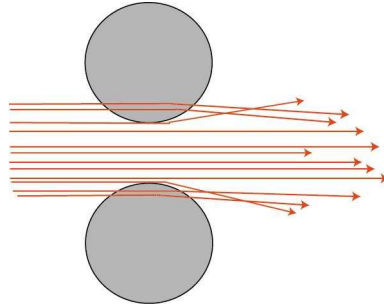


Figure 3.11 Common microbeam lenses configurations.

At present the best performances for a microbeam (in term of resolution) belongs to the group of F. Watt at the University of Singapore [42]: using an Oxford OM-2000 triplet, a 3 MeV proton beam is focused down to a spot of 300 nm by 400 nm in size. This is truly an impressive result, but it is practically of no interest in the field of Radiation Effects Microscopy as it is difficult to maintain similar levels of performance with high mass high energy ions. No significant improvements in spatial resolution have been reported in over 5 years. To understand the reason of this stagnation, we need to consider the main causes that set a limit to the practical resolution obtainable with a microbeam.

Several factors limit the final resolution in a microbeam system, i.e. the beam spot size on the target. Some of them are engineering issues and presumably it would be possible to solve them. They span from mechanical stability (vibrations, long term drift due to thermal changes, for instance) to stray magnetic fields. Also scattering from residual gas in vacuum can contribute to worsen the resolution.

On the other hand two main issues are directly related to microbeam systems. First, a microbeam works by projecting a demagnified image of an object, the slit aperture. When the beam passes through the slit, particles that interact with the edge are scattered and arrive to the optical system with different energies and direction with respect to an ideal, parallel and monochromatic beam (Figure 3.12).



**Figure 3.12 Ions scattering due to interaction with slits.**

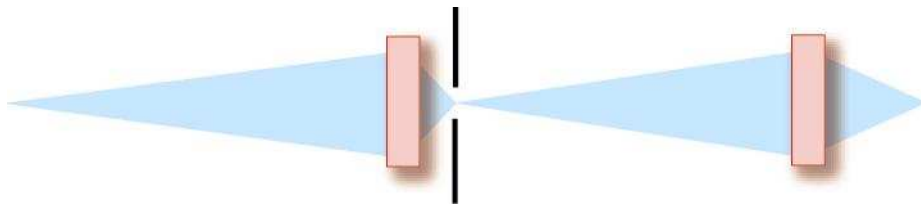
Lenses can correctly focus only particles with energy and direction inside a narrow spread around specific values, so scattered particles are poorly focused by the optics and form a halo around the ideally focused beam spot, decreasing the final resolution. In table 3.2 we report the ratio of scattered ions versus direct ions for different ranges and slit apertures.

	Slit aperture ( $\mu\text{m}$ )	
Range ( $\mu\text{m}$ )	20	1
60	0.060	1.2
10	0.002	0.033

**Table 3.2 Ratio of scattered beam versus direct beam.**

As one can see from the table, for ions with a range of 60  $\mu\text{m}$  in the slit metal, the ratio of scattered ions versus direct ions goes from 0.06 for a 20  $\mu\text{m}$  aperture to 1.2 for a 1  $\mu\text{m}$  aperture. This means that there is a lower limit on the minimum usable aperture size set by the increasing aberration due to scattering phenomena, and this limit sets the smallest available beam size on target, as the demagnification is a fixed parameter of the design.

To improve resolution, the common approach is to adopt high demagnification systems, usually employing more sophisticated optics or multi stage systems (Figure 3.13).



**Figure 3.13** Schematic of a multi-stage system.

This configuration provides for an aperture at the intermediate image plane which removes the halo from the slit scatter. The high overall demagnification allows a large object aperture and, as the final stage can have long working distance, it helps design of target chamber.

It is important to note that, in principle, higher demagnifications should allow one to use larger object slits, but in practice they are not because it usually means higher aberrations.

The second major issue is that microbeams, like all optical systems, suffer from aberrations due to the lenses themselves. These aberrations may be divided into two main categories: geometrical and chromatic. Aberrations blur and deform the ideal focused spot so degrading the overall system resolution.

Geometrical aberrations are generated by imperfections of the optical system: e.g. the field shape is not exactly hyperbolic; the yokes are not perfectly aligned with the beam; the power supply exhibits ripples that affect the uniformity of fields in time, and so on. An improved engineering and/or more sophisticated optical design can greatly reduce the effects of this kind of aberration. Instead, differently from geometrical aberrations, chromatic aberration is an intrinsic behavior of any lens, and cannot be corrected by improving lens manufacturing. The only way to significantly reduce chromatic aberration is to implement a multi-lens design where the net chromatic aberration is removed by mutual cancellations between lenses. While such an approach is common in conventional optical system, at present ion beam optics technology cannot provide an equivalent solution. Hence, the only practical way to keep chromatic aberration under control is to have an extremely monochromatic beam: the particle beam energy spread must be as small as possible and the mean beam energy value must remain constant over time. As high-energy accelerators of heavy ions with monochromatic beams are hard to obtain, this is by far the most important intrinsic limitation in using a microbeam to perform Radiation Effects

Microscopy. The production of the microbeam with a spot size as small as 1 $\mu$ m by quadrupole lenses requires the energy spread of the beam  $\Delta E/E < 0.02\%$ . Even in the case of an ideally monochromatic beam, strong magnetic lenses are required to bend heavy and energetic ions necessary for SEE testing.

At present, the best results in focusing down to micron size heavy energetic ions were obtained by the microbeam at the SNAKE tandem ( $\Delta E/E < 0.01\%$ ) that uses superconducting focusing quadrupoles. They have focused 100 MeV  $^{16}\text{O}$  down to a spot diameter of 500 nm [43] and lateral resolutions as low as  $\Delta x = 600$  nm and  $\Delta y = 150$  nm have been reported.

Recent important progress has been made at the AVF cyclotron of TIARA. The energy spread in the cyclotron beam depends on a waveform of the acceleration voltage and beam phase acceptance of the cyclotron. The typical energy spread of the cyclotron beam is around 0.1% in the ordinary acceleration mode using a sinusoidal voltage waveform. Recently the energy spread was successfully reduced to allow for submicron beam spots by superimposing a fifth-harmonic voltage waveform on the fundamental one to generate a flat-top waveform for uniform energy gain.

### 3.4.3 REM limits

The main limitation of microbeam is the difficulty to work with energetic heavy ions necessary for SEE sensitivity measurements. In addition, as new circuits grow in complexity, the direct irradiation of the front surface of a device becomes more difficult to do because of the presence of structures and several micron thick layers of metallization for surface electrical contacts (Figure 3.14 a) that can affect the beam before it reaches the sensible nodes of the circuit.

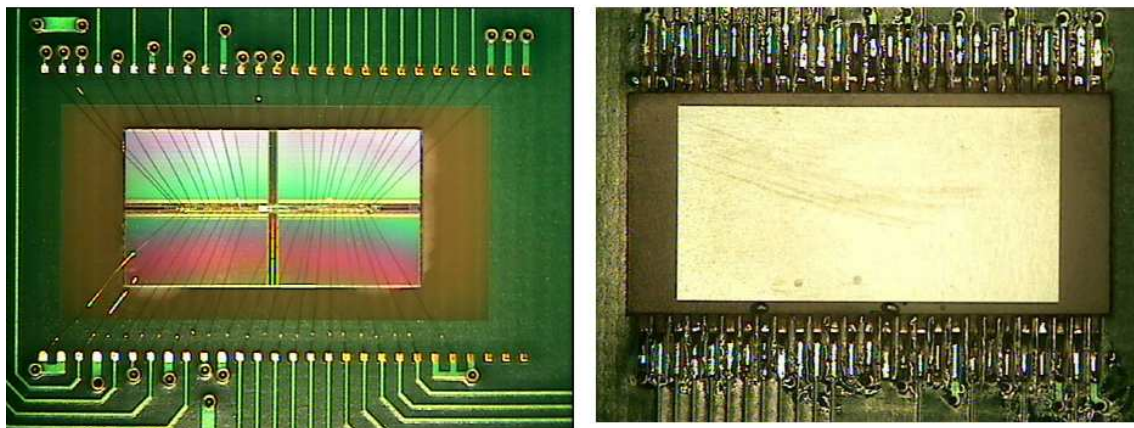
In the case of ASICs or R&D test structures, it is generally possible to obtain tailor-made samples especially conceived for REM investigations. But for the growing majority of standard production devices (COTS) a similar procedure is clearly not possible.<sup>16</sup> The dense layers and superstructure will clearly degrade the energy of the impacting heavy ion. This is an important problem when one considers that not all SEE depend only on the charge induced in the thin ( $\sim 1$   $\mu$ m) active layer

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<sup>16</sup> In any case the plastic case should be removed.

of the device. For instance a SEL involves the collection of charge from depths extending for several micrometers and it is generally considered appropriate to test for SEL using ions for which the range in silicon is at least about twice the epitaxial layer thickness. Nonetheless, space agencies (NASA, ESA) require dedicated validation measurements with greater range ions to remove all doubts about SEL rate test. These considerations exemplify the importance of developing irradiation facilities at ion accelerators at even higher energies.

A feasible approach for SEE irradiation at higher energy ion accelerators consists in irradiating the sample from the backside thereby avoiding all the surface structures on the top side. This technique requires a back-thinning procedure to reduce as much as possible the thickness of the silicon substrate (Figure 3.14 b). Anyway it requires that the ions travel through the substrate for several tens of microns ( $\sim 50 \mu\text{m}$ , in the example) before reaching the sensible structures on the front surface of the device.



**Figure 3.14 Hyunday 256-Mbit SDRAM, front side (a) and back-thinned sample (b)**  
(Courtesy of ESA)

This trend, requiring high range, hence high energy heavy ions, is difficult with microbeams for two reasons. First, as already stated, it is difficult to focus heavy energetic ions. Second, to accelerate ions to even higher energies requires accelerating machines different from electrostatic accelerators such as Tandems that are the most suitable for microbeams. Microbeams are used in combination with electrostatic accelerators because they provide the highly monochromatic and stable beam necessary for the microbeam optics to achieve micron resolutions. In table 3.1 we list the typical ion species and energies deliverable by a big electrostatic accelerator (15 MV Tandem of the INFN Legnaro National Laboratory). The values



listed well represent the practical upper limit to the energies obtainable by such kind of machines. Note that for LET values higher than  $20 \text{ MeV}\times\text{cm}^2/\text{mg}$  ( $^{48}\text{Ti}$  at 196 MeV) the ion range in silicon falls under  $40 \mu\text{m}$ , a value that is considered a lower limit to allow performing backside device irradiation.

To obtain higher range heavy ions for future state-of-the-art SEE testing requires using a different type of accelerator system, such as using RFQ boosters at the exit of an electrostatic accelerator, cyclotrons or even more complex accelerator systems. Cyclotron accelerators and boosting systems, while able to deliver heavy ions with higher energies, even higher than 1 GeV, do not ensure the beam monochromaticity and stability necessary for microbeam systems.

For SEE testing there is at present the need to ensure good resolutions for very energetic (high range) ions over a very wide range of heavy ion species (high Z for high LET). It is important to note that the feature size of state-of-the-art electronics is less than 100 nm, more than a factor three smaller than the very best microbeams. It is unlikely that microbeam resolutions will improve much. On the other hand electronic technology continues to evolve and feature sizes continue to shrink.<sup>17</sup> No foreseeable microbeam design will ever reach comparable resolutions.

We conclude that present REM techniques are limited when evaluated in terms of present and certainly future requirements for SEE testing with heavy ions with high LET and large range values. This is the reason for the necessity to have an alternative and flexible approach to Radiation Effect Microscopy, that we are going to describe in the following chapter.

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<sup>17</sup> The feature size of present technology is already comparable to the lateral spread of the ions due to multiple scattering in the metallization layers  $\sim 10\mu\text{m}$ .



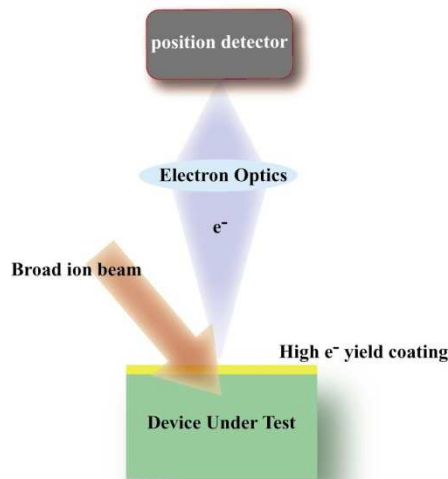
## 4 Ion Electron Emission Microscopy

### 4.1 *An alternative approach*

#### 4.1.1 Introduction

An alternative to the traditional microbeam technique, Ion Electron Emission Microscopy, was first proposed in 1999 and developed by the group of B. L. Doyle at SANDIA National Laboratory [44].

This approach discards the need for precisely focused and scanned ion beams and uses a broad (non-focused) beam (Figure 4.1).



**Figure 4.1** Schematic of IEEM technique: the position of the impinging ions is revealed by imaging the emitted secondary electrons.

Instead of relying upon the scanning system to know where the ion beam spot is when a radiation effect is detected, the IEEM technique precisely images the position of the secondary electrons emitted from the surface of the target as a result of single ion impacts. The secondary electrons are collected by a series of electrostatic lenses

and the magnified secondary electron image of the target surface is projected onto a focal plane. To reconstruct the impact points of the impinging ions the electron emission points of the hit surface are imaged by coupling the electron emission microscope to a fast two-dimensional position detector that gives the spatial coordinates of the ion impacting with micrometric resolution. The detector time-resolves individual ion hits in the field of view of the microscope up to impact rates of several kHz. The timing of the emissions of secondary electrons at the mapped positions on the sample surface is correlated with the ion-induced signals from the device or material sample under test to match a particular ion interaction to a particular place on the sample.

It is important to keep in mind that the IEEM technique is not *perfectly* equivalent to traditional microprobes. The possibility to aim with micrometric precision at the target is a prerogative of microbeams and this is an extremely useful feature when one has a reason to test a very specific spot of the device under test. An IEEM instead furnishes only the precise coordinates of random ion impacts in a small area (hundreds of square microns). A systematic scan with a microbeam or the random IEEM technique are used when the user does not know “a priori” which spots of the device are more critical.

The traditional microbeam approach is arguably the preferred one, as one can decide where the next ion is going to strike, but it needs by far greater development. It is very challenging to focus to micron size a wide variety of energetic heavy ion beams. A competitive SEE heavy ion microbeam facility for modern microelectronic devices is invasive and requires great technical, human and economic resources to develop and implement. On the other hand an IEEM is relatively simple, not too expensive and compact; i.e. it can be easily installed and used by a relatively small group of people at high energy heavy ion accelerators, such as cyclotrons and post-accelerators that deliver ions with great range and are more suitable to test the latest microelectronic devices.

#### **4.1.2 Secondary electron emission – generalities**

The physical mechanism at the basis of Ion Electron Emission Microscopy is the emission of secondary electrons from the target surface as a consequence of an ion

strike. The average number of secondary electrons emitted for each impact depends on the interaction of that particular ion with the target surface and is an important parameter for an IEEM since it sets the efficiency of this technology [44].

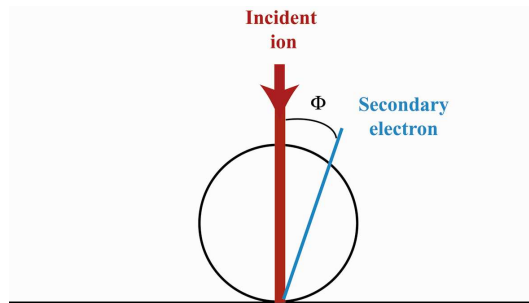
According to the theory of Sternglass, the physics of secondary electron production involves three stages:

- *formation of secondary electrons*: the energy lost by fast ions is given up in two types of collision processes: elastic collisions where low energy (1÷20 eV) secondary electrons are produced; inelastic collisions that give rise to energetic knock-on electrons ( $\delta$  rays) which, in turn, produce secondaries that may then produce tertiaries, and so on, in higher order collisions. Although the number of  $\delta$  rays is very small, the total energy going into their formation approximately equals that going into the direct formation of slow secondaries at high ion velocities;
- *secondaries diffusion*: low energy secondaries move by diffusion through the medium. Elastic collisions involve small amount of energy transfer to the thermal vibrational modes of the lattice and it takes on the average only a few collisions (2÷5) to reduce the energy of a secondary below the minimum value necessary to overcome the surface barrier potential. Considering that the mean free path between collisions in metal is approximately of the order of a nanometer, escaping secondary electrons are only those produced at shallow depths in the target, about 1÷5 nm below the surface;
- *emission* into vacuum by overcoming the surface barrier, which is the surface dipole potential, originated by the asymmetry in the electron charge cloud of the surface atoms projecting outward beyond the positive charges of the ion core.

According to Sternglass theory [45], the electron yield  $Y$  (i.e. the average number of secondary electrons able to escape from the surface for ion impact) is:

$$(4.1) \quad Y = P \frac{\lambda}{\cos \theta} \frac{LET_0}{W}$$

where  $\lambda$  is the Mean Free Path (MFP) for electron scattering,  $\theta$  is the beam's angle of incidence,  $W$  is the ion energy required to ionize an electron in the medium,  $P$  is the probability for an electron to escape the surface potential barrier and  $LET_0$  is the value of the LET of the ion at the surface of the target. The emission depth is thought to be very shallow (1÷5 nm) for metals but much larger for insulators [46] and has a cosine angular distribution [47] (Figure 4.2): the maximum number of secondary electrons is emitted along the surface normal ( $\Phi = 0^\circ$ ).



**Figure 4.2** Angular distribution of secondary electrons emitted by the target surface for normal impact.

The energy distribution of the secondary electrons is peaked at a few eV, and the shape of this distribution is independent of ion species and energy. The LET parameter is here assumed to be constant (equal to  $LET_0$ ) due to the fact that the very few nanometers under the surface, where secondary electrons are produced, is a small depth compared to the range of energetic incident ions. As a result, to a very good approximation, one may consider the emitted secondary electrons to have originated in at a depth in which the incident ions still possess their original energy. The amount of energy lost per unit path length which is available for secondary electron formation may accordingly be taken as constant throughout this region.

Equation (4.1) can be contracted in the following form by grouping all medium-dependent parameters:

$$(4.2) \quad Y = \Lambda \frac{LET_0}{\cos \theta}.$$

The  $\Lambda$  parameter represents the medium respect to ion induced secondary electron emission and ranges, for smooth metal surfaces. Its value is reported to range between 0.07 and 0.13  $\text{\AA}/\text{eV}$  (in the energy range from 80 keV to 1 MeV [48]), but can be significantly reduced by surface structures/defects that perturb the electric field uniformity.

The most important approximation made in (4.2) was to assume the extraction work to be independent from the ionization track generated by the ions: while this is a good approximation for lighter ions (protons), ionization becomes relevant for heavy ions. As a consequence of the strong ionization of heavy ions, the secondary electron yield is significantly diminished and the  $\Lambda$  parameter is not a constant but it depends on the ion species and energy [46].

As no experimental data on the electron yield from gold surfaces from energetic heavy ions available at SIRAD was present in literature, specific measurements were performed at SIRAD using a wide selection of ions [76]. We used three Au targets (one bulk and two thin gold deposition, 70  $\mu\text{g}/\text{cm}^2$  and 200  $\mu\text{g}/\text{cm}^2$  on 2  $\mu\text{m}$  thick mylar). Measurements were also made using an aluminum (oxidized) target.

In figure 7.15 we show the experimental yield data for the Au target of table 7.4 as a function of the atomic number  $Z$ . The figure also shows the expected values at SIRAD with the tandem at 14 MV and using the highest probability charge states. The dashed black curve shows the expected yield if one naively assumes it to be proportional to the LET of the ion, while the red diamonds, joined by the red dashed curve, are the expected yields for the typical ions and energies available at SIRAD according to fit function:

$$(4.3) \quad Y = a \cdot Z^{b-2} \cdot LET_0 \left( eV/\text{\AA} \right)$$

For Au targets the best fit parameters are  $a = 0.168 \pm 0.015 \text{\AA}/\text{eV}$  and  $b = 1.561 \pm 0.035$  using the  $LET_0$  ( $\text{eV}/\text{\AA}$ ) values of SRIM2003. The best fit function represents the average yields value, the effective secondary electron emission by ion impact on Au following Poisson statistics, as shown by Itoh et al. [77] for ions with  $Z \geq 10$ . For

$\text{Al}_2\text{O}_3$  the best fit parameter values we obtained are  $a = 0.268 \pm 0.041 \text{ \AA/eV}$  and  $b = 1.51 \pm 0.06$ .

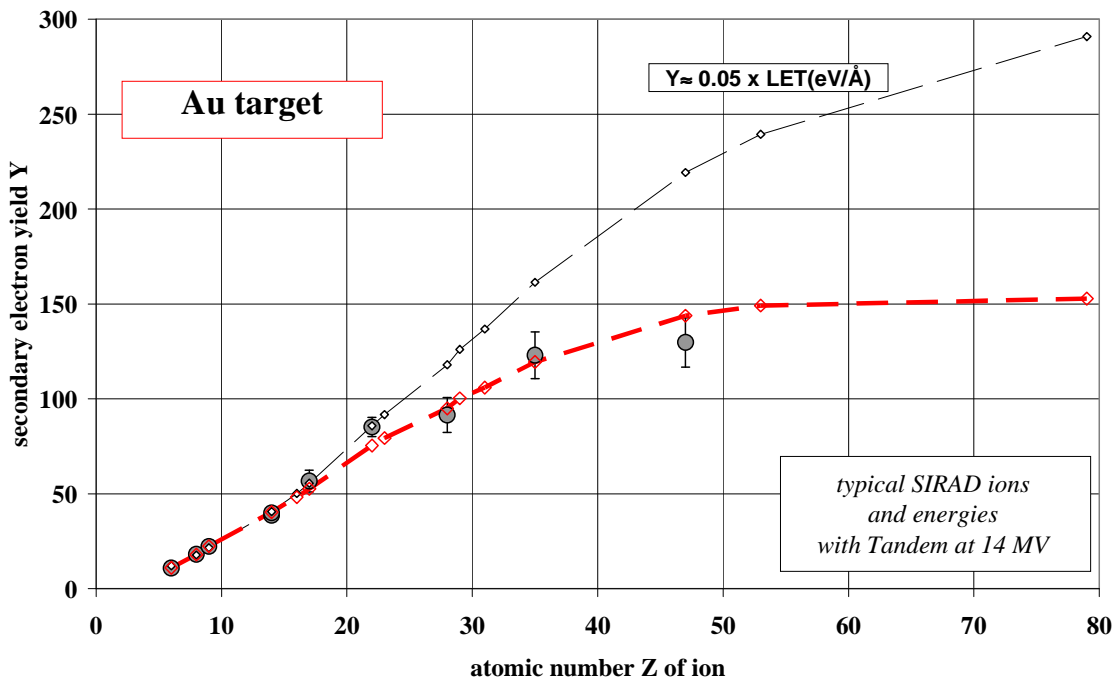


Figure 4.3 The mean number of secondary electrons  $Y$  emitted from a gold target expected at SIRAD as a function of the atomic number  $Z$  of impinging ions. The data points are the values obtained at SIRAD. The red diamonds, joined by the red dashed curve, are the expected values according to the fitting function 7.2. The black dashed curve is the expectation assuming naively that  $Y$  be proportional to the LET.

We note that the mean energy of emitted electrons and energy spread are important factors for electron emission microscopy as they affect the final resolution. In the same experiment we measured that secondary electrons are emitted from Au surfaces with energies up to around 5 eV.

While the above picture is a good approximation for metals, matter is quite different in the case of insulators where slow electrons cannot lose their energy by elastic collisions with conduction electrons and this results in an increased free mean path. The increased path length and the inelastic collisions that characterize the transport of electrons in semiconductors/insulators make the path of the secondaries much more complicated than that described in conductors. Moreover in semiconductors and insulators the medium ionization is a threshold process, because the ion energy loss per interaction is higher than the small amount we found in



conductors. In addition charge-accumulation effects increase the surface potential barrier. For these reasons the emission yield for semiconductors and insulators is greatly reduced, if not absent at all. This is of great importance as many semiconductors devices present protective passivated layers ( $\text{SiO}_2$ ) on their surface, making them potentially unsuitable for the IEEM technique unless their surfaces are first suitably treated.

Measurements performed by the Doyle group observed no emission from the passivated surface of a PIN diode [44]. This indicates the need to perform some kind of surface preparation in the case of a non-emitting sample. This preparation should provide a sufficiently high secondary electron yield to allow the IEEM to detect ion impacts with reasonable efficiency.

## **4.2      *Electrons imaging***

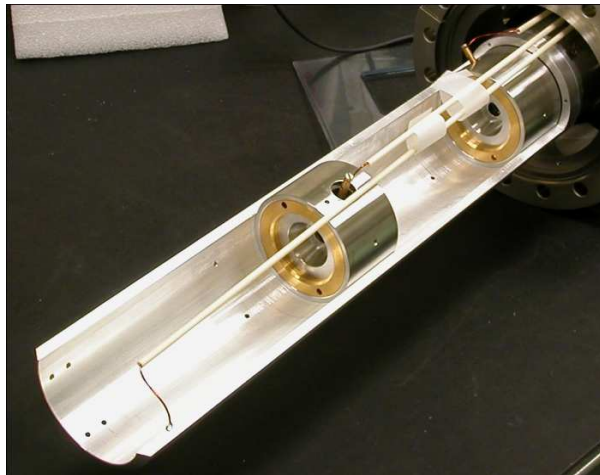
### **4.2.1      *Imaging electrons***

The field of electron emission microscopy is approximately 40 years old and has been reviewed by several authors, most recently by Griffith and Engel [49]. Emission microscopy in general is a direct imaging technique. In other words, the image is not formed by scanning a beam or sequential composition, but by collecting all the information from the electrons over the whole field of view and in real time, two features that are shared by IEEM.

Electron emission from surface can be induced in various ways: thermally, via excitation by photon irradiation or electron/ion bombardment or by field emission. Among the wide range of possibilities offered by the electron microscopy, Photon Electron Emission Microscopy (PEEM), which uses electrons extracted from UV photons to image the sample surface, is suitable to be used as off-the-shelf technology to implement Ion Electron Emission Microscopy. Therefore the imaging core of an IEEM is a commercial PEEM microscope (Figure 4.3).

A variety of contrast generating mechanisms contribute to distinguish surface features on a submicron scale. The small energy of the electrons used to form the image ( $\sim 1$  eV) accounts for the surface sensitivity of the PEEM: contrasting

techniques are used to study slight variations of electron energy due to surface features. Contrast techniques are not applicable for IEEM: the secondary electrons emitted by ion impact are more energetic electrons ( $\sim 5$  eV) and less sensitive to surface imperfections. Indeed the different purpose of IEEM is to provide a measurement of the impact position of an ion and to this end the SE average yield is the main consideration. In an IEEM experiment the ideal situation is obtained when the yield is high and constant across the sample for uniform ion detection.

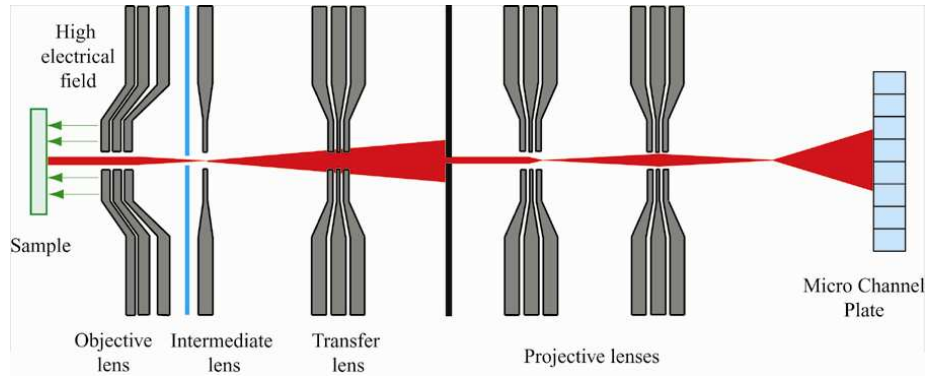


**Figure 4.4** The disassembled PEEM column; two electrostatic lenses are visible.

The electron optical column of the microscope is formed by several electrostatic elements shown in Figure 4.4: the objective lens, the zoom lens, two projective lenses and finally the X Y position sensitive detector (PSD).

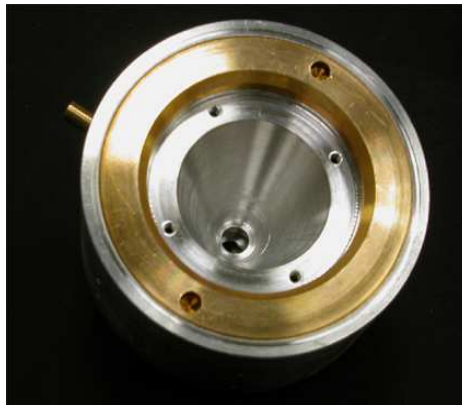
The magnification ranges from  $160\times$  to  $1600\times$  (when projector A is not used, the magnification increases to  $8000\times$ ) which corresponds to a field of view between  $250$  and  $25\ \mu\text{m}$ . The magnification is set by adjustments to the zoom lens, focusing is performed with the objective lens, and projector B is adjusted so that the field of view fills the PSD.

The sample surface itself is part of the objective lens. This lens is basically an immersion lens formed by four electrodes (a tetrode lens): the sample surface and a three electrode lens (Figure 4.5).



**Figure 4.5** Schematic diagram of the five PEEM lenses system and the diaphragms.

An accelerating field of the order of several kilovolts per millimeter is applied between the sample and the first element of the lens (transfer voltage). The field strength and its uniformity are a key figure to determine the best lateral resolution. Keeping the sample at ground or at least near ground potential simplifies handling and current measurements; however, it also requires that the whole column is at the transfer potential (up to 15 kV in our case) with the sample positioned at a distance of a few (3÷5) millimeters from the first lens element, allowing a maximum field strength of ~5 kV/mm.



**Figure 4.6** Internal view of the objective immersion lens of the PEEM.

The homogeneous electric field between the sample and the first lens electrode accelerates the electrons and forms a virtual image below the sample surface. The three electrode lens forms a magnified real image behind the objective lens.

The zoom and two projector lenses account for the final magnification on the image detector. An aperture in the source plane of the projector B limits the field of

view. This aperture is useful to limit the area of the sample where SEs are produced and also to protect other areas from ion induced damage (particularly important for testing semiconductor electronic circuits) but is not needed in many cases. The zoom lens is used to set the total magnification. Two imaging modes are accessible; a low magnification mode and a high magnification mode. High magnification mode means a high field strength in the zoom lens. In this mode, the objective lens forms a real magnified image in front of the zoom lens, which is further magnified onto the aperture of the projector lens B. Low magnification mode means a low field strength in the zoom lens. In this case, there is not a real but only a virtual intermediate image formed. Switching between the imaging modes accounts for a flip in the observed image.

A further lens (decelerating lens) with a separate power supply placed after the last projective lens can decelerate electrons down to  $\sim 1$  keV to optimize the performances of the electron amplifier (usually a Micro-Channel Plate, MCP) placed on the microscope focal plane. This lens can be excluded if required.

### 4.2.2 Resolution

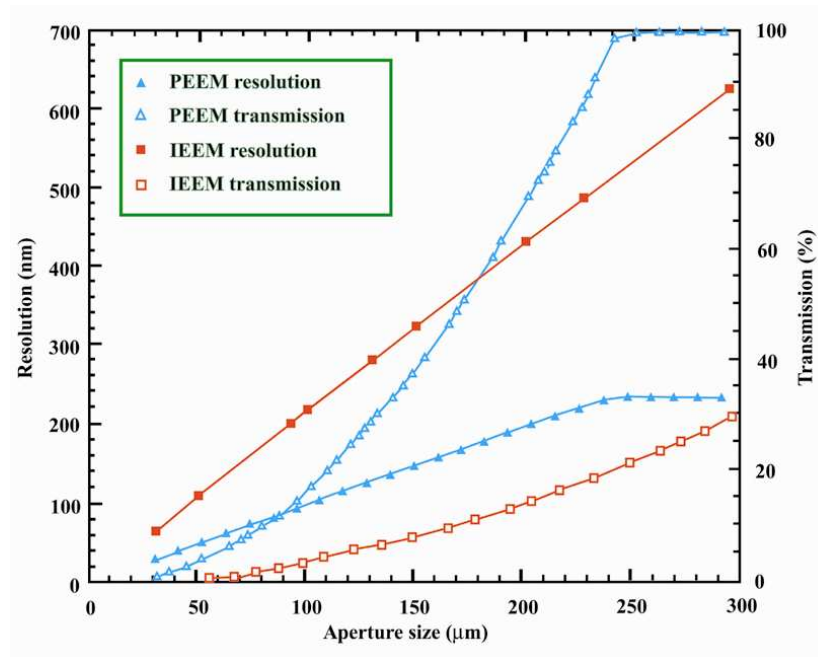
Like any other “optical” instruments, the PEEM microscope presents problems of distortion and aberration. Distortion causes an information modification (geometrical distortion), but not its complete and definitive loss or degradation: as information is only changed, a subsequent image analysis can restore it to its original appearance. On the contrary, aberrations lower the resolving power of the instrument and lead to an unrecoverable loss of spatial information.

An extracted secondary electron will enter the PEEM column with a starting angle to be transported to the focal plane. The spread in energy and emission angle of the secondary electrons will introduce aberrations; i.e. electrons following non-ideal trajectories will not be focused and the image will blur. Spherical aberrations will not occur along the optical axis of the system, while they increase when the starting angle of the electrons diverges respect to the optical axis. By using a high electric field strength at the surface most electrons will be transferred into the PEEM column, even those electrons emitted up to nearly  $90^\circ$ . On the other hand the energy spread of the secondary electrons leads to energy-dependent trajectories (chromatic

aberration). The easiest way to limit both spherical and chromatic aberrations is to put a diaphragm with an aperture that cuts electrons with improper trajectories. A small aperture will select small starting angles and small energies, but the transmission efficiency (the fraction of secondary electrons accepted by the PEEM) is reduced. A good lateral resolution can only be achieved with a small contrast aperture and a high extraction voltage.

The PEEM was designed and tested to work with electrons generated by UV photons, that exhibit a low energy mean value (1 eV) and a narrow energy distribution (1 eV FWHM); using a PEEM to image more energetic and less monochromatic electrons generated by ion impacts will affect the resolving power.

In order to get a quantitative estimation of the PEEM resolution when used as an IEEM, the Sandia team, in collaboration with the PEEM manufacturer, performed a ray-tracing calculation of the theoretical resolution (for chromatic aberrations only) and transmission efficiency versus aperture size [44].



**Figure 4.7** Efficiency and resolution as a function of the diameter of the aperture of the contrast diaphragm of the PEEM for both photon induced secondary electrons and high energy ion induced secondary electrons, assuming electron mean energies of 1eV and 5eV respectively.

For these calculations the energy distribution of secondary electrons at the sample was assumed to be peaked at 5 eV with a 5 eV FWHM and to be emitted with a

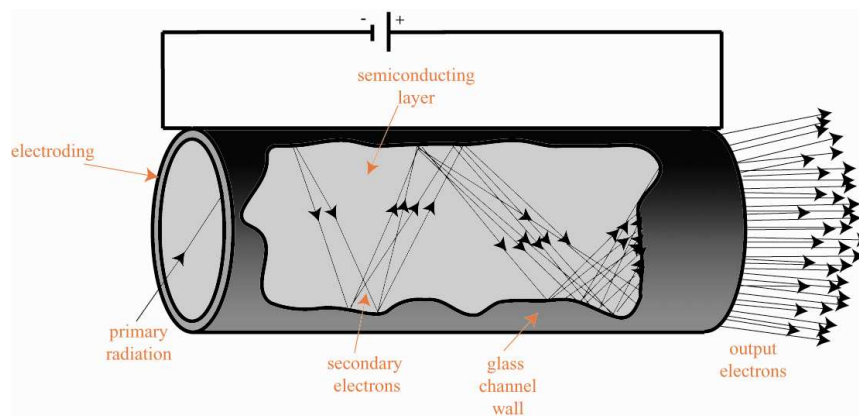
cosine angular distribution. With these assumptions the intrinsic resolution of the IEEM is  $\sim 500$  linear resolved points (lrp); i.e. it is possible to distinguish 500 equally spaced points lined up along the diameter of the field of view (FOV). Using the largest  $300\mu\text{m}$  aperture, to maximize electron transmission and hence ion detection, the IEEM resolution is  $\sim 0.6\mu\text{m}$  and the transmission efficiency is  $\sim 30\%$  (Figure 4.6). With the  $300\mu\text{m}$  aperture the PEEM is 100% efficient with a resolution of  $\sim 0.2\mu\text{m}$  (the intrinsic resolution of the PEEM is  $\sim 1500$  lrp). For the IEEM to achieve a  $0.2\mu\text{m}$  resolution would require a  $\sim 100\mu\text{m}$  aperture but the transmission efficiency would be only  $\sim 2\div 3\%$ .

### 4.2.3 Electron detector

For each ion impact, a number of electrons are emitted but only a fraction of them is transmitted by the microscope column. An electron multiplier is placed on the focal plane of the microscope to make a robust electronic signal. This detector must not degrade the intrinsic spatial resolution of PEEM and must have a refresh rate fast enough to sustain a useful rate of ion impacts in the microscope field of view.

The commonly chosen detector for this kind of application is a multi stack Microchannel plate (MCP). A microchannel plate is an array of miniature electron multipliers oriented parallel to one another. Typical channel diameters are in the range of  $5\text{-}100\mu\text{m}$  and have length to diameter ratios ( $\alpha$ ) between 40 and 100. Channels are typically normal to, or biased at a small angle ( $\sim 8^\circ$ ) to the MCP input surface. The channel matrix is usually fabricated from a lead glass, treated in such a way as to optimize the secondary emission characteristics of each channel and to render the channel walls semiconducting so as to allow charge replenishment from an external voltage source (Figure 4.7). Each microchannel is a continuous-dynode electron multiplier, in which the multiplication takes place under the presence of a strong electric field. A particle or photon that enters one of the channels through a small orifice is guaranteed to hit the wall of the channel due to the angle of impact. The impact starts a cascade of electrons that propagates through the channel, which amplifies the original signal by several orders of magnitude ( $10^4\text{-}10^7$ ) depending on the electric field strength and the geometry of the micro-channel plate. After the cascade, the microchannel takes time to recover (or recharge) before it can detect

another signal. MCPs show excellent time resolution ( $< 100\text{ps}$ ) and a spatial resolution limited only by the channel dimensions and spacing. Detection efficiency of a microchannel plate depends upon the type, energy and angle of incidence of the primary radiation and the first strike conversion of the microchannel plate. Under common operating conditions, the detection efficiency is limited by the open area ratio (channel area/ total plate area), since events striking the inter-channel area are not typically collected. The open area ratio for standard MCPs ranges between 55-85%.



**Figure 4.8** A channel electron multiplier.

The typical working voltage is  $\sim 1\text{kV}$ , corresponding to a gain of about  $10^4$ . Higher gains (up to  $10^9$ ) can be achieved by coupling two or more into stacks. In imaging applications it is usual to express the spatial (lateral) resolution of an instrument in line pairs per millimeters (lp/mm). For a single high resolution MCP the limiting resolution is 40 lp/mm; for a two stack (chevron) it is better than 25 lp/mm; for a three stack (Z-Stack) high gain assembly it drops to 16 lp/mm. Still higher gain solutions (5 plates stack) further drop the resolution performance. MCP sizes (the diameter of the circular active area) are standard, and the most common are 18 mm, 25 mm and 40 mm and the choice of the proper sensor size depends on the resolution requested by the specific application.

In paragraph 4.2.2 we expressed the resolving power of the IEEM in terms of lrp (the maximum number of distinguishable points lined up along the diameter of the field of view). When resolution is stated in lp/mm, the width of the line, i.e. the size of smallest resolvable feature, is equal to  $2 \times$  resolution expressed in lp/mm. As an example we consider a large diameter three stack MCP assembly. The resolution of a

such a detector is better than 16 line pairs (lp)/mm. For a detector with a diameter of 40 mm, this corresponds to a resolution better than  $(2 \times 16 \text{ lp/mm}) \times 40 \text{ mm} = 1280$  lrp across the diameter. Such a detector will not degrade the IEEM intrinsic resolving power ( $\sim 500$  lrp). It must be noticed that this is also true for a smaller MCP diameter of 25 mm which will have a resolution better than 800 lrp<sup>18</sup>.

For IEEM applications, an MCP is used in high gain (saturation) mode, i.e. the output signal strength is only weakly dependent on the number of incoming electrons. This feature is useful to discriminate real events against dark counts from thermally generated electrons (typically of the order of  $\sim 0.5$  cts/s·cm<sup>2</sup> and increasing with the gain factor). In fact, electrons thermally generated inside the chevron MCP have an output signal significantly weaker than real events. Of course, for electrons thermally generated near the input of the first stack, the discrimination will be nearly impossible, as their output signal will be comparable with the one from a real ion impact.

Saturation is also a desirable condition because it ensures a stable output, which does not depend too much on the statistic of secondary electron emission, their transport through PEEM column and the MCP amplification factor. This stable output makes easier the coupling with a Position Sensitive Detector (PSD) device.

The time resolution of an MCP is related to the avalanche evolution time, and is of the

order of few ns for a multi-plate stack. The avalanche electronic signal, thanks to its prompt response to events, should be hence the ideal candidate to provide (unless noise-pickup problems) a fast trigger signals.

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<sup>18</sup> However in UV-mode the intrinsic resolution of the PEEM is three times better than when used as an IEEM (see Figure 4.6) and the 25 mm diameter MCP assembly would be inadequate for PEEM applications.



## 4.3 *Ion Electron Emission Microscope at SIRAD*

### 4.3.1 **General description**

The Ion Electron Emission Microscope installed at SIRAD irradiation facility (see section. 4.5) uses to image electrons the same commercial PEEM from Staib [50] of the SANDIA team. The contrast diaphragm has 200  $\mu\text{m}$  of diameter, which set the transmission efficiency to 70% and the achievable resolution in PEEM operations to 0.4 nm.

The ion beam passes down through the MCP and along the microscope lenses (axial configuration) and strikes the sample orthogonally (Figure 4.8). The position detector of the SIRAD IEEM doesn't directly detect the electron avalanches at the output of the MCP output, but it detects flashes of light from a phosphor screen coupled directly to the output of the MCP. The avalanche electrons from the MCP, initiated by the secondary electrons from a single ion impact, excite a phosphor screen that emits a burst of photons [51]. These are reflected by a 45° mirror and extracted from the vacuum chamber through a quartz window and focused onto an external image intensifier. The regenerated light signal is finally focused onto a custom-made, digital, high rate and high resolution position sensitive detector which detects the photons and returns the x and y coordinate of the original ion impact. This sensing solution has been nicknamed STRIDE, which stands for Space & Time Resolving Imaging DEvice. The device is connected to the control PC via an USB connection and has no need of any further external hardware.

A remote controlled sample holder, with three degrees of freedom (three linear motorized stages (2.5 mm travel range) allows target positioning with a resolution of 0.01  $\mu\text{m}$  with a repositioning error better than 0.1  $\mu\text{m}$  [52] and is suited for high vacuum (down to  $1 \times 10^{-7}$  mbar).

The same computer controls the proprietary data acquisition system, the DC motor stage, the dosimetry software and the vacuum logger, without the need of other external electronic module.

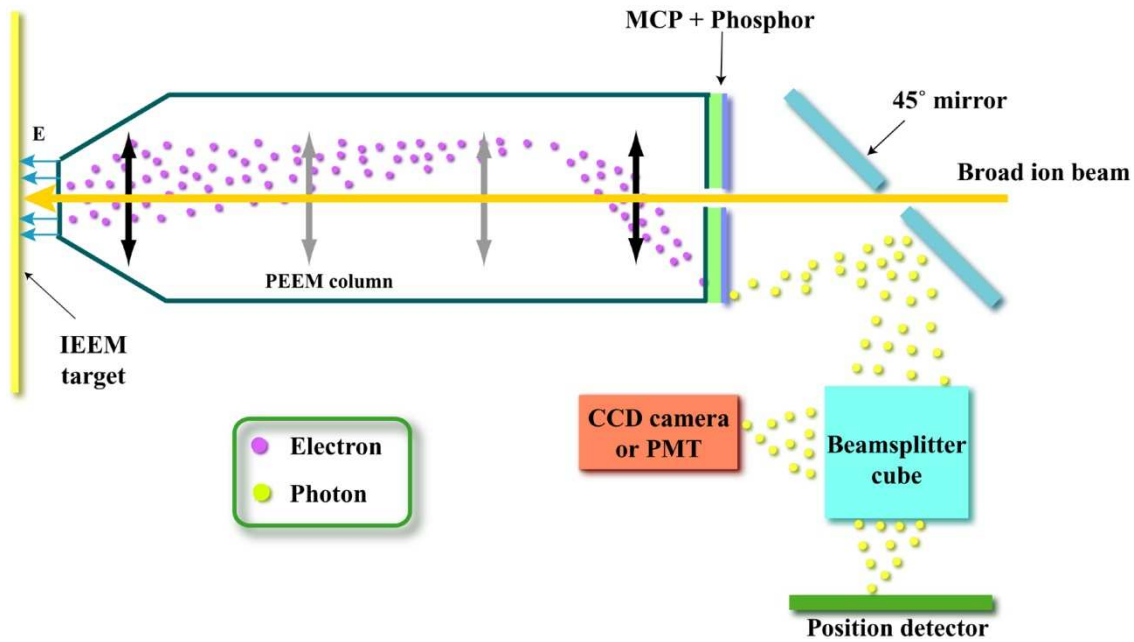
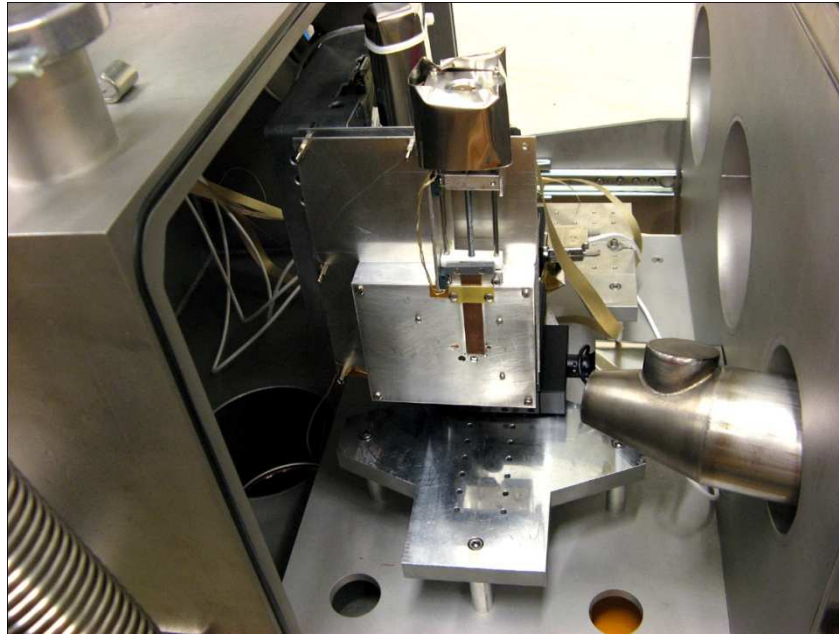


Figure 4.9 Schematic drawing of SIRAD IEEM setup.

### 4.3.2 The irradiation chamber

The irradiation chamber has a box-like shape and a whole side opens like a large drawer allowing easy access to the target, to the 3 axis sample holder and to ancillary electronics (if any). The entire sample holder and every item inside the chamber are mounted on the sliding floor of the drawer. Thus, by opening the chamber everything inside slides out completely from the chamber providing tabletop-like working conditions (Figure 4.9).

The relatively small volume of the chamber ( $70 \times 40 \times 50$  cm of dimensions) allows reaching the operational vacuum level ( $\sim 1 \times 10^{-6}$  mbar) in a reasonable amount of time. The chamber provides enough space to host ancillary electronics that might have to be kept as close as possible to the target DUT.



**Figure 4.10** View of a target mounted on the sample holder with linear DC motor stages inside the extracted drawer of SIRAD IEEM irradiation chamber.

Two DN160CF flanges with D-style multi-pin connectors (one with  $8 \times 15$  sub-D type feedthrough and one  $2 \times 50$  sub-D type feedthrough) allows a wide possibility of connections between the vacuum chamber and any external setup (DC motor controllers, beam diagnostic, sample DAQ, etc.) In case of need, it is possible to add flanges with special connections without changing anything in the setup by means of the user serviceable flanges (Figure 4.10).

Two flanges are oriented  $75^\circ$  respect to the PEEM axis and aim at the target plane. One of these hosts a quartz viewport for a UV lamp. Before the experiment, preliminary calibrations and tests are in fact performed using UV photons, to help alignment and fine focusing of the PEEM.

Two orthogonal pairs of Helmholtz coils outside the IEEM vacuum chamber, centered at the position of the DUT, are used to compensate stray magnetic fields that affect the collection of the secondary electrons and hence the formation of the IEEM image.

At present, the chamber is rigidly mounted on a fixed stand but isolated from the rest of the beam line. The turbo pump is mechanically decoupled by means of a vibration dumper.

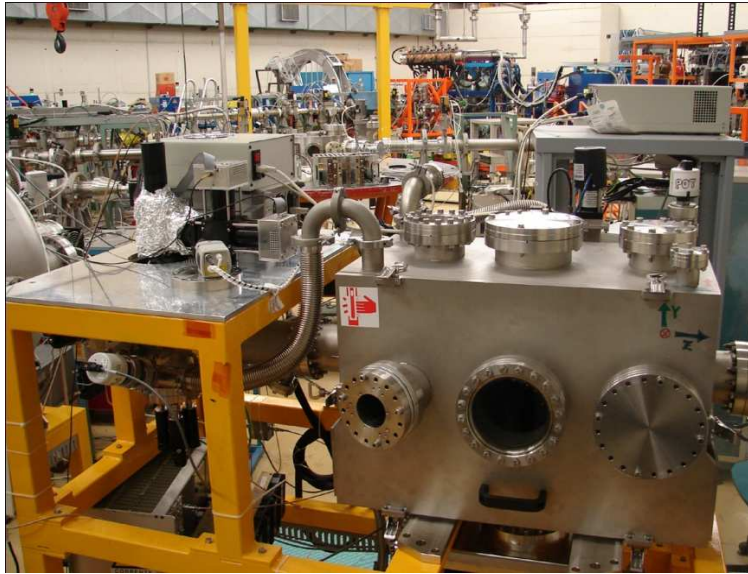


Figure 4.11 View of axial SIRAD IEEM chamber and setup in the experimental hall.

### 4.3.3 Fixed membrane configuration

As already stated, the surface of a typical electronic device is usually passivated and is an unreliable secondary electron emitter. In addition, devices to be irradiated might have complex surface features, which could introduce unacceptable perturbations on the electric field of the IEEM used to collect the secondary electrons. To both ensure copious secondary electron emission and strive for perfect electron collection, we use a Silicon Nitride ( $\text{Si}_3\text{N}_4$ ) ultra-thin membrane with a thin deposition of gold [53]. At first, the membrane window we used [54] [55] was 5 mm wide, 100 nm thick with a 40 nm gold layer deposition (Figure 4.11). Ions lose a negligible amount of energy in traversing it, so avoiding any significant energy degradation. The window presented a flat side, where the membrane is flush with the support frame (525  $\mu\text{m}$  thick, 10 mm wide), and a deep concave side. These membranes are very delicate and cannot be placed directly in contact with the DUT. As a consequence, the lateral resolution of the IEEM is degraded. For this reason, given its shape, we chose to deposit gold on the non-flat side of the membrane to minimize the lever-arm to the DUT.

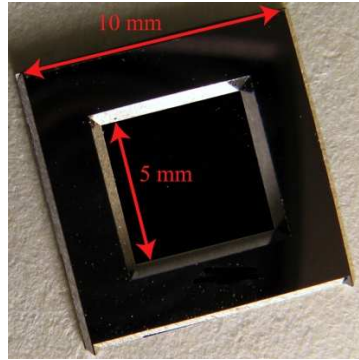


Figure 4.12 Silson golden  $\text{Si}_3\text{N}_4$  membrane 100 nm thick in a 10×10 mm frame.

The use of this configuration was problematic for several important reasons. First, these membranes were very wide and they bulged significantly in the electric field of the IEEM. As a consequence, the trajectories of the electrons were perturbed and the final image distorted. In addition, the concave shape of the support-frame of the membrane facing the IEEM distorted the electrical field that collects the secondary electrons IEEM (Figure 4.12 a).

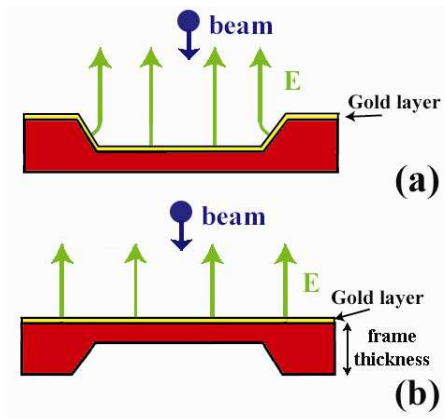
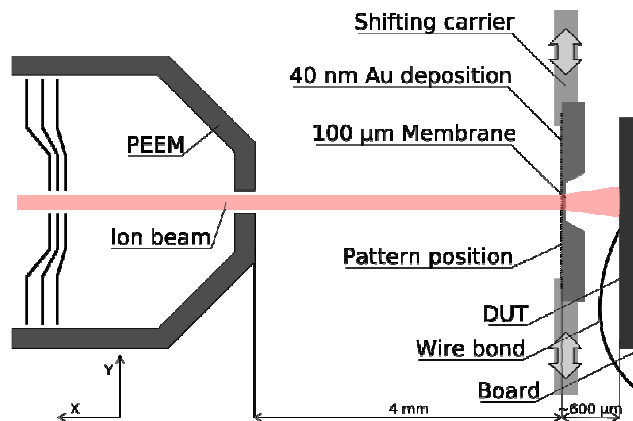


Figure 4.13 Membrane with the concave side towards the IEEM head; (b) membrane with the flat side towards the IEEM head.

The collection of the secondary electrons would be perfect for a flat membrane. To reduce membrane distortions in the electric field of the IEEM we now use a new  $500 \times 500 \mu\text{m}^2$  ultra-thin (100 nm) membrane window of  $\text{Si}_3\text{N}_4$  with a 30 nm deposition of gold on a 200  $\mu\text{m}$  thick Si window frame, mounted on a holder independent of the DUT position. To ensure the uniformity of the electric field of the microscope, used to collect the secondary electrons, the thick window frame is now

oriented towards the DUT so that the flat side is exposed to the IEEM (Figure 4.12 b).

Besides providing a reliable secondary electron emission, the membrane has also the great advantage of screening the DUT from the electric field and avoids destructive discharges. The already cited drawback is the unavoidable degradation of the lateral resolution of the IEEM. For a given ion species and energy, the resolution depends linearly on the distance of the DUT from the membrane because of the angular deflection from multiple scattering projected over said distance. The closest distance achievable with the current design is  $\sim 300 \mu\text{m}$ , mostly due to the thickness of the Si window frame.



**Figure 4.14** Actual configuration of the  $\text{Si}_3\text{N}_4$  membrane: independent of the position of the DUT (image not to scale). The carrier can shift along the Y axis allowing the microscope to image the pattern

The surface of the membrane is uniform and to focus the IEEM we now image a pattern on the frame surface near the membrane. The pattern is made of  $5 \mu\text{m}$  wide gold strips, deposited on the  $\text{Si}_3\text{N}_4$  surface, that cross to form a set of  $16 \times 16$  squares ( $25 \times 25 \mu\text{m}^2$ ). A frame holder can mount up to 3 window frames; a step motor is used to shift, with micrometric precision, the chosen window along the X-axis in front of the IEEM, to first focus the IEEM by imaging the pattern near a window, then to position the membrane. A quick way to focus the IEEM is to use UV lamp to extract photo-electrons. It is important to note that this can be done thanks to the presence of the membrane that effectively screens the DUT from the UV photons which can

otherwise charge-up and destroy it. In addition, by mounting the membrane in a fixed position in front of the IEEM the magnification and focus can be set once and for all, independently of the DUT, reducing the time needed for the irradiation arrangement (Figure 4.13).

## **4.4      *Photons production and detection***

### **4.4.1      Introduction**

We obtain the positions of the ion impacts by imaging light spots on the phosphor screen directly coupled to the MCP.

The output electrons of the MCP are accelerated across a small gap (~ 1mm) and locally excite a phosphor screen; each output electron avalanches is converted to a blue light spot. An optical assembly, consisting of a 45° mirror (with a central hole) and a system of lenses, collects the photons from the luminous spots and extracts them outside the irradiation chamber where they are detected by a photon position-sensitive detector. This is a simple and relatively inexpensive solution, but the main drawback is that only a small fraction of the photons are collected (low optical efficiency). To regenerate the light signal, for ease of detection, we use an external image intensifier, which amplifies the light signal by a factor  $10^6$ . The light signal strength is now suitable to be revealed by the final position detector.

For position sensing applications the choice of sensors is very wide, but only few solutions have been investigated. The natural approach seems to be CCD or CMOS arrays as they offer up to mega-pixel level resolutions (our minimal requirement of 500 points on the image diameter is not an issue at all!) and the ability to work with very low light levels. The main drawback of these arrays is the need to readout the entire array to determine if and where the light-spot arrived and hence the difficulty of sustaining data throughputs useful for SEE applications. A completely new digital position sensitive detector system was hence developed [56] [57], that provides the required high-rate and high-resolution performances. The system reduces the number of pixels to read and makes the digital approach feasible. It will be described in the following paragraph.

#### 4.4.2 Photons production, amplification and detection

A double stack MCP (40 mm large) with a central hole (8 mm diameter) has been chosen as the main electron detector. Working in saturation mode, this device ensures an amplification factor up to  $1 \times 10^7$   $e^-/e^-$ , with a dark count rate of  $\sim 0.5$  counts /s·cm<sup>2</sup>, corresponding to less than 7 counts/sec on the entire area.

The 40 mm diameter phosphor screen, coupled to the MCP, converts the out-coming electron clouds into luminous spots. Among the available types of phosphors, the P47 (Y<sub>2</sub>SiO<sub>5</sub>:Ce,Tb) has been chosen, because its peak emission is at 400 nm, it has a fast decay time (from 90% to 10%) shorter than 100 ns with a tail decay time (from 10% to 1%) of 2.9  $\mu$ s. The light signal is short enough to allow in the field of view of the IEEM ion impact rates well above those necessary for SEE applications.

The MCP focal plane detector we use ensures a resolution better than 25 lp/mm, equivalent to more than 2000 *lrp* over the 40 mm diameter. This is not degraded by the phosphor layer which, thanks to its micro-crystal structure, can give resolutions better than 100 lp/mm. A variable potential gap (0÷2 kV) between the second plate of the MCP and the phosphor screen accelerates the electrons to increase the phosphor conversion efficiency. The corresponding conversion yield for 2keV electrons is  $\sim 50$   $\gamma/e^-$ . This value refers to a single electron impinging on the screen, but when a cloud of particles (up to 10<sup>7</sup> in a double stack MCP) reaches the phosphor, saturation phenomena may occur. Dedicated measurements were performed to get an indicative value of this parameter ( $\gamma_{sat}$ ), as no specific data are present in literature [57]. Taking into account the area of the phosphor interested by the electron current ( $\sim 200$   $\mu$ m diameter) and the duration of the current itself (2÷4 ns FWHM), the order of magnitude of the maximum outgoing number of photons for a single incoming electron can be expressed as:

$$(4.4) \quad \gamma_{yield} = \gamma_{sat} \cdot area \cdot time = \frac{100\gamma}{\mu m^2 ns} (\pi \cdot 100^2) \mu m^2 \cdot 3ns \approx 10^7 \gamma$$

The light signal must be carried out of the vacuum chamber and focused onto the PSD system. A low-distortion system of lenses has been design to perform this task. Taking into account the transmission efficiency of this system (1%), the reflectance



efficiency (95%) and the hole geometrical factor (6 mm diameter) of the 45° mirror to bend the photons, the final global optical transmission efficiency is reduced to  $\cong 1\%$ , corresponding to  $10^5\gamma$ . Given this very low value, the corresponding expected signal for 400 nm photons in a solid state detector is  $< 10fC$ , which is one order of magnitude smaller than ENC of a typical pixel detector. We solved this problem by adding an image intensifier, a device that amplifies the light signal to be detected by the final sensor.

An image intensifier is a *plug-and-play* device that is composed by a photocathode, an internal MCP and a phosphor screen, all items being enclosed in an air-tight case. The image intensifier we use has a 2-stack MCP and a P47 phosphor screen [58]. However it has a 25 mm diameter and therefore the resolving power is  $25 \text{ lp/mm} \times 25 \text{ mm} = 625 \text{ lp} = 1250 \text{ lrp}$ . It meets the time and spatial resolution requirements for the whole system. Considering the number of photons arriving on the photocathode ( $10^5\gamma$ ), the photocathode efficiency at 400nm (30%), the maximum gain ( $10^6 \text{ e}^-/\text{e}^-$ ), the acceptance factor (55%), the phosphor yield ( $50 \gamma/\text{e}^-$  for the P47) and saturation effects, the expected number of out-coming photons is:

$$(4.5) \quad \gamma_{II} \approx 10^{10} \gamma.$$

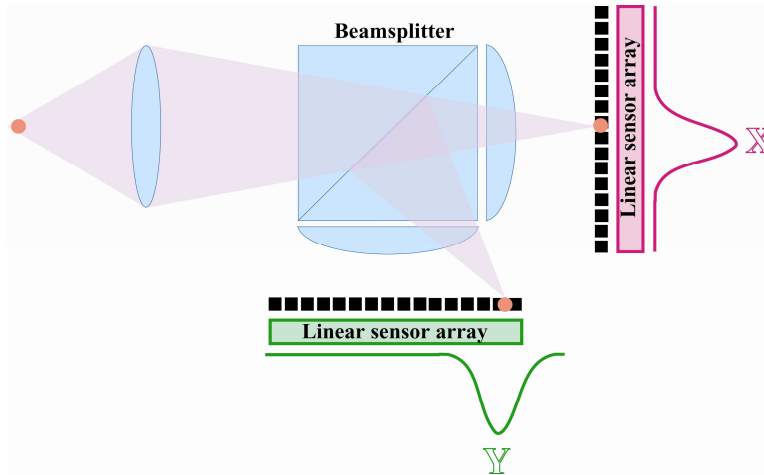
This is to be considered the maximum photon yield that it is possible to obtain from a single electron impinging on the MCP placed at the focal plane of the PEEM.

To couple the image intensifier output with the final position sensor, additional optics is needed. The efficiency of this optics is of the order of few percent. Considering the maximum photon yield (4.4), the lenses efficiency ( $\sim 2\%$ ) and the detector sensitivity (15%), the light level on the silicon sensor can be estimated to be

$$(4.6) \quad 10^{10} \gamma \cdot 4.97 \times 10^{-7} \text{ pJ} \cdot 0.02 \cdot 0.15 \approx 15 \text{ pC}.$$

The last step to get a working system is to provide a fast, efficient, high-resolution and low-noise position sensitive detector. As anticipated in paragraph 4.4.1, a tailored 2-D detector (STRIDE), has been developed to match IEEM requirements. In the present paragraph, I will give a brief review of the STRIDE; for a deeper and detailed description, I refer the reader to PhD thesis work of P. Giubilato [57].

The approach we adopted projects the light spot onto two orthogonal linear arrays (as sketched in Figure 4.13). The number of pixels to be readout is  $N$  (the two linear arrays are read out in parallel) rather than to  $N^2$  for a square array, while the spatial resolution remains unaffected. A position of the peak in one linear array will indicate the coordinate, along the direction of the linear array, of the light spot.



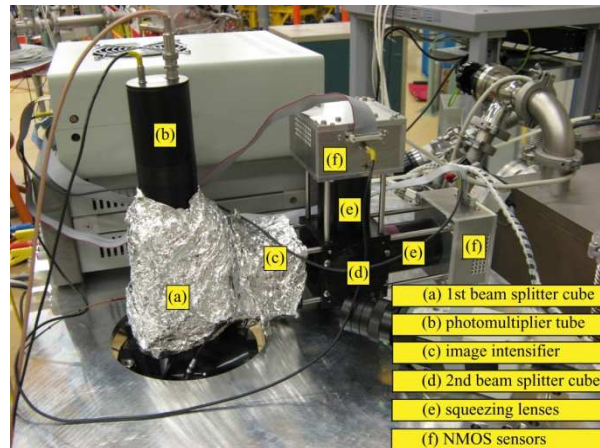
**Figure 4.15** Schematic drawing of the IEEM bilinear sensor.

The two projections of the light signal are obtained by an optical system consisting in a beamsplitter, that splits the original light spot into two copies, and cylindrical lenses, placed along the two orthogonal optical paths, that squeeze each light spot into a blade shape (Figure 4.13 and Figure 4.14). The two orthogonal light blades are then detected by an NMOS linear array [59], chosen for its ease of use and pixel shape ( $2.5\text{mm} \times 50\mu\text{m}$ ). The pixels are very wide and this maximizes the collection of the photons in the light blade, important when working in these low-light level conditions. The main drawback of the chosen sensor is its very low speed readout rate (2 MHz). In the present prototype, the device is overclocked to 3.125 MHz, resulting in a frame rate of  $3.125 \times 10^6 / 256 \sim 12.2\text{kframe/s}$ .

Proprietary electronics has been developed to both drive and read the two linear sensors. Two fast (40MHz) 12 bits ADCs (one per axis) convert the analog signal read from the sensor into digital format. Digitized data incoming from the ADCs are processed in parallel by an FPGA-based system, loaded with proprietary firmware. The position of the light spot is detected and fitted. When an event has been identified, a packet of 8 bytes is sent to the control PC via a USB connection. The event reconstruction (i.e. the peaks matching) is implemented at software level. The

analysis package also allows one to deal with multiple events per frame by watching the height of the registered peaks and matching peaks of equal eight.

Bench measurements for estimating the spatial performance shows that, everywhere in the useful area of the sensor, the resolution is better than 650 *lrp* (better than 1000 *lrp* over 70% of the useful area), with a distortion (a systematic error that can be corrected) under 1%.



**Figure 4.16** The bilinear detector system. The optical signal is reflected upwards by a mirror and out a viewport into a first beam splitter (a). Part of the signal is detected by a PMT (b), the rest is reflected horizontally, regenerated by an image intensifier(c) and sent to a 2nd beam splitter (d). Each copy of the image is squeezed (e) and detected by a linear NMOS array (f).

## 4.5 *PEEM imaging capability*

### 4.5.1 The calibration target

With the experimental setup previously described, we tried to quantify the performances of our microscope when working in PEEM mode. In the present section I will report on a resolution measurement performed on our IEEM when exposed to UV photon irradiation.

To measure the performances of our present setup in terms of spatial resolution, we imaged a tailored target (Figure 4.15) used for Photon Electron Emission Microscope calibration [60]. This target consists of a Silicon substrate (10 mm × 10 mm), with a gold pattern deposited. The pattern consists of metalized strips 10 $\mu$ m

wide, separated by unmetallized regions, with widths increasing across the pattern in steps of  $0.2 \mu\text{m}$  from a minimum of  $0.2 \mu\text{m}$  to a maximum of  $5 \mu\text{m}$ . The metallization layer is 35 nm Au film over 5nm Ti adhesion promoting film.

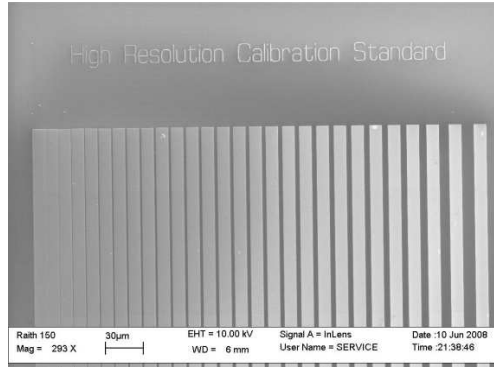


Figure 4.17 High Resolution pattern from Applied Nanotools.

We illuminated directly the target with UV photons, for which the expected resolution is 200 nm [44]. The image reconstructed by the IEEM is shown in Figure 4.17.

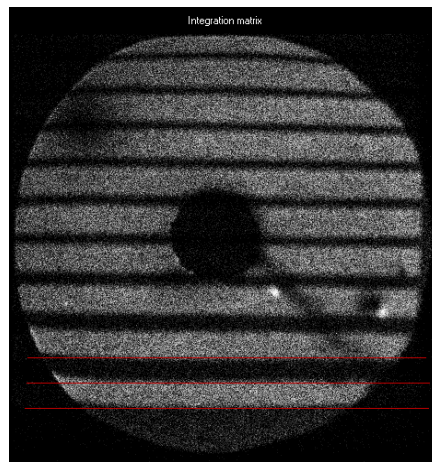


Figure 4.18 UV-induced image of the calibration pattern, reconstructed by the IEEM system.

To get from this qualitative picture a quantitative estimate of the PEEM spatial resolution, we used the Edge Spread Function (ESF), which describes how a system responds to a sharp straight discontinuity (i. e. to an edge). The analysis was performed using data inside different rectangular regions like the black rectangular region shown in Figure 4.18-a. To this end, we built histograms with the Y-

coordinates of the data inside said regions and studied the shape of the edge; the way the data falls from a high values in bright, emitting regions (Au strips), to low values from non-emitting Si-regions. The edge projection was fitted with the Error Function (*erf*), a special function of sigmoid shape, defined as:

$$(4.7) \quad p_0 + p_2 \operatorname{erf}\left(\frac{p_1 - x}{p_3}\right) = p_0 + p_2 \cdot \frac{2}{\sqrt{\pi}} \int_0^x e^{-\left(\frac{p_1 - y}{p_3}\right)^2} dy$$

The *erf*, which is twice the integral of a Gaussian distribution of mean  $p_1$  and variance  $\sigma = p_3/\sqrt{2}$ , models the shape of the measured edge: the deviation from an ideal (infinitely sharp) edge is characterized by the  $\sigma$  and the position of the edge is  $p_1$ .

An edge in the chosen rectangular region was fitted with an *erfc* and the  $p_3$  parameter was determined (see Figure 4.18). The  $\sigma$  value may be taken as the estimate of the present PEEM resolution ( $\text{RES}_{\text{PEEM}}$ ). The resulting  $\text{RES}_{\text{PEEM}} = 1.3 \pm 0.2 \mu\text{m}$  which is significantly worse than the theoretical value [44]. The error we quote for  $\text{RES}_{\text{PEEM}}$  was evaluated by considering data from different rectangular areas.

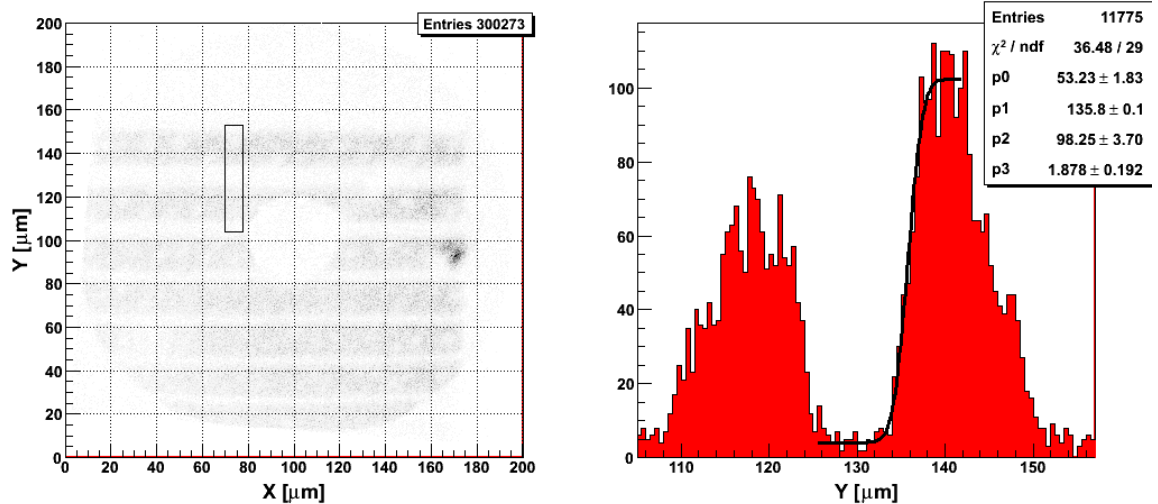


Figure 4.19 (a) PEEM Image of the widest strips of reference target. (b) Histogram of the the Y-coordinates of the PEEM events inside the black rectangle shown in (a) with an erf fit (see text).



## 5 A resolution measurement of the IEEM using a SDRAM

### *5.1 Introduction*

As for every imaging device, a figure of merit of the IEEM system is the resolution: here the ability to reveal the smallest details in the sensitivity map of an integrated circuit. To measure the resolution we need a reference target, to be able to precisely locate the impact position of every single ion independently by that measured by the IEEM. In addition we need a high statistics measurement. In practice we are looking for a device with a resolution not worse than that of the IEEM, with a sensitive area that fills the field of view of the IEEM, that is able to withstand an intense fluence of heavy ions (several ions/ $\mu\text{m}^2$ ) and that can be readout with a speed comparable with the one of the IEEM ( $\sim 1000$  ions/s).

We identified as suitable for this purpose a memory chip, a Synchronous Dynamic Random Access Memory (SDRAM) of the kind routinely used in computers: a 256 Mb Micron Technology high speed CMOS SDRAM, (chip model MT48LC32M8A2-7E B).

Other commercially available pixel devices were briefly considered. Charge Coupled Device arrays are not suitable, as individual pixels would be irreparably damaged (stuck) by single heavy ion impacts. Flash memories are more robust, but the information needed to reconstruct the location of the ion impact in the array is reserved (typically not available), and it was not possible to reconstruct this information experimentally with a method similar to that applied to the SDRAM.

When an ion impacts the SDRAM, it generates electron-hole pairs which diffuse in the silicon substrate. The cells near the ion trajectory can collect enough charge to undergo a bit upset, changing the value of their stored data. However the SDRAM

directly provides the logical address of each cell, not its coordinates. A remapping operation is required to associate to a logical address the corresponding coordinates. The location of the centroid cluster of flipped-bit cells is then determined and it is assumed to be the position of the ion impact.

To understand how we use the SDRAM it is necessary to describe how it works. We will describe the mapping and then the experimental characterization of the IEEM in terms of resolution and image distortions, using a high statistics data set obtained in a heavy ion experiment.

## **5.2      *The SDRAM system***

The SDRAM chip is glued to an electronic board, electrically connected to it by means of wire bonds that provide the power supply and the driving signals. The SDRAM board is then connected to a Virtex-5 LX evaluation board (Avnet). The Virtex-5 FPGA hosts the firmware that drives the SDRAM and the communication with the control PC.

In order that the SDRAM based test system match the mechanical constraints imposed by the IEEM environment, a custom Test Board (TB) has been implemented. To obtain maximum readout speed using the advanced input-output features of the SDRAM (burst mode, self refresh, etc.), the TB is based on Virtex 5, a high performance Field Programmable Gate Array (FPGA) (see fig. 8.2). The communication between the TB and the Test Control PC is obtained by a USB connection.

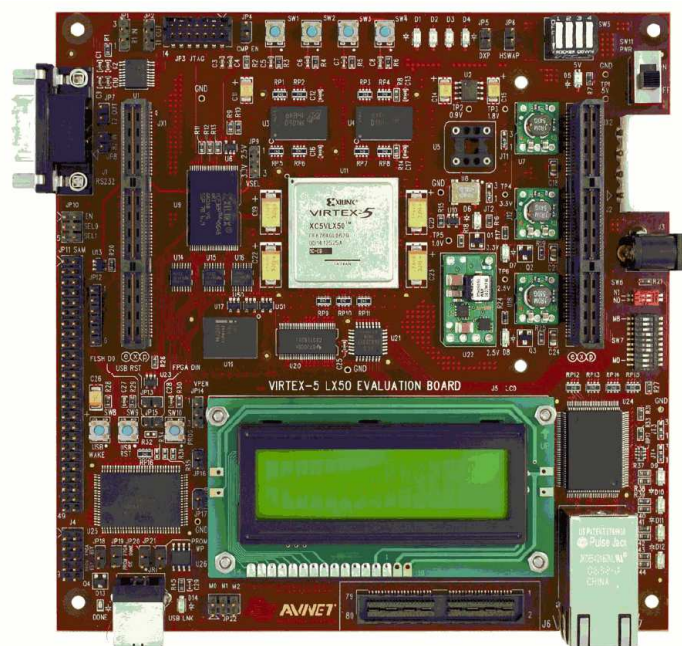
The time information is provided to the SDRAM system by STRIDE through a flat cable connection. The synchronization of the two systems is done the following way: the SDRAM system is first initialized and put into an acquisition state (ready); the STRIDE system, when started, sends a digital signal every 106  $\mu$ s, the time needed to complete the readout of the NMOS array sensors. Actually the time resolution of the STRIDE system is given by the 2.5 MHz clock that controls the read-out: the pixel is readout at every rising edge of the control clock and immediately refreshed. The readout of the NMOS sensor requires 265 control clock signals (one for each of the 256 pixels, plus 9 clock signals to reinitialize the sequence), that corresponds to 106  $\mu$ s. This time interval is the time resolution of the



SDRAM system. This signal feeds a FrameNumber counter that counts the number of frames that have been read from the beginning of the STRIDE acquisition.

The system core mapped in the FPGA is able to:

- address each cell;
- perform read and write operations;
- refresh the cells (normally every 64 ms) .



**Figure 5.1** Avnet demo board, hosting a Virtex 5 FPGA. The LCD display and the rubber keys were removed to avoid out-gassing in the vacuum chamber.

Beside these basic operations, the FPGA-based system performs complex test procedures as:

- writes an internally generated pattern on blocks of adjacent cells (the boundaries of this block is user defined through the control PC);
- reads the previously written block of cells;
- detects the presence of upsets;
- saves the logical address of the upset cell and its readout time and sends this information to the control PC.

In an ion beam experiment, the preliminary step is to identify the small region of the SDRAM that is actually exposed to the ion beam (200  $\mu\text{m}$  diameter area defined by the contrast diaphragm of the IEEM). This is done using the ion beam and by reading out the whole SDRAM: the high density of upsets immediately reveals the position of the exposed area. We then restrict the search of upsets to the cells in the row and column intervals that circumscribe the irradiated area and, at this point, the actual experiment may begin. The SDRAM system continuously reads the contents of the SDRAM cells in the selected address interval, looking for unexpected logic values.

### 5.3 SDRAM output file

Every time the system detects an upset, the row and column logical addresses of the upset, the value of the flipped bit, and the FrameNumber in which the upset occurred are save and sent to the control-PC via the USB connection. The computer generates an ASCII-format file in which every line is the record of the upset information mentioned above. An example of a portion of this ASCII-file is shown hereafter:

Bank	Row	Col	Data	FrameNumber
3	719	109	0	15344
3	890	98	8	15367
3	-890	98	8	15367
3	-890	99	8	15367
3	-890	99	8	15367
3	-890	99	8	15367
...				

The size of such files can be some millions of entries.

Every entry is made up of five values:

- *Bank*: indicates the bank number of the upset cell. The 2<sup>nd</sup> and 4<sup>th</sup> banks are never used because they covered by the wire bonds. The only banks we read are 1 and 3;
- *Row*: the raw address of the upset cell;

- *Column*: the column address of the upset cell;
- *Data*: the logic value associated to the read address;
- *FrameNumber*: is the number of the frame in which the upset was detected (not to be confused with the timestamp of STRIDE which is the number of clocks from the beginning of the acquisition).

The analysis code was written in C/C++, using the CERN Root framework [62], and a custom function library developed by P. Giubilato and D. Contarato.

To increase the speed of execution of the analysis code, ROOT *ntuples* are used: structures of entries made up of numerical values, fast to access and smaller than the original text files of data.

Since the SDRAM is read several times before being emptied, every upset has a chance to be read more than once. This is avoided by discarding all the repetitions of an entry if it reoccurs within 100 lines. This simple algorithm would reject good data if a given cell experiences upsets due to different ion hits occurring within a time interval of some milliseconds, but the ion flux in the field of view of the IEEM in our experiments is low enough (maximum flux  $\sim 1000$  ion hits/s  $\sim 3 \times 10^6$  cm<sup>-2</sup> s<sup>-1</sup>) that the probability that this happen is negligible.

## 5.4 Mapping the SDRAM with a laser

To use the SDRAM chip as a position detector, we need to know the correspondence between the address of a memory cell and its physical location in the chip. Unfortunately, this information is not made available by the manufacturer. The only information in our hands is that the array of cells of the SDRAM is internally organized in 4 banks, each one made up of 8,912 row by 1,024 column logical addresses of 8 bits, the word length used by our memory. Each bank is physically partitioned into 4 quadrants (Figure 5.4): the 8 bit long words are broken into 4 pairs of bits:  $\{\{b_0, b_1\}, \{b_2, b_3\}, \{b_4, b_5\}, \{b_6, b_7\}\}$  (Figure 5.4); every pair is stored in a different quadrant of the same bank:  $\{b_0, b_1\}$  and  $\{b_2, b_3\}$  share the same physical columns (*bit-lines*) and so the couple  $\{b_4, b_5\}$  and  $\{b_6, b_7\}$ ; the two bits forming a

couple are stored in adjacent cells in the same row (*wordline*). The left and right quadrants are identical (translational symmetry), while the upper and lower ones are inverted copies of one another (reflection symmetry).

To associate logical addresses to coordinates we implemented a system based on an infrared laser that illuminates the chip in a small spot, the position of which is controlled with a precision motorized stage (Figure 5.2).

The laser emits infrared radiation with a wavelength of 1060 nm: at this frequency the Silicon absorption coefficient is quite low and the radiation crosses the whole device. The radiation of the laser is guided to the front side of the device, where the microelectronic circuit is implanted, using the thinnest available optical fiber (5  $\mu\text{m}$ ), without using any focusing optics. The high density spot we obtain is about 10  $\mu\text{m}$  across. The spot intensity is high enough to generate a local density of electron-holes pairs capable of inducing Upsets in a small number of memory cells and thereby simulate the action of an ion impact. However the time needed to provide such a high charge density exceeds the 64 ms recommended refresh time.

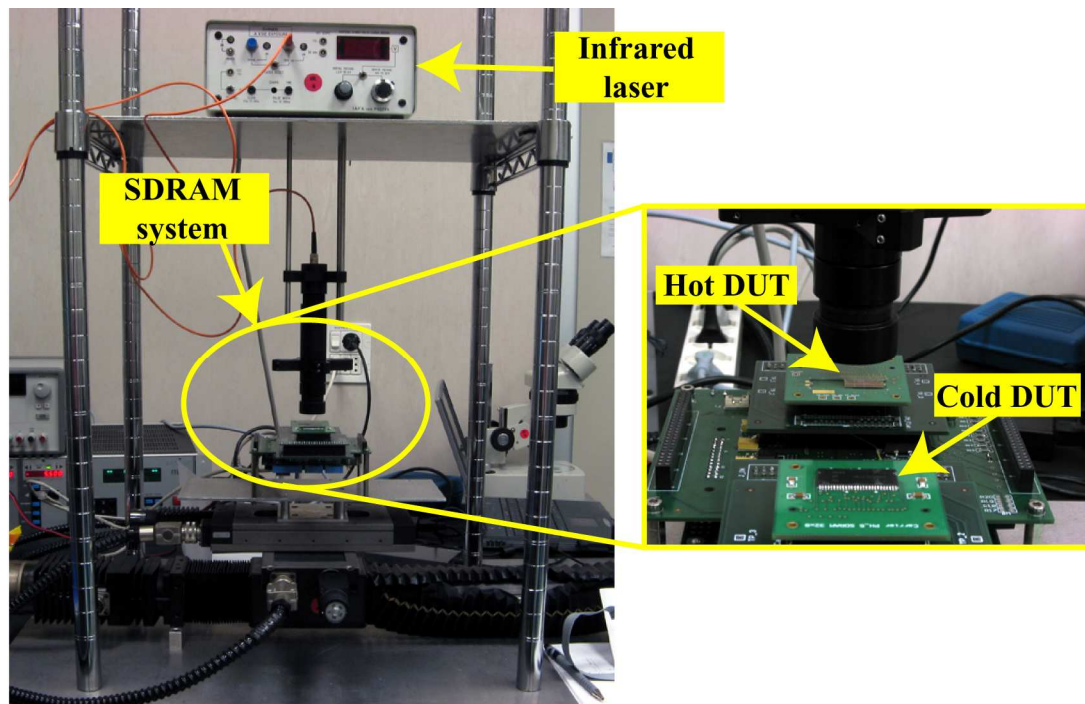


Figure 5.2 Setup for laser-based system for SDRAM mapping.

Since in our system we can set any refresh time and even suppress the refresh feature, we based our experiment on the Bit Retention Time (BRT). For a single memory cell, the BRT is the time the information is retained before it is lost due to

the unavoidable charge leakage<sup>19</sup>. Once the memory refresh is inhibited, the cells gradually lose their information, each cell with its own BRT (according to some distribution). The effect of the laser is to significantly shorten the BRT of the cells illuminated by the beam spot.

The experiment was performed by comparing the output of two identical memories: one DUT was exposed to the laser spot (*hot DUT*); the other DUT was not exposed (*cold DUT*). After a precise positioning of the hot chip with respect to the optical fiber, the two twin memories were filled with a common logical value: '0000 0000'. The laser irradiation was applied for some seconds, before reading the memories and comparing their outputs. The spatially contiguous cells illuminated by the laser spot were observed as Upsets with consecutive addresses (a cluster).

The experiment was performed by comparing the output of two identical memories: one DUT was exposed to the laser spot (*hot DUT*); the other DUT was not exposed (*cold DUT*). After a precise positioning of the hot chip with respect to the optical fiber, the two twin memories were filled with a common logical value: '0000 0000'. The laser irradiation was applied for some seconds, before reading the memories and comparing their outputs. The spatially contiguous cells illuminated by the laser spot were observed as Upsets with consecutive addresses (a cluster).

In the areas located in the first half of each sector of the SDRAM (from row 0 to row 255), the reconstructed map revealed the alternate presence of a pair of rows sensitive to upsets, followed by a pair of insensitive rows. When we repeated the measurement loading the memories with a logic pattern '1111 1111', we observed the previously flipping cells now insensitive to the radiation, while the previously insensitive cells underwent now to bit flips. Even though we do not know the detail of the memory technology, we suppose that charged storage capacitors may be discharged by the high density of free carriers generated by the ionizing radiation and define *positive logic* the one in which a charged capacitor corresponds to a '1' logic-state and a discharged capacitor corresponds to a '0' logic-state. We then can say that, in these regions of the SDRAM, two consecutive rows are implemented in

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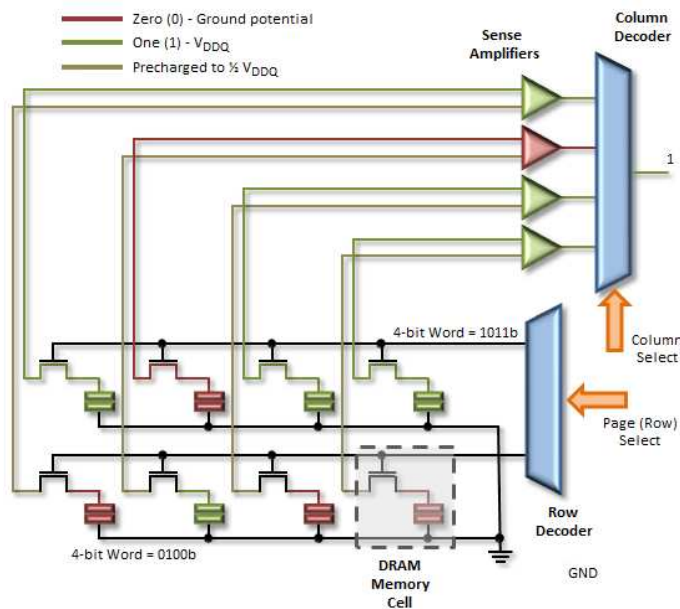
<sup>19</sup> To avoid losing any information, the SDRAM must be refreshed at time intervals inferior to the BRT of the worst memory cell. The typical refresh time interval given by the manufacturer (64 ms) ensures that no cell will lose information before the next refresh.

positive logic, while the following two rows are implemented by negative logic. The rest of each sector does not show this effect and we can assume that it is implemented in negative logic (one in which a '0', implemented as a charged capacitor, may undergo a flip).

### 5.5 The SDRAM remapping

The laser experiment revealed that SDRAM implements a folded bit-line architecture, as depicted in Figure 5.3.

Figure 5.5 represents the lower-half of quadrant 4: the sense amplifiers are placed along the top; the memory array is subdivided into 12-by-16 subarrays (segments). The surface of the SDRAM is not uniformly SEU-sensitive because the cells are located exclusively inside the segments. Under visual inspection (optical microscope) the segments appear as rectangles covered by equally spaced metallization lines parallel to the vertical direction of the Columns (Figure 5.6), while the cells are not visible



**Figure 5.3** Folded bit-line architecture implemented our SDRAM: each sense amplifier is connected to two parallel bit lines.

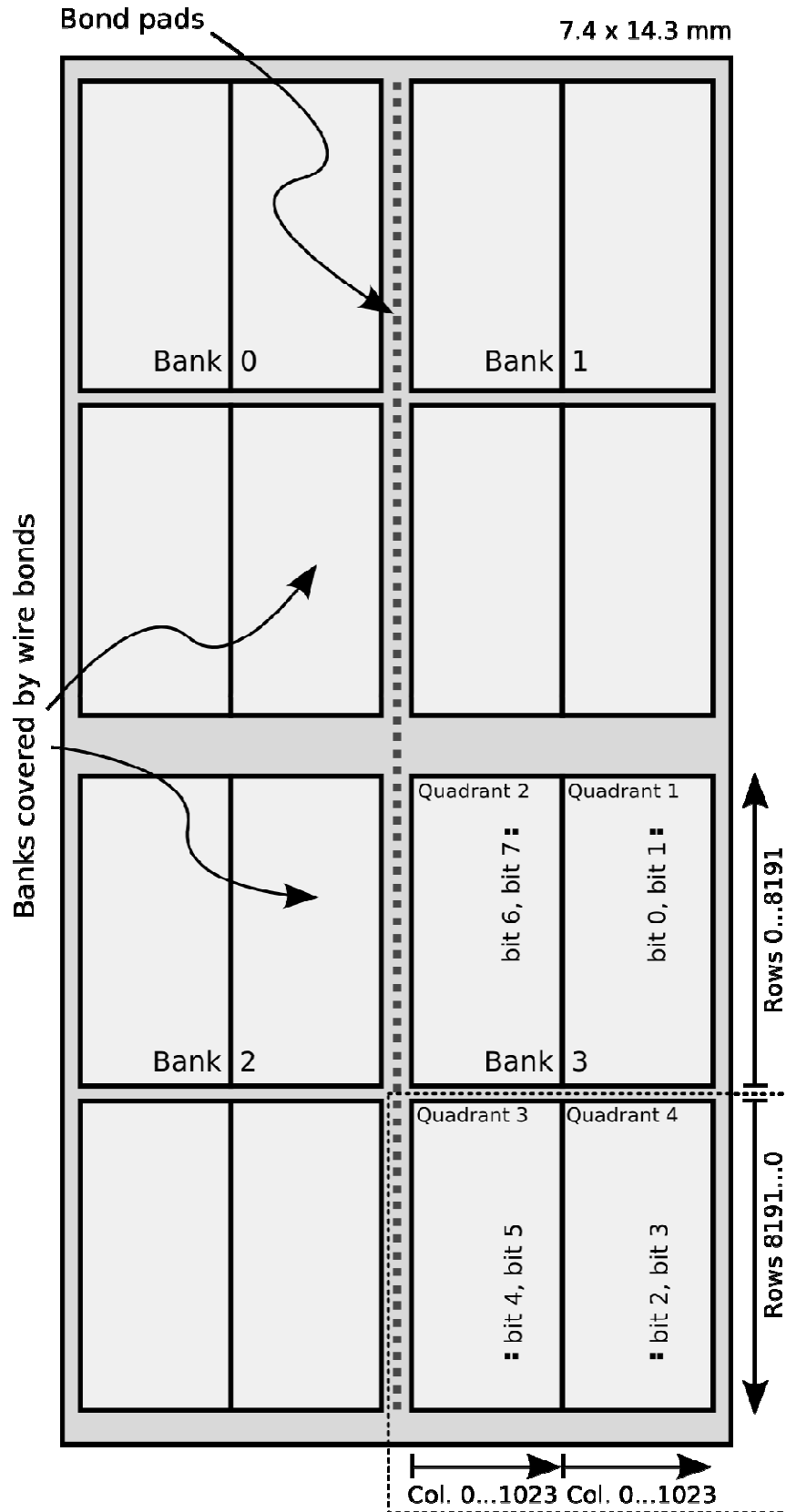


Figure 5.4 The SDRAM chip layout. Chip size is 7.4 x 14.3 mm. The area in the dashed rectangle is shown in detail in the following figure.

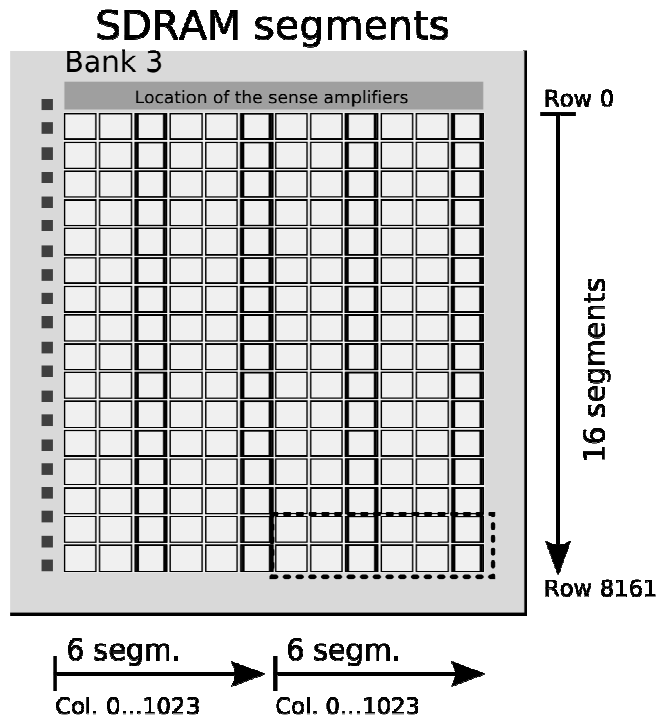


Figure 5.5 SDRAM layout, detail of the dashed rectangle in the previous figure. The cells Rows and Columns are organized in 12 x 16 segments. The area in the dashed rectangle is shown in detail in the following figure.

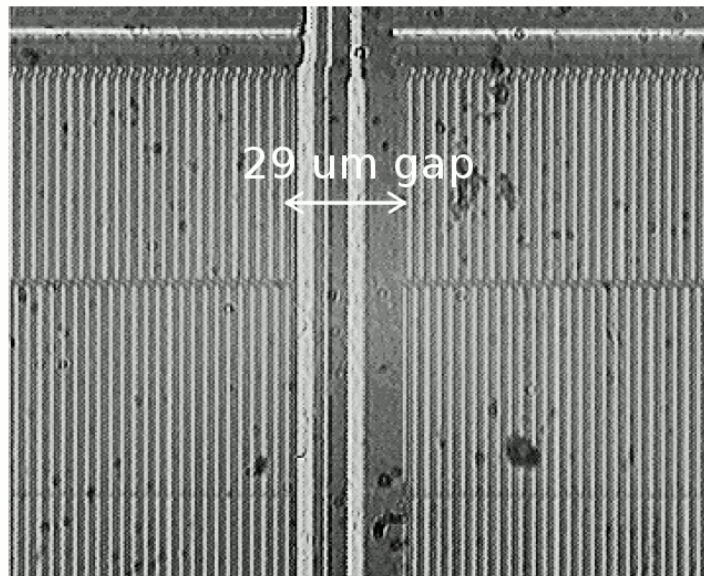


Figure 5.6 Microphotograph of one detail of the SDRAM (the field of view is 165 by 135  $\mu\text{m}$ ): the picture shows the corners of two SDRAM segments and the 29  $\mu\text{m}$  gap between them.



Most of the 12-by-16 segments have 86 lines (corresponding to 168 cells columns), with the exception of the segments highlighted in Figure 5.7 (segment-columns 3, 6, 9 and 12) which are a little bit larger and have 87 metallization lines (corresponding to 176 cells columns). The horizontal and vertical gaps between the segments are all 29  $\mu\text{m}$  wide.

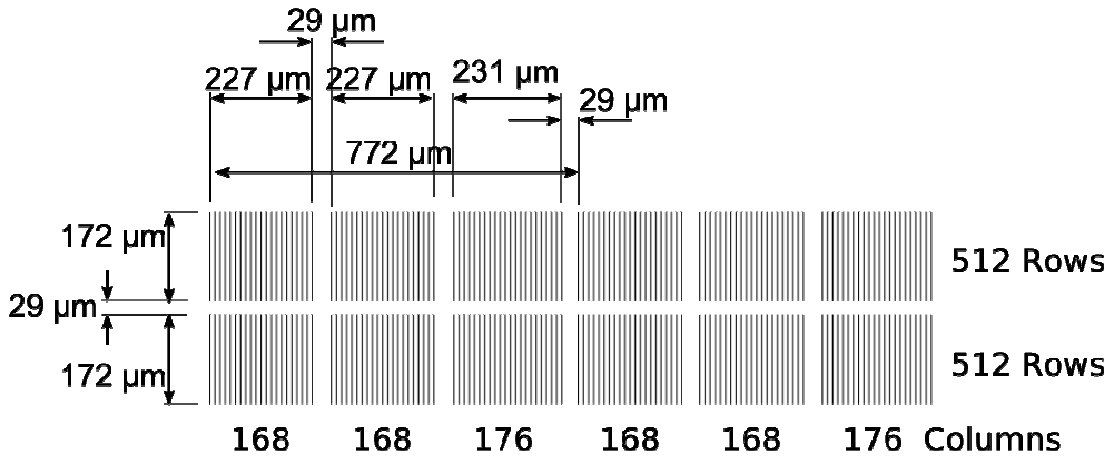


Figure 5.7 Detail of the SDRAM cells segments size and organization.

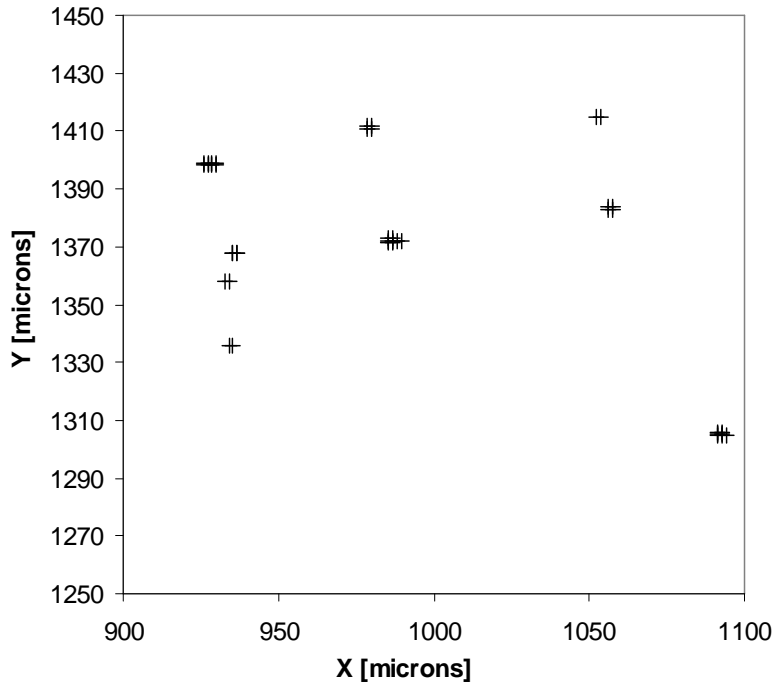
By dividing the 172  $\mu\text{m}$  high segments by 256 rows, we obtain a row pitch of 0.336  $\mu\text{m}$ , which is assumed to be the same in all segments. In the 168 columns wide segments, the column pitch is 1.31  $\mu\text{m}$ , while in the 176 columns segments, it's a little different: 1.35  $\mu\text{m}$ .

The laser experiment revealed that the sensitive area of the SDRAM coincides with the region below the metallization strips, but as the cells are not visible under the optical microscope, we have to make an assumption on their position inside the segment. The most reasonable assumption is that the Rows and Columns be straight, each equally spaced and orthogonal, with the Column direction parallel with the metallization lines observed in the segments and with the cells located at the intersection points of the bit-lines and word-lines. However these working assumptions, that might not reflect the real construction of the SDRAM, produce negligible effects when compared with all the other uncertainties.

## 5.6 SDRAM output file: data analysis

At this stage of the analysis we associate to the logical address of every upset its physical location (remapping). Figure 5.8 show the upsets accumulated in a sequence of 5 frames. One can observe the presence of 9 groups of upsets that are interpreted as being due to 9 heavy ion impacts (in this case 241 MeV  $^{79}\text{Br}$ ).

The next step is to implement a clustering algorithm to distinguish the groups of upsets. The SDRAM is read row by row. The algorithm records the position of a seed: the first upset it finds. The position of the next upset is compared with that of the seed and the Pythagorean distance ( $dist^2 = \Delta x^2 + \Delta y^2$ ) is calculated. If the distance is less than a maximum distance  $D_{max}$ , the new upset it is associated to the seed to form a cluster, otherwise the cluster of the seed is closed, the centroid of the cluster is calculated and the new upset becomes a new seed. The process is repeated till the end of file is reached.



**Figure 5.8** The 41 upsets found in a sequence of 5 frames: nine groups are visible.

The maximum distance  $D_{max}$  was set to 5  $\mu\text{m}$ . This value was chosen looking at the experimental event distribution not to arbitrarily mix separate clusters; for  $D_{max} < 3 \mu\text{m}$ , the risk becomes high to break a single event in two clusters.

Table 5.1 shows the result of the simple clustering algorithm of the upsets shown in Figure 5.8. The first column gives the frame in which the upsets were found; the second column is the progressive cluster number found by the algorithm; the third column is the progressive number of the upset inside a cluster (the first is the seed of the cluster); the 4<sup>th</sup> and 5<sup>th</sup> columns report the X and Y coordinates of the upsets. In this case the algorithm correctly found all 9 groups.

Sequence of data parsed in clusters

Frame	Cluster #	X [ $\mu$ m]	Y [ $\mu$ m]	Frame	Cluster #	X [ $\mu$ m]	Y [ $\mu$ m]		
1	1 <sup>st</sup>	1	1052.28	1414.67	3	5 <sup>th</sup>	1	1056.34	1382.75
		2	1053.63	1414.67			2	1057.69	1382.75
2	2 <sup>nd</sup>	1	935.38	1367.63			3	1056.34	1383.76
		2	936.734	1367.63			4	1057.69	1383.76
		3	935.38	1367.97	4	6 <sup>th</sup>	1	934.026	1335.89
		4	936.734	1367.97			2	935.38	1335.89
3	3 <sup>rd</sup>	1	1091.54	1304.98	4	7 <sup>th</sup>	1	932.672	1358.22
		2	1092.9	1304.98			2	934.026	1358.22
		3	1094.25	1304.98	4	8 <sup>th</sup>	1	978.708	1410.98
		4	1091.54	1305.31			2	980.062	1410.98
		5	1092.9	1305.31			3	978.708	1411.98
		6	1091.54	1305.65			4	980.062	1411.98
		3	4 <sup>th</sup>	1	985.478	1371.66	5	9 <sup>th</sup>	1
2	986.832			1371.66	2	927.256			1398.54
3	985.478			1372	3	928.61			1398.54
4	986.832			1372	4	929.964			1398.54
5	988.186			1372	5	925.902			1398.88
6	989.54			1372	6	927.256			1398.88
7	985.478			1373.01	7	928.61			1398.88
8	986.832			1373.01	8	929.964			1398.88

**Table 5.2** Table of the sequence of clustered upsets corresponding to Figure 5.8. In the first column the cluster number, in the second the event number inside a cluster, then the X and Y coordinate of the upset.

This simple clustering algorithm fails when two separate groups of upsets inside the same SDRAM frame share a row (Figure 5.9); a distant upset on a row (B1) becomes a new seed and breaks the clustering of the first group into two clusters (clusters A and C). For the same reason even the second group is broken: the upsets in the D cluster are not grouped properly with the B upsets. However only few events fall in this category.

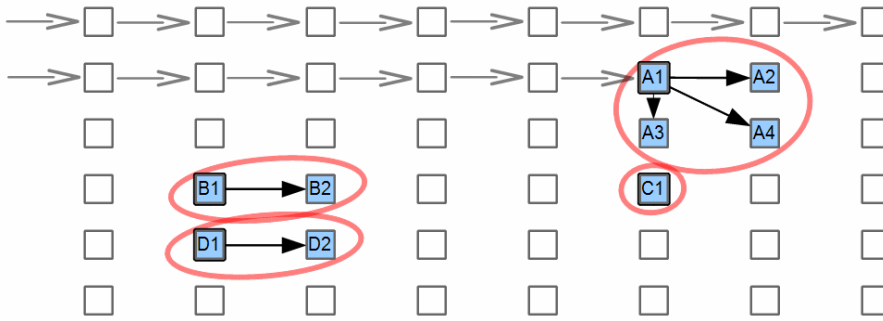


Figure 5.10 Exemplification of how the simple clustering algorithm may fail. Upset C1 is not grouped with cluster A while the cluster D is not grouped with cluster B.

## 5.7 Using the SDRAM to study the IEEM performance

### 5.7.1 Introduction

The high spatial regularity of the SDRAM makes it useful to measure the effective lateral resolution of the IEEM and to map-out distortions in the IEEM image. This is done by comparing the positions of the ion-induced SEU-clusters in the memory array with the map of the ion impacts on the ultra-thin gold membrane above the SDRAM as reconstructed by the IEEM.

We here report on a very high statistics experiment to measure the IEEM performances. The experiment was made possible because of the important upgrades to the SDRAM system:

1. the time-stamp is now available
2. the readout of the SDRAM can now be limited to any part of the memory array, in particular to only that small portion that is exposed to the ion beam and that that is the field of view of the IEEM.

Previously [54] the time-stamp was not implemented and the SDRAM readout was very slow, as the whole memory was readout. For this reason a mechanical shutter was used to inhibit the beam during the long readout process. The SDRAM was exposed to a few tens of ions, during a short shutter-opening, as all the SEU clusters in the exposure were then compared with the ion impacts registered by the IEEM during the same exposure. This proof-of-principle experiment did give a first

indication of the effective resolution of the IEEM setup, but the number of events was too low to study image distortions.

In this experiment the 150×300 memory cells located in the 200 μm area exposed to the ion beam are continuously read-out and refreshed at a frequency of 600 Hz and the system looks for changes in the loaded logic pattern. In this way a temporal coordinate can be assigned to every ion-induced upset cluster with an accuracy of ~1.7 ms, the readout period of the portion of the SDRAM exposed to the ion beam.

The ions are detected by the IEEM system as they passes through the Au-Si<sub>3</sub>N<sub>4</sub> membrane and the spatial and temporal coordinates of the impact point are recorded; the events collected by the SDRAM system and by the IEEM are put into correlation employing the time-stamp coordinates associated to each event. This analysis is performed offline, by comparing the files generated by the two systems. The readout period of the IEEM system is 17 times faster than the SDRAM one (the temporal accuracy of the IEEM system is 106 μs). Therefore every SDRAM centroid is associated with all the IEEM events detected up to 1.7 ms earlier. In this experiment the ion flux ( $10^6 \text{ cm}^{-2} \text{ s}^{-1}$ ) was high to accumulate enough statistics. With this flux 3–5 IEEM events, on average, were associated with every SDRAM readout, only one of which may correspond to the ion that created a SDRAM cluster. Some of the additional events were beam-related background signals in the IEEM system, not due to real ion impacts on the SDRAM<sup>20</sup>.

### 5.7.2 A high statistics experiment using 241 MeV Br79 ions

In this high statistics experiment we used a 241 MeV <sup>79</sup>Br ion beam, collecting 240,000 events (fluence of  $10^9 \text{ cm}^{-2}$ ), a number that allows us to evaluate the quality of the image generated by the IEEM in a way not previously possible. The distance of the SDRAM from the Au-Si<sub>3</sub>N<sub>4</sub> membrane was comfortably adjusted to 800 μm, which we consider a large distance, almost a worst-case scenario. This choice is due to the presence of contact pads for the wire bonds located at the middle of the SDRAM. The ion flux of this experiment was ~500 ions/s in the field of view.

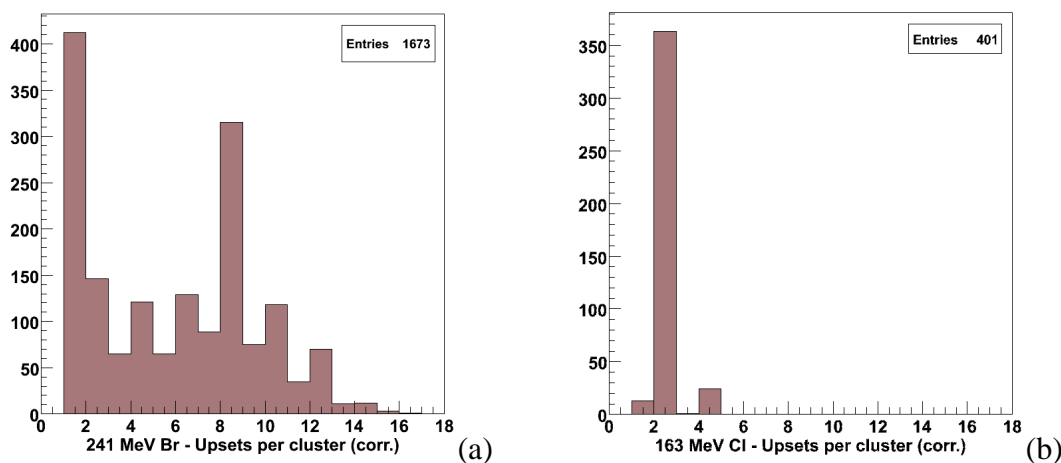
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<sup>20</sup> These background signals is now reduced by placing a 500 μm collimator 1 m upstream of the MCP of the IEEM. The background suppressing collimator, now a standard feature, was not available at the time of the experiment here described.

The SDRAM area fitted by the IEEM field of view did not show the alternation in cell behaviour described in Section 8.4: all cells were regularly filled with 0 and the presence of a 1 was interpreted as an upset in the cell. The distribution of the number of upsets in clusters produced by the 241 MeV  $^{79}\text{Br}$  ion beam that are correlated with IEEM is reported in Figure 8.11(a), along with analogous data collected with a 163 MeV  $^{35}\text{Cl}$  ion beam for comparison (Figure 8.11(b)). In the 241 MeV  $^{79}\text{Br}$  data one can see the presence of two populations, one with low multiplicity and a second one, centred around 8 flipped cells, which is absent in the 163 MeV  $^{35}\text{Cl}$  data.

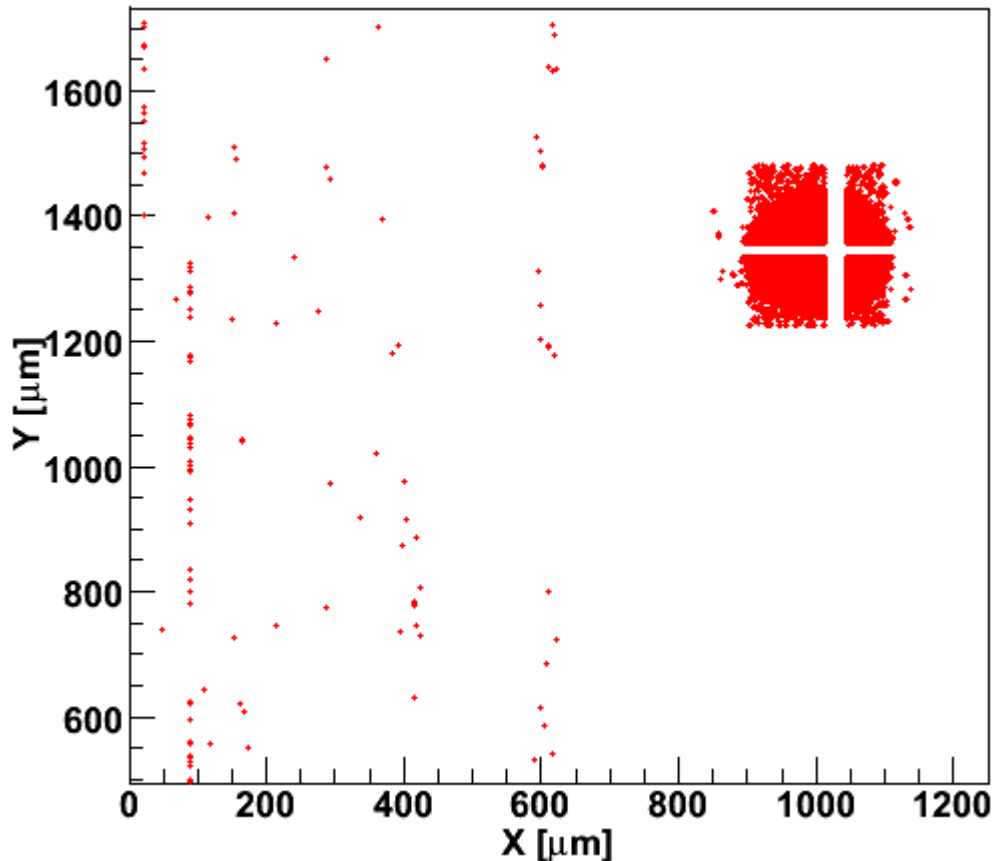
The electron-hole pairs an ion generates in the SDRAM diffuse in the silicon and cells near the ion trajectory can collect enough charge to undergo an upset, changing the value of their stored data, as exemplified by Chlorine ions. The behaviour of the SDRAM with a highly ionizing Bromine ion is more complex because the stronger perturbation may propagate along the metallization lines and affect cells at greater distances.

The two populations were analyzed together, as the long clusters develop along a row and we will be interested in how precisely we locate the impact in the column direction. The positions of the flipped cells are reconstructed and the clusters and the coordinates of its centroids, assumed to be the position of the ion impacts, are determined using the algorithm described in 8.5.



**Figure 5.11** In figure (a), the distribution of the number of upsets in clusters that are correlated with IEEM events in our 241 MeV  $^{79}\text{Br}$  ion beam experiment. For comparison, in figure (b), the same distribution for an experiment performed using 163 MeV  $^{35}\text{Cl}$  ion beam.

Figure 5.12 shows the coordinates of the SEU found in the SDRAM in this experiment. Most of the SEU are located inside the 200  $\mu\text{m}$  diameter disc given by the contrast diaphragm of the IEEM. The empty crossed region inside the disc is due to the absence of memory cells outside the array segments; in this region run the data connection lines of the SDRAM. The points outside and far from the disc are due to occasional corruptions of addresses.

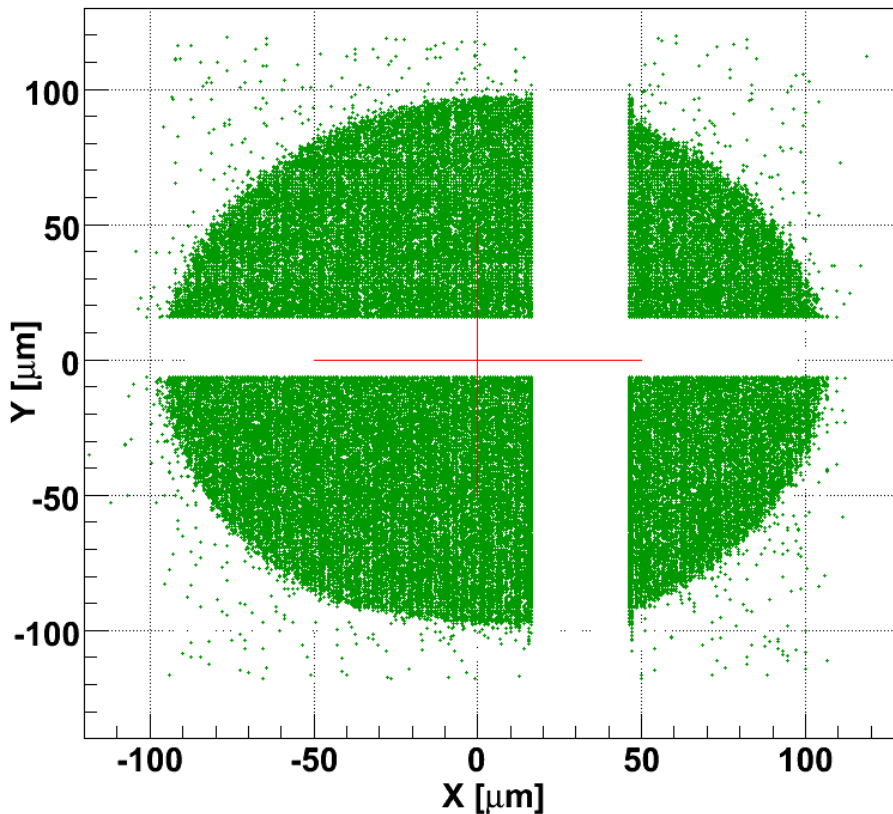


**Figure 5.12** The SEU locations as reconstructed by the mapping. The locations outside the disc-like region (the exposed area) are due to the corruption of the address of upset cells.

The clustering algorithm is now employed to calculate the centroid of the SEU-clusters (Figure 5.13). The centroid is assumed to be the position of the ion impact on the SDRAM.

For the following discussion, it is important to keep in mind that the centroid is determined with a better uncertainty in the Y-direction as the distance of the rows of the memory cells (Y-direction) is 0.3  $\mu\text{m}$ , while the distance of the columns (X-direction) is 0.6  $\mu\text{m}$ . However the cells of the array are organized in pairs of bits that

occupy the same row and two adjacent columns. When we detect a SEU of only one cell of a pair, we cannot establish with certainty the column of the flipped cell, so we decided to map the X-coordinate of a bit flip at the center of the cell-pair<sup>21</sup>. With this choice the granularity of the X-coordinate is 1.2  $\mu\text{m}$ . For this reason the resolution studies and results we report will always refer to the Y-coordinate.

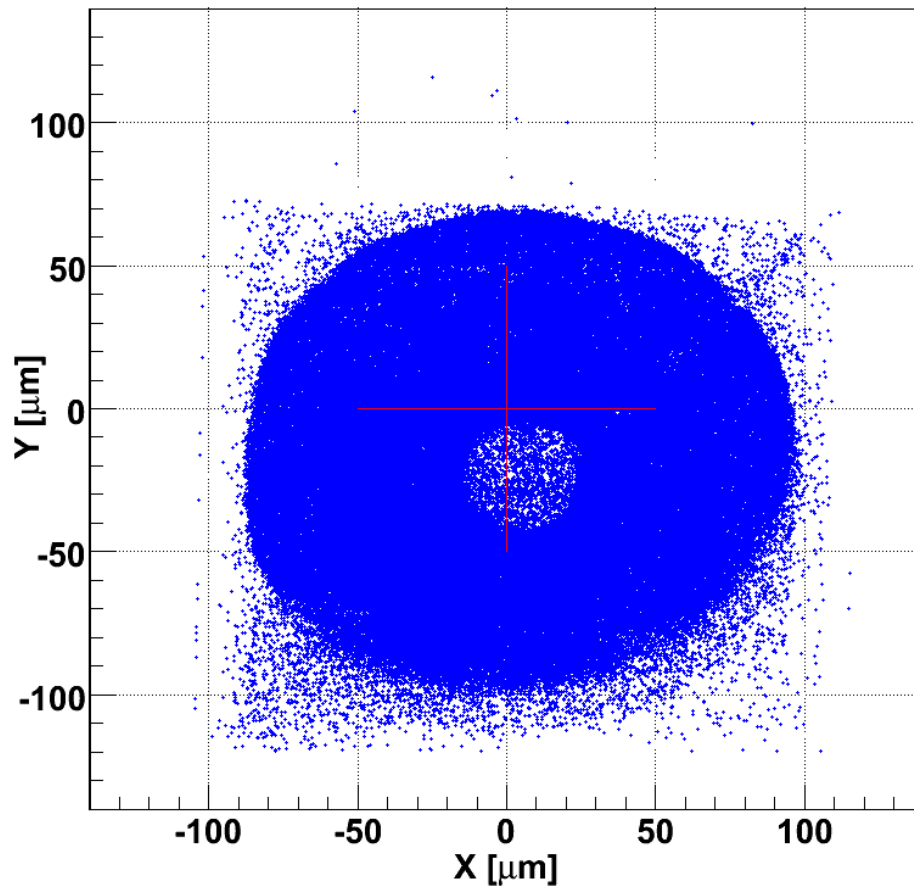


**Figure 5.14** The centroids calculated by the clustering algorithm. The centroid is taken to be the ion impact point as detected by the SDRAM. These points will be then compared to the ion impact points on the gold membrane ad reconstructed by STRIDE.

Figure 5.15 shows the ion impact points on the ultra-thin gold membrane as reconstructed by the IEEM. Most of the points are distributed in a roughly annular region: the central region corresponds to the hole of the annular MCP secondary electron detector. The otherwise scattered points (including the ones inside the central region) are due to occasional errors in determining one or both the impact coordinates.

<sup>21</sup> This ambiguity could not be resolved with the laser remapping technique because the laser spot was too big ( $\sim 10 \mu\text{m}$ ).





**Figure 5.15** The ion impact points on the ultra-thin gold membrane as reconstructed by the IEEM. Most of the points are distributed in a roughly annular region: the central region corresponds to the hole of the annular MCP secondary electron detector. The scattered points (including the ones inside the central region) are due to occasional errors in determining the impact coordinates.

The present STRIDE algorithm makes errors when:

1. STRIDE matches the X-coordinate of one event with the Y-coordinate of the preceding or the following event. This may occur when the ion detection rate is high, as in this high statistics experiment.
2. when two ion impact events are recorded in the same frame. In this case the X and Y ambiguity may only be resolved if the two signals have a different amplitude. These errors occur easily when the ion impact is near the edge of the field of view since the amplitude of the near-edge signal is suppressed by the optical system (aberrations);
3. a real signal on one coordinate is matched with a noise signal.

### 5.7.3 IEEM-SDRAM Data Correlation

We now present the results of the data analysis that matches the ion impacts detected by the IEEM and by the SDRAM.

The SDRAM centroids and the IEEM detected impacts are put into correlation by employing the time coordinate associated to each event. To readout the irradiated area of the SDRAM typically takes about 17 FrameNumbers, which corresponds to a 1.7 ms readout time. The time correlation between SDRAM and STRIDE events is performed in this time interval in the following way: the time coordinate of a SDRAM cluster is the FrameNumber in which it was detected; all the STRIDE events that occurred in the 1.7 ms time interval prior to that FrameNumber are associated to the cluster. Figure 5.16 shows a SDRAM centroid (red circle) and four STRIDE events (blue dots) that preceded it within 1.7 ms.

The time information is therefore not sufficient to unambiguously associate a SDRAM event with a STRIDE one. The ambiguity can be resolved by requiring spatial proximity. In Figure 5.16 the IEEM signal that lies within the 4  $\mu\text{m}$  radius circle centred around the SDRAM fired cell is likely to be due to the ion that caused the upset in the SDRAM.

However a circular proximity cut is meaningless to measure the spatial resolution of the IEEM. Instead a Transverse Cut is applied in the following by requiring the difference of the X-coordinates (the less precise ones) of the STRIDE event and of the SDRAM centroid to be less than 10  $\mu\text{m}$ .

Figure 5.17 shows a set of nine SDRAM centroids in a  $50 \times 50 \mu\text{m}^2$  region and the STRIDE events that are correlated temporally and accepted by the Transverse Cut: 6 out of 9 centroids have a STRIDE event nearby.

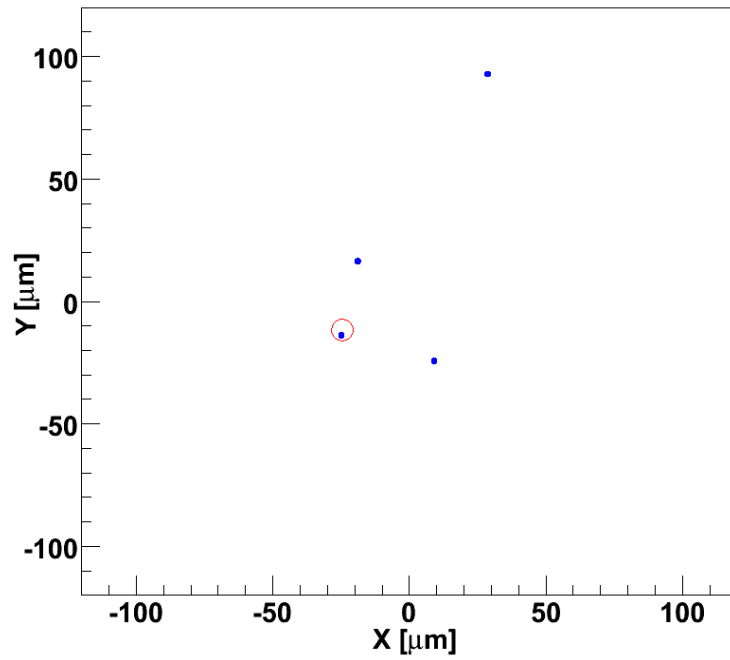


Figure 5.16 The red circle is centred at the position of the centroid of one SDRAM cluster. The blue dots are IEEM events that are temporally associated to it. The radius of the red circle is 4 μm.

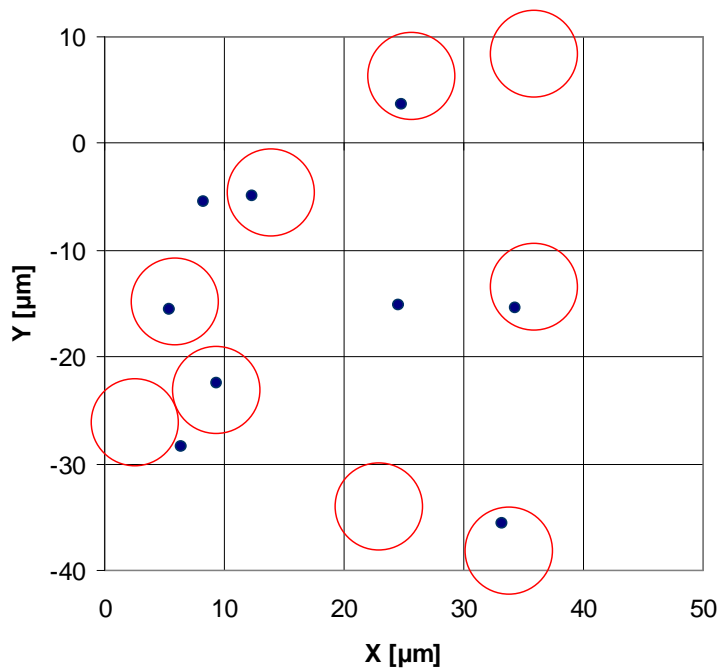
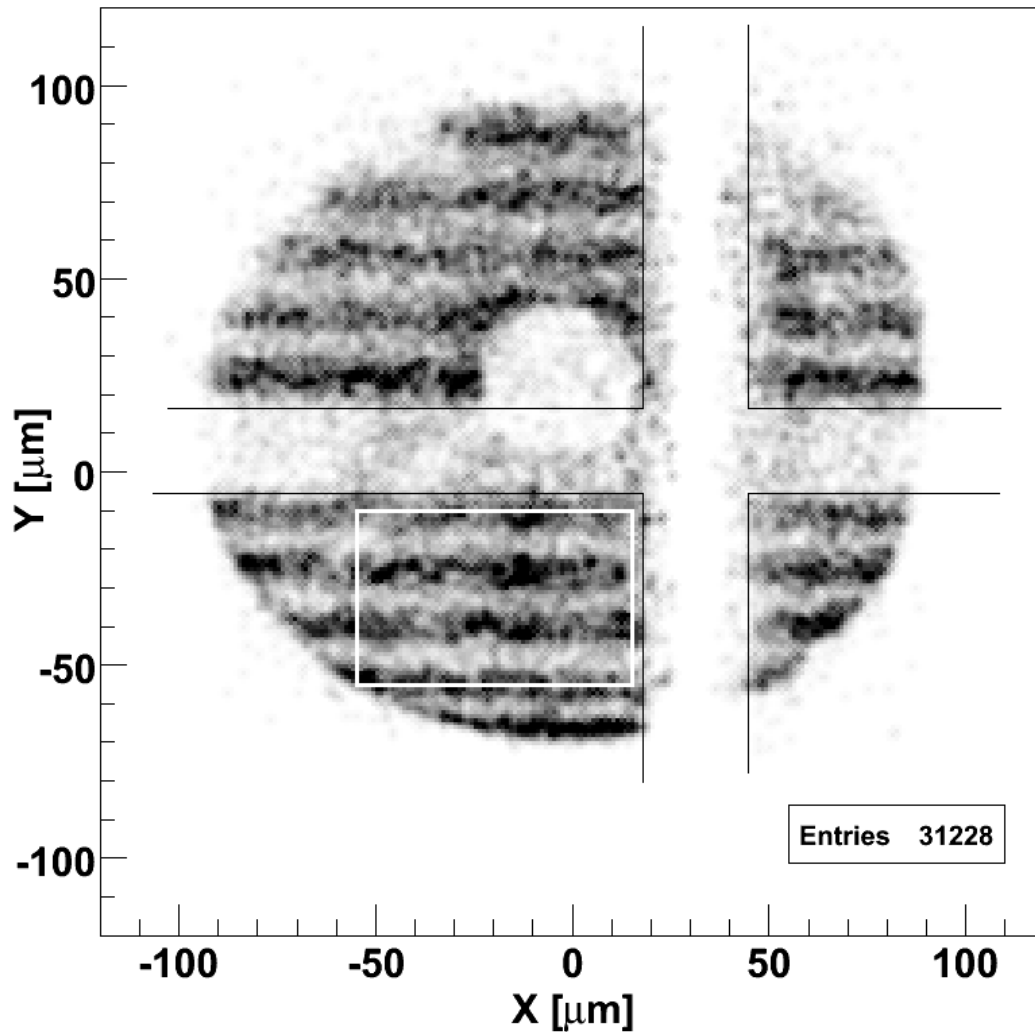


Figure 5.17 The red circles of radius 4 μm are centred at the positions of the centroid of SDRAM clusters and the IEEM events (blue dots) that are temporally associated to them. In addition the Transverse cut (see text) is applied to impose a proximity requirement.



**Figure 5.18** IEEM events time-correlated with a SDRAM centroid after the Transverse Cut (see text). For the events in this figure, SDRAM centroids are required to lie inside horizontal stripes 8 μm wide separated by 8 μm wide gaps. The wide vertical and horizontal gaps represent the non sensitive regions that divide the SDRAM into segments. The central circular area corresponds to the hole in the annular MCP. The region inside the white rectangle was used for the peak-correlation analysis discussed in the text.

Figure 5.18 is an illustration of the capability of IEEM to image the sensitive areas of the SDRAM. The figure is a 2D histogram of all IEEM events that are correlated temporally and spatially (Transverse Cut) with SDRAM centroids. SDRAM centroids were selected inside horizontal stripes 8 μm wide separated by 8 μm wide gaps for display purposes.

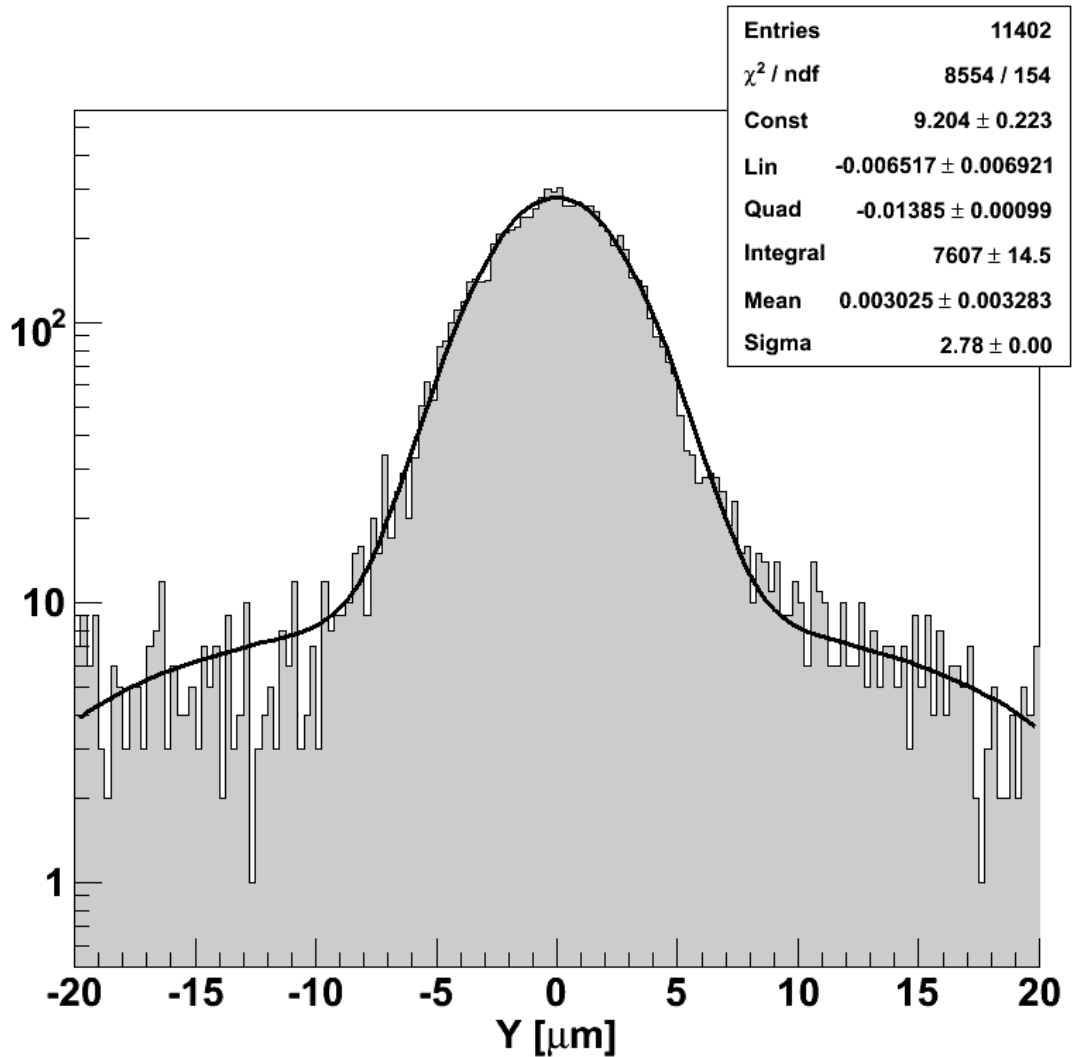


Figure 5.19 The experimental correlation peak distribution for the events lying in regions I and II shown Figure 5.18.

We measured the resolution of the IEEM with the *correlation-peak* technique [54] which consists in filling a histogram of the Y-coordinate difference of every SDRAM centroid with all the IEEM events accepted by time correlation and the Transverse Cut. Only the events within the 45  $\mu\text{m}$ -by-70  $\mu\text{m}$  fiducial region of Figure 5.18 were considered in the analysis.

The histogram, shown in Figure 5.19, presents a Gaussian shaped correlation peak ( $\sigma = 2.8 \pm 0.1 \mu\text{m}$ , corresponding to  $\text{FWHM} = 6.6 \pm 0.2 \mu\text{m}$ ) above a quadratic combinatorial background. The error we report is the spread of the values of the

sigmas we obtained performing the analysis in 4 equal regions obtained by dividing the white rectangle into 4 equal parts.

The correlation-peak signal above background is due the successful matching of STRIDE events with SDRAM centroid and the width of the peak is taken to be the measure of the spatial resolution of the IEEM.

In spite of the high statistics this experiment does not improve the preliminary resolution measurement reported in the previous work [54]. This unsatisfactory outcome, in spite of the improvement in the experimental apparatus and the high collected statistics, deserves to be carefully studied. Some results of this study will be reported in the following chapter. We only recall here some experimental differences between this and the previous experiment and we make explicit an assumption.

1. the distance of the SDRAM from the gold membrane (now 800  $\mu\text{m}$ ) was previously 300  $\mu\text{m}$  only;
2. two different SDRAMs were used in the two experiments;
3. the two SDRAMs were not irradiated in the same specific area but these were arbitrarily chosen;

#### **5.7.4 Efficiency of the IEEM system in reconstructing ion impacts**

Not all of the SDRAM centroids can be detected by the IEEM. The main sources of inefficiencies of the IEEM are:

- the field of view of STRIDE (diameter 180  $\mu\text{m}$ ) is smaller than the irradiated area (diameter 200  $\mu\text{m}$ );
- the annular MCP is geometrically inefficient (central hole; blind spots);
- the biasing wire of the diaphragm of the annular MCP casts a shadow;
- the inefficient detection of secondary electrons (the MCP was not at full voltage<sup>22</sup>);

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<sup>22</sup> The annular MCP is showing signs of age. To slow aging and avoid the formation of new blind spots we set the working voltage at 4.8 kV instead of the nominal 5.0 kV.

- the inefficiency of the image intensifier in detecting photons created by the MCP+phosphor stack inside the IEEM;
- the measurements errors of STRIDES.

To evaluate the efficiency of the IEEM system to correctly reconstruct ion impacts we calculated the fraction of times a STRIDE event is successfully associated with a SDRAM centroid respect to the total number of SDRAM centroids. The region we used is the fiducial region shown in Figure 5.18; it was chosen as it is:

- away from the gaps between the segments of the SDRAM;
- away from the central hole of the annular MCP and other inefficient areas of the MCP;
- away from the shadow of the biasing wire.

A total number of 12452 SDRAM centroids are inside the fiducial region. The number of correlated STRIDE events, in this case 7607, is determined by the number of entries under the correlation-peak, i.e. the area of its gaussian fit. The measured effective efficiency of reconstructing the ion impact and associating it to a SDRAM cluster is hence measured to be 61%, instead of the previously reported ~90% [55]. It is the net effect of the degradation in efficiency of:

1. the annular MCP inside the IEEM in detecting the secondary electrons emitted by the ion impacts on the ultra-thin gold membrane;
2. the image intensifier in detecting photons from the MCP+phosphor stack of the IEEM;
3. the NMOS sensors;
4. the STRIDE system in correctly reconstructing the ion impact positions in a high statistics experiment.

We do not worry about the loss in efficiency which is essentially a money problem.





## 6 Resolution degradation studies

The resolution of the IEEM system at SIRAD ( $\sigma=2.8\pm0.1 \mu\text{m}$ ) appears to be at least two times worse than the one reported by Doyle [6]. We note that also the resolution using UV photo-electrons (the PEEM mode) is worse than the one reported by the manufacturer (see 4.2.2).

The global IEEM performance can be affected by many factors:

1. the presence of image distortions in the field of view (FOV);
2. the scattering of the ions crossing the gold-Si<sub>3</sub>N<sub>4</sub> membrane;
3. the presence of vibrations in the IEEM system;

In this chapter we will take advantage of the high statistics collected in the BR experiment, which was not available in the previous ones, to try to disentangle the different factors that can affect our spatial resolution. In addition we will describe two studies we performed to investigate the discrepancy of the resolution of the PEEM/IEEM system: a study of the vibrations and a study of the output signals of the light sensor of the DAQ.

### **6.1 Evaluation of the factors affecting the resolution**

The analysis reported in this section is based on the events collected with the 241 MeV <sup>79</sup>Br ion beam discussed in the previous chapter.

To study large scale distortions across different regions of the full field of view, we divided it into  $10\times10 \mu\text{m}^2$  areas and performed in each the correlation-peak analysis to measure the resolution in the Y-direction. Figure 6.1 shows the distribution of the differences among the means of the correlation peaks calculated in the single small size areas and their global average: for more than 90% of the areas the difference is less than 2  $\mu\text{m}$ . Some systematic effects are present as outlined by the 2D distribution of the means of the correlation peaks shown in Figure 6.2. In this

figure the size of each marker is proportional to the difference from the global average; the sign of the difference is encoded by the grey intensity

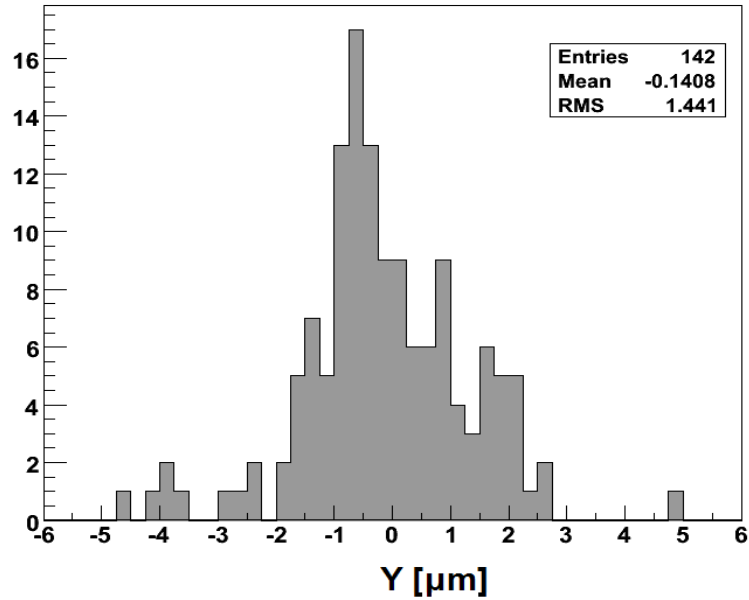


Figure 6.1 Distribution of the differences from the average value of the means of the Y-coordinate correlation peaks in the  $10 \times 10 \mu\text{m}^2$  areas of Figure 6.2.

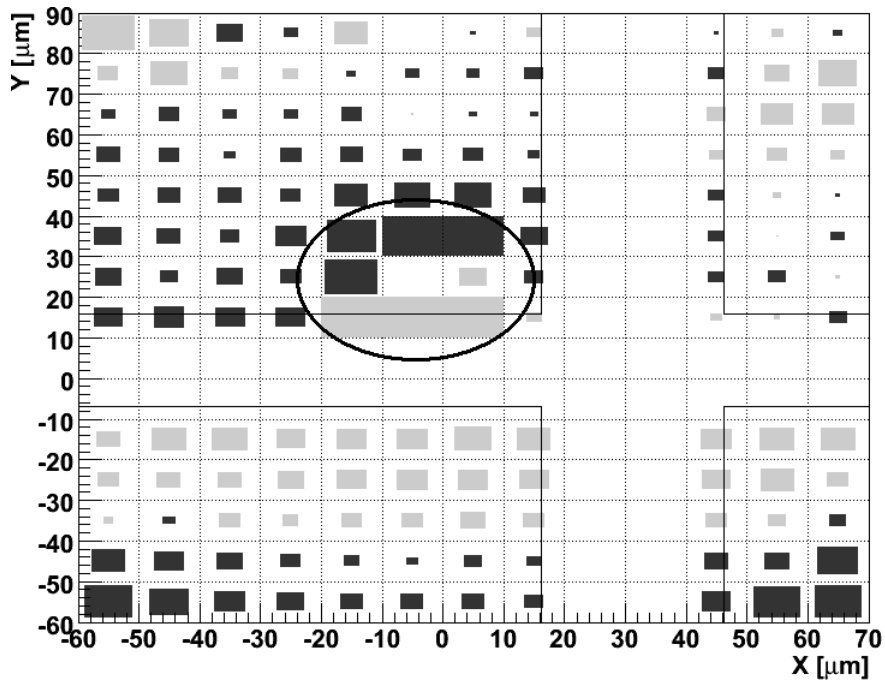


Figure 6.2 2D histogram of the means of the correlation peaks in the Y-coordinate in the  $10 \times 10 \mu\text{m}^2$  areas of the central region on the field of view. The size of each marker is

proportional to the difference from the global average; the sign of the difference is encoded by the grey intensity.

Nevertheless the histogram of the sigmas of such distributions is Gaussian (Figure 6.3) with an average value (*average local resolution*)  $\sigma_{\text{ave}} = 2.81 \pm 0.38 \mu\text{m}$ . The spatial resolutions calculated on small size areas do not disagree with the global one, indicating that, although distortions are present and may be corrected, they are not the major factor in degrading the spatial resolution of our IEEM.

To simulate the effects of the membrane (a 30 nm layer of gold on a 100 nm layer of  $\text{Si}_3\text{N}_4$ ) on 240 MeV  $^{79}\text{Br}$  ions we used the SRIM [63] code. In our simulation the ion direction is orthogonal to the membrane surface and ions are uniformly distributed within the fiducial box of Figure 8.19. The SRIM output file was used to project the scattered ions onto a parallel plane 800  $\mu\text{m}$  away (the distance between membrane and SDRAM in the experiment). The two sets of the ion impact coordinates (on the surface of the membrane and on the distant parallel plane) were then analyzed with the correlation-peak technique. The correlation peak in the Y-coordinate is slightly non-Gaussian (10% of events are not accounted for by a Gaussian distribution with  $\sigma = 0.86 \mu\text{m}$ ) over a small combinatorial background (Figure 6.4 (a)). In any case we can conclude that the scattering of the ions on the membrane is not the factor that affects most our experimental spatial resolution.

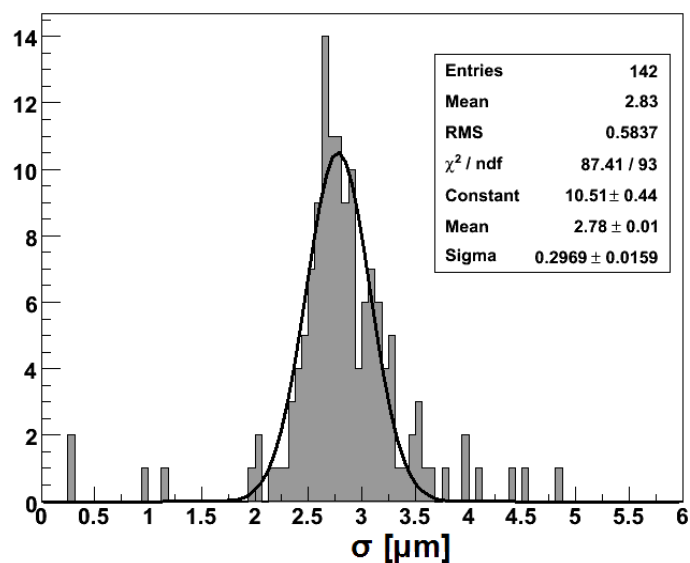


Figure 6.3 Distribution of the sigmas of the Y-coordinate correlation peaks in the  $10 \times 10 \mu\text{m}^2$  areas of Figure 6.2.

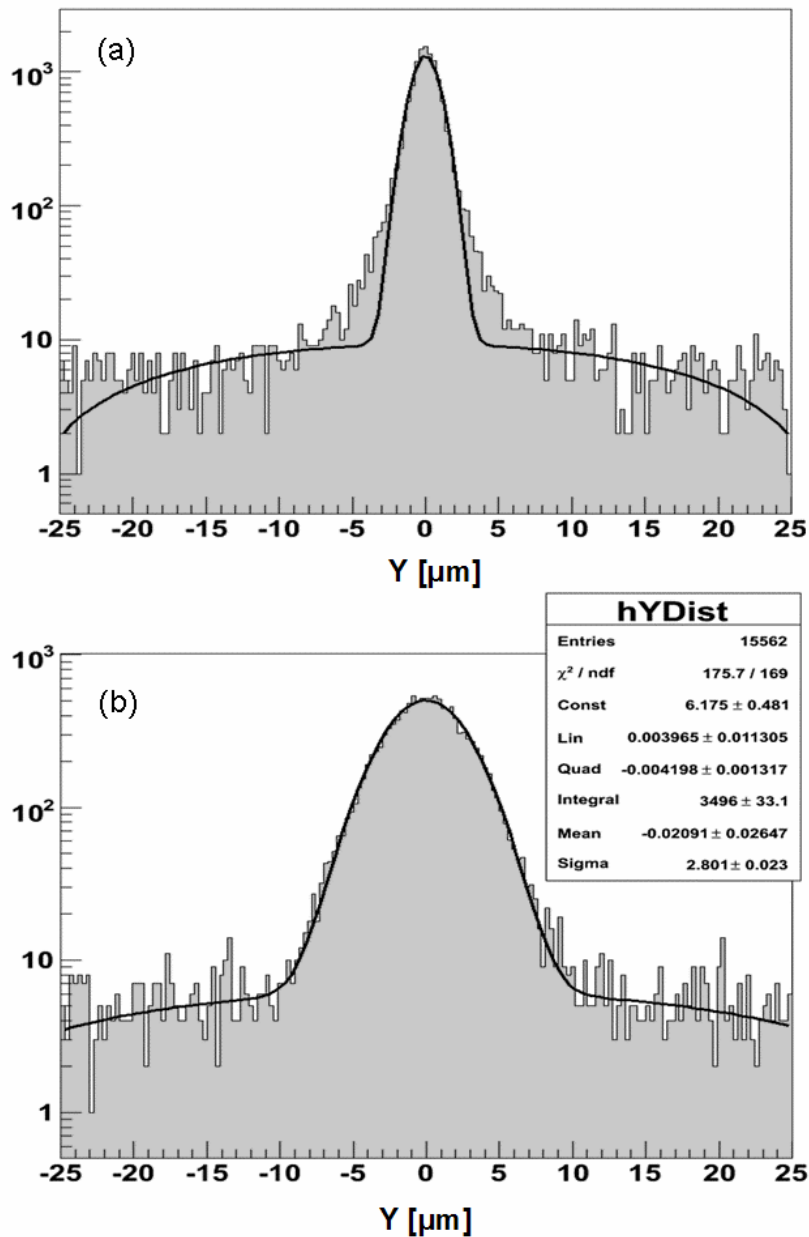
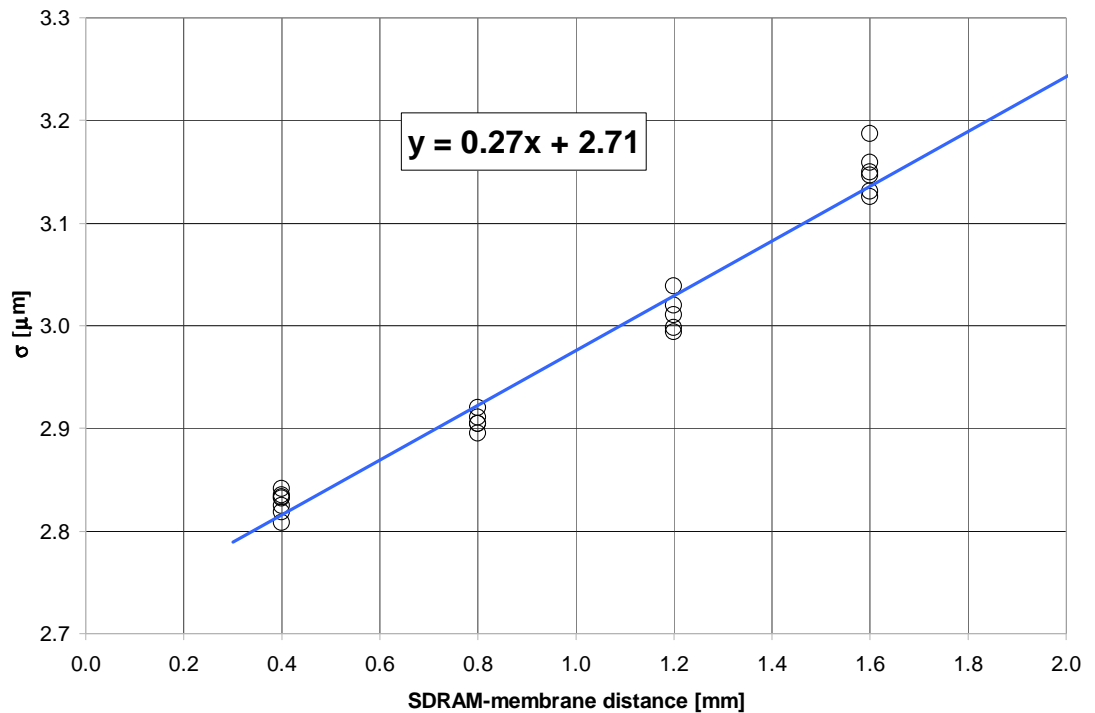


Figure 6.4 (a) Correlation peak (in log scale) of SRIM simulated data (240 MeV  $^{79}\text{Br}$ ) broadened only by the scattering due to the membrane (*membrane contribution*): the peak is slightly non-Gaussian. (b) The above SRIM distribution convoluted with a Gaussian (the fit is a Gaussian plus a quadratic background).

All other resolution degradation effects (for example: vibrations, STRIDE reconstruction errors, ...) can be collectively accounted for by performing a convolution of the scattering effect of the membrane reported above with a Gaussian distribution: the X and Y coordinates of the simulated SRIM scattered events were further randomly scattered with a Gaussian probability distribution function, of zero

mean and given sigma. We then applied the correlation-peak analysis. This was repeated with convolving Gaussians different with different sigma, in order to determine the best sigma value of the convolving Gaussian  $\sigma_{cv}$  that would reproduce the average local resolution of the experimental data. Figure 6.4-b shows that the simulated data used in Figure 6.4 -a convoluted with a Gaussian distribution with  $\sigma_{cv} = 2.5 \mu\text{m}$ , are well fit by a Gaussian with  $\sigma = 2.80 \pm 0.02 \mu\text{m} = \sigma_{ave}$ , i.e. the average value of the local experimental spatial resolution.



**Figure 6.5** The  $\sigma$  of the correlation peak of SRIM simulated events for different distances of the SDRAM behind the membrane.

We can now estimate the expected spatial resolution at different membrane-SDRAM distances with the same technique used above: simulating the effects of the ultra-thin gold membrane on 240 MeV  $^{79}\text{Br}$  ion, projecting to different membrane-SDRAM distances, convoluting with a gaussian ( $\sigma_{cv} = 2.5 \mu\text{m}$ ), and performing the correlation peak analysis. The trend line of the simulated sigma data points, shown in Figure 6.5, has a positive slope of  $0.65 \mu\text{m}/\text{mm}$  which corrects the spatial resolution value, for a membrane-SDRAM distance of  $300 \mu\text{m}$ , to  $\sigma=2.8 \mu\text{m}$ .

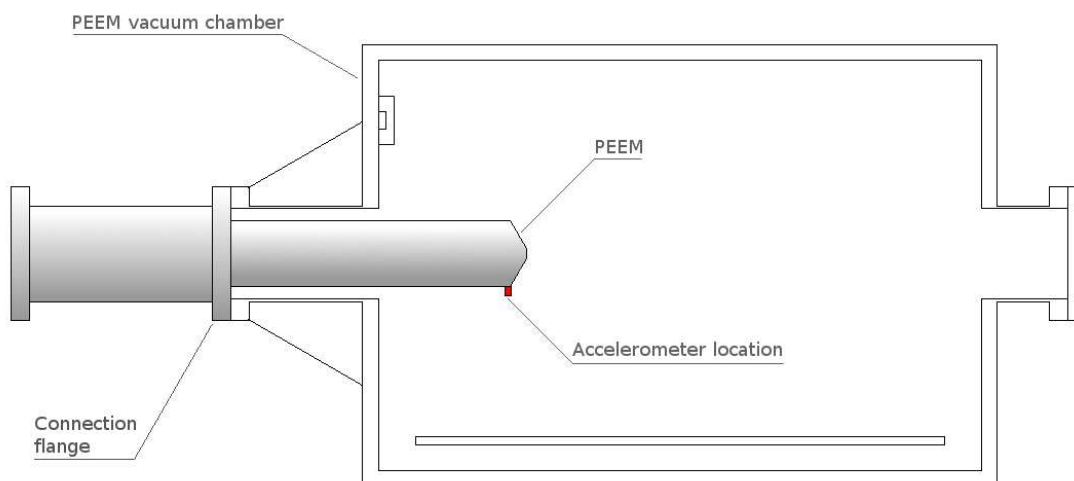
This result confirms that the spatial resolution is practically insensitive to the SDRAM-membrane distance, below 1 mm, and that it is dominated by other factors.

### ***A study of the vibrations of the IEEM system***

Vibrations could be one of the principal causes of the resolution degradation. Indeed we did not invest great efforts to ensure a vibration-free platform, but simply decoupled the IEEM from the vacuum pumps by means of a rubber damper.

To answer to this issue we used an accelerometer (PCB Piezotronics, model 352B10) to measure the vibration of key parts of the IEEM which could be afflicted by this problem.

The first element of the IEEM system we suspected to be prone to vibration problems was the PEEM itself (Figure 6.6), since it is a heavy horizontal metal cylinder mounted as a cantilever with only one full moment connection (the restrained end keeps the PEEM from rotating in the vertical plane; *from falling*). The accelerometer was mounted on the side of the cylinder, as close as possible to the free tip of the PEEM, with the axis in vertical position.

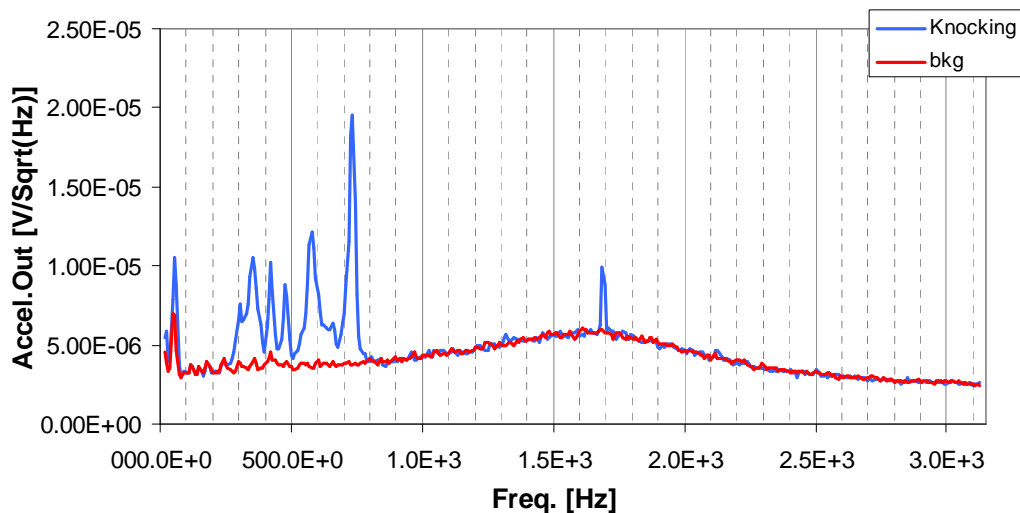


**Figure 6.6** Schematic of the PEEM (shadowed in grey) anchored to the IEEM vacuum chamber.

A low noise signal conditioner (PCB Piezotronics, model 482A22) was used to power the accelerometer and to condition the measured signal for a spectrum analyzer (Stanford Research Systems SR770 FFT network analyzer). The analyzer displays the square root of the Power Spectral Density ( $\sqrt{\text{PSD}}$ ) of the voltage output signal expressed in  $\text{V}/\sqrt{\text{Hz}}$ . The analysis of the PSD immediately reveals the dominant vibration frequencies, allowing the fast identification of the frequency of a particular vibration source. Once identified, a source could be switched off or the disturbance minimized, for example by moving it away. We expected the vacuum pumps to be the main causes of vibrations and this study was intended to be just the starting point for the elaboration of a strategy to minimize its amplitude as the pumps cannot be shut off or removed during IEEM operations.

The presence of characteristic harmonics in the vibration spectrum of the PEEM was quickly verified by simply knocking on the vacuum chamber (Figure 6.6). A set of power peaks appeared in the 300–750 frequency band, together with an excitation peak centred on 1.69 kHz and another one at a lower frequency, centred on 58 Hz.

In particular the 58 Hz peak was very susceptible to excitation when the flange holding the PEEM was slightly tapped (Figure 6.7).



**Figure 6.6** The plot shows the square root of the power spectral density of the output signal of the accelerometer placed on the tip of the PEEM. The blue line is the vibrational spectrum of the PEEM by simply knocking on the vacuum chamber; in red the background.

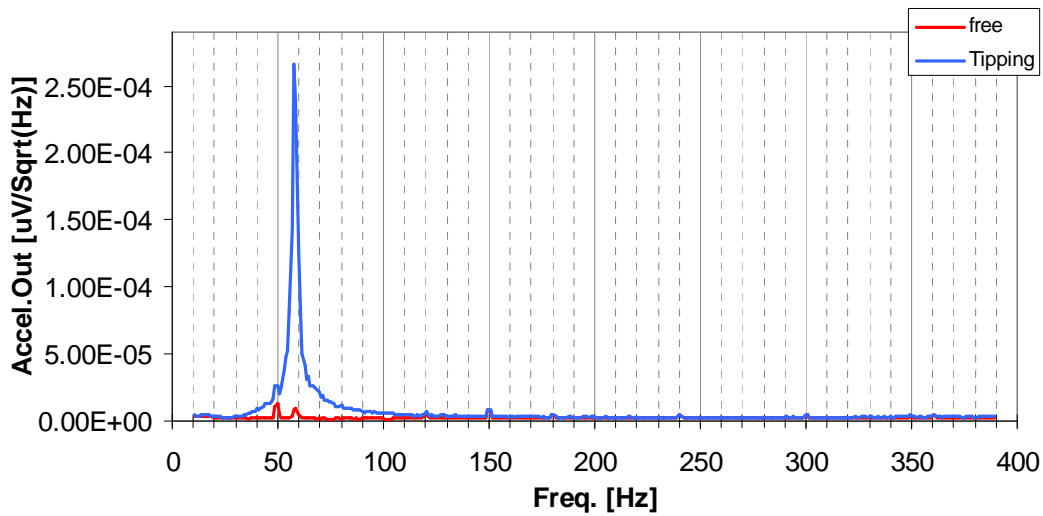


Figure 6.7 In blue the vibration spectrum of the PEEM in the low frequency region. In blue the 58 Hz peak is excited by lightly tapping on the flange of the PEEM; in red the background.

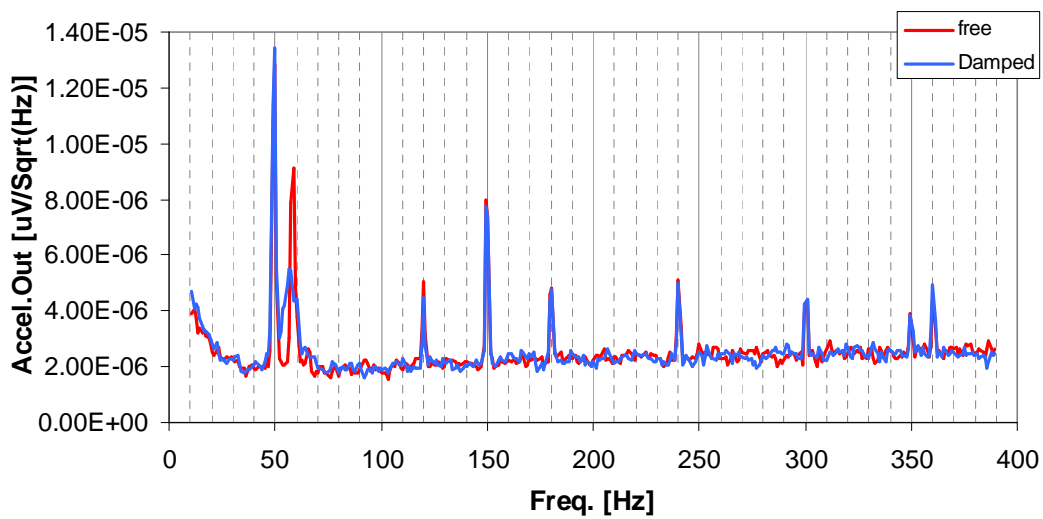
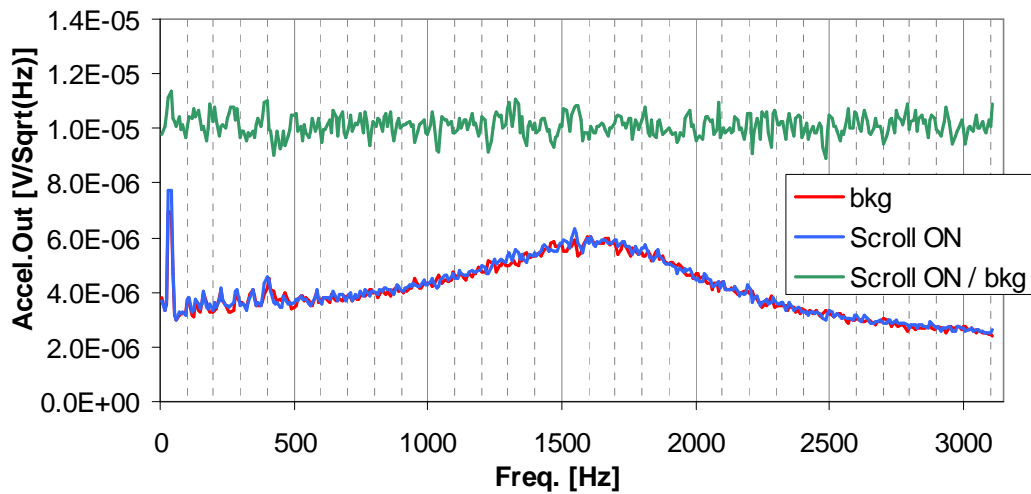


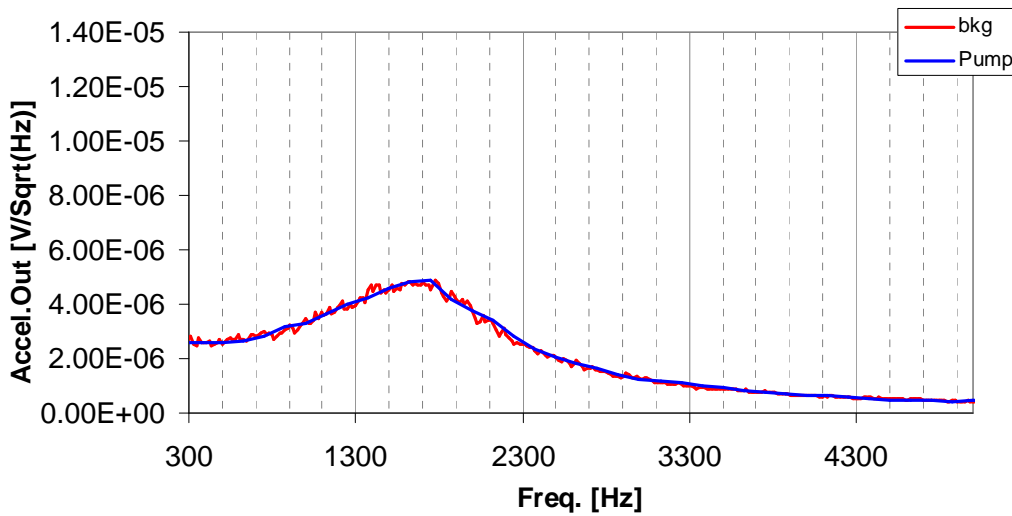
Figure 6.8 In blue the power spectral density of the vibration of the PEEM perturbed tightening the tip with a hand; in red the PEEM free to vibrate.





**Figure 6.9** Contribution to the vibrations due to the scroll pump: in red the vibration power spectrum with the scroll pump on (signal), in blue the pump is off (background). In green the ratio of the signal and the background (multiplied by a factor  $10^{-5}$  to fit the plot).

Figure 6.8 shows in red the power spectrum in the lower frequency band (0-390 Hz): peaks near 50 and 60 Hz and their multiples are evident. We believe these peaks are artefacts caused by the power stage of the spectrum analyzer. To check this we firmly held with a hand the tip of the PEEM (the blue spectrum): all the peaks remain unchanged, with the exception of the 58 Hz peak, which now appears lower and broadened. This confirmed the existence of a true vibration mode with a frequency of 58 Hz that affects the PEEM even when no external perturbation is exerted. In this acquisition, both the scroll and the turbomolecular pumps of the IEEM and all the other sources of vibration that are under our direct control were inactive; i.e. other vacuum pumps on the SIRAD beam line were turned off while pumps on other beam lines in the experimental hall were not.



**Figure 6.10** Contribution to the vibrations due to the turbomolecular pump: in red the vibration power spectrum with the scroll pump on only, in blue both the scroll and the turbomolecular pumps are running at top speed.

We then measured the contribution to vibrations given by the IEEM vacuum pumps. Figure 6.9 shows in blue the power spectral density of the signal of the accelerometer when the scroll pump is ON, in red the same signal with pump OFF. For clarity the ratio between the two lines is reported in green (multiplied by a factor  $10^{-5}$  to fit the plot), showing no meaningful contribution to the vibration spectrum<sup>23</sup>. Similarly, we found no evidence of contributions coming from the turbomolecular pump (Figure 6.10) which, working at a frequency of 700 Hz, was expected to excite high frequency vibrations.

A rough estimate of the amplitudes of the vibrations can be made by modelling our system as an harmonic oscillator: the rms amplitude of the vibration ( $V$ ) increases linearly with the rms amplitude of the impressed acceleration ( $A$ ) and is inversely proportional to the square root of the frequency ( $f$ )

$$(6.1) \quad V = \frac{1}{4\pi^2 f^2} \cdot A$$

<sup>23</sup> To show that there is no significant difference between the two cases (pumps ON/OFF), we did not consider the simple difference of the spectra because it is not meaningful to subtract two noise spectra to look for a signal that is smaller than the noise.

In our case, the dominant vibration mode has an amplitude of  $\sim 10 \mu\text{V}/\sqrt{\text{Hz}}$  rms, that corresponds to an acceleration of  $10^{-3} \text{ g}/\sqrt{\text{Hz}}$  rms ( $1 \text{ g} = 9.81 \text{ m/s}^2$ ), integrated over the width of the power peak: a 1 Hz frequency band (the binning of the PSD output). With this data we calculate a vibration amplitude of  $\sim 70 \text{ nm}$  rms which is more than an order of magnitude smaller than the actual measured resolution of our PEEM with UV photons, and 7 times smaller than the resolving power featured by the PEEM in ideal conditions (manufacture's specs).

These first measurements suggest that the main limiting factor of the system resolution is not due to the PEEM vibrations.

The second element we suspected was the holder of the Device Under Test, a complex micrometric-precision motorized stage; i.e. the holder is not a mono-block but is made of movable parts. For these measurements we built a dummy aluminium DUT provided with a notch on one side to host the accelerometer. The accelerometer was mounted on the upper face of the dummy DUT with the axis in the vertical position to give a measurement of the vertical component of the acceleration.

An analogous analysis performed on the sample holder found no evidence of excited proper oscillation modes.

To support this conclusion, we chose to artificially excite the 58 Hz vibration mode of the PEEM and measured the consequent image degradation as a function of the induced vibration amplitude.

To excite the vibration we used a vibrational exciter (Brüel & Kjær, type 4308) placed on the floor that pushes up on the base of the frame that holds onto the base of the mechanical support of the PEEM system (Figure 6.11). The exciter was powered by an amplifier (Brüel & Kjær, type 2712) driven by a 58 Hz sinusoidal voltage signal, provided by a function generator. Figure 6.12 shows the amplitude of the power frequency spectrum of the 58 Hz peak (expressed in  $\text{V}/\sqrt{\text{Hz}}$ ) as a function of the amplitude of the driving voltage of the excitation. The red dot represents the amplitude of the vibration of the PEEM when no controlled excitation is provided. The blue diamonds show the linear regime of the excitation response (a linear fit in lighter blue), while the green diamonds show the non-linear regime of the response for a more intense excitation.

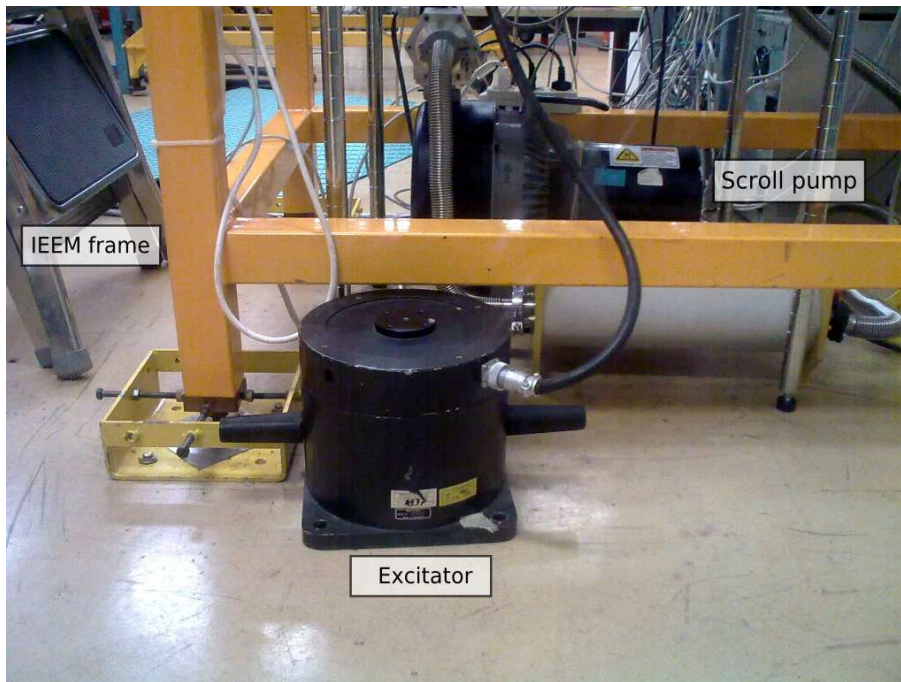


Figure 6.11 Photograph of the Excitator in a standby (extracted) position. When used it is pushed under the yellow IIEM frame.

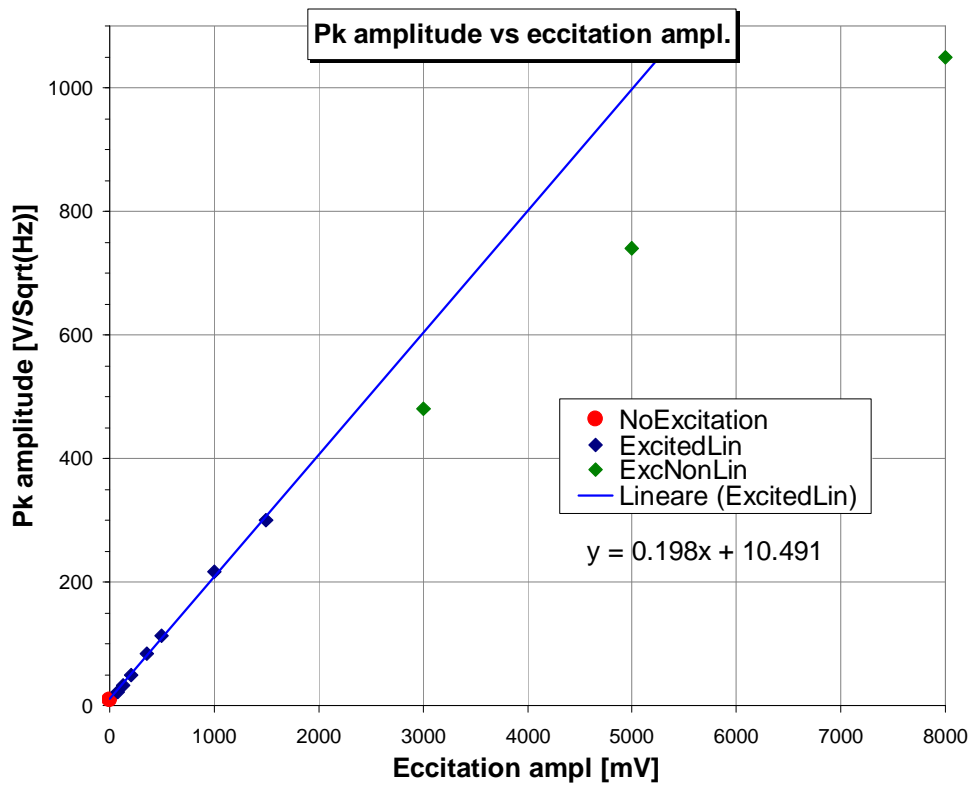
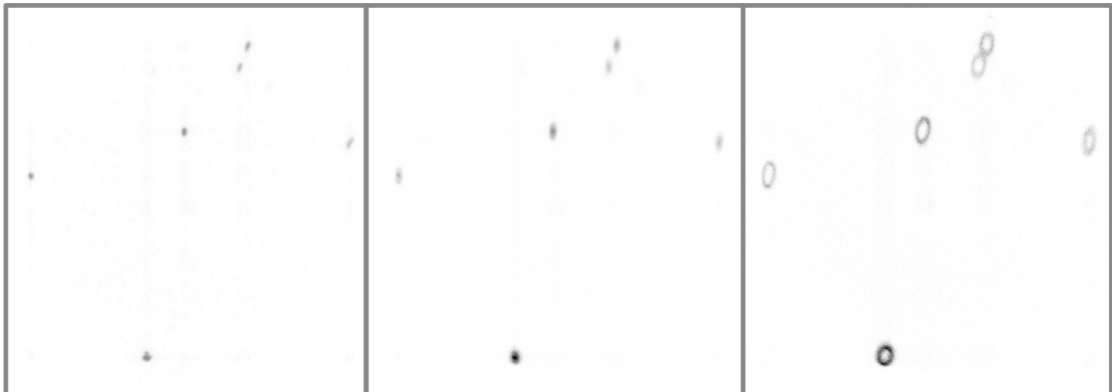


Figure 6.12 Variation of the amplitude of the PEEM vibration, as a function of the excitation amplitude: linear and non-linear regimes, with the fit function of the linear regime.

To analyze the dependence of the PEEM resolution as a function of the vibration amplitude, we took several images of a constellation of bright spots located on the non-emitting surface of the PEEM reference target.

We first accurately focused the system by acquiring a series of four images, setting slightly different voltage values in the objective lens (1.230; 1.235; 1.240; 1.250 kV) and choose the condition providing the best resolved image (following table):

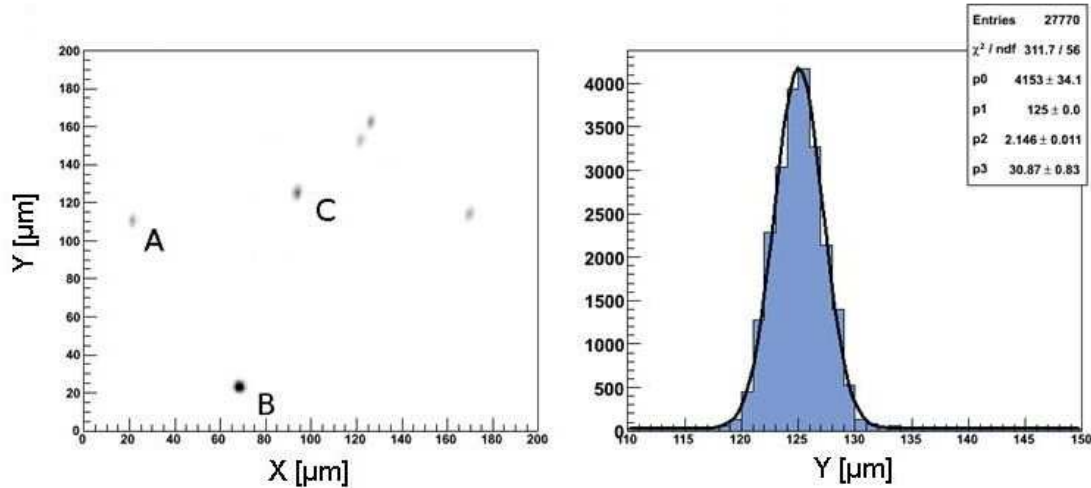
IEEM focus condition			
$V_{\text{Transfer}}$	10.00 kV	$V_{\text{Projective B}}$	0.21 kV
$V_{\text{Objective}}$	1.205 kV	$V_{\text{Decel}}$	1 kV
$V_{\text{Intermediate}}$	9.98 kV	MCP voltage	5 kV
$V_{\text{Projective A}}$	7.03 kV	Image Intens. gain	5 V



**Figure 6.13** The constellations of emitting spots in three different conditions: A) no excited vibrations; B) natural vibration increased by a factor 45: twofold worst resolution; C) excited vibration at full scale: the tip of the PEEM is actually turning around in a circle.

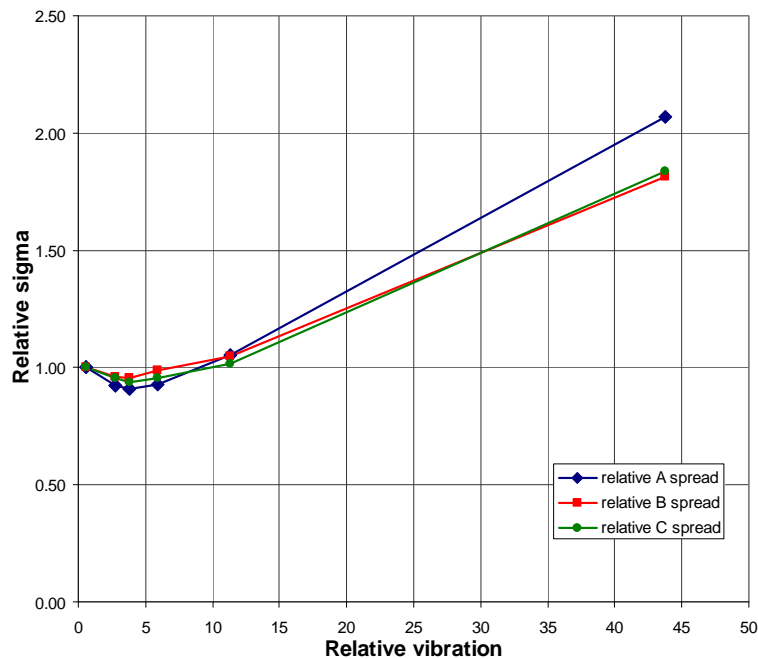
Once the PEEM optics was adjusted, we activated the mechanical excitator to increase the amplitude of the 58 Hz proper vibration of the PEEM and acquired new images (Figure 6.13). In the hypothesis that the dominant contribution to the degradation of the resolution of the IEEM was due to this vibration power peak, we expected to see a blurring of the imaged spot when the external excitation was active, proportional to the amplitude of the vibration. To measure this effect, we analyzed the imaged spots by projecting them along the X axis (Figure 6.14) and by fitting this

projection with a gaussian function. Figure 6.15 shows the plot of the gaussian fit sigma versus the excitation amplitude (in reality the ratio of both variables to the value when no external perturbation was applied).



**Figure 6.14** On the left: IIEEM image of a constellation of small electron-emitting spots in a non-emitting background (arbitrary units). On the right the horizontal projection of the spot C with a gaussian fit.

A slight improvement of the resolution is visible when the external excitation is activated; this could be due to a settlement of the target carrier, caused by the vibration itself, that slightly varied its distance from the microscope, resulting in a drift of the focus condition. This effect doesn't affect the conclusion of the measurements that show that even if we increase by one order of magnitude the proper PEEM vibration, no meaningful increase of the spots blurring was observed. To obtain a twofold blurring increase, we had to rise the PEEM vibration of a factor 45, reaching a vibration amplitude of  $\sim 3 \mu\text{m}$  rms.



**Figure 6.15** Relative variation of the gaussian sigma of the three imaged points (relative to the condition without excitation) as a function of the relative amplitude of the exerted excitation (relative to the proper vibration amplitude). The error along the Y axis is of the order of 1%.. The points are joined with segments to guide the eye.

We conclude that the IEEM system does vibrate at 58 Hz but the amplitude of vibration is too small to account for the discrepancy between the PEEM resolution we obtain and the nominal one reported by the manufacturer. The PEEM has been sent back to the producer for refitting.

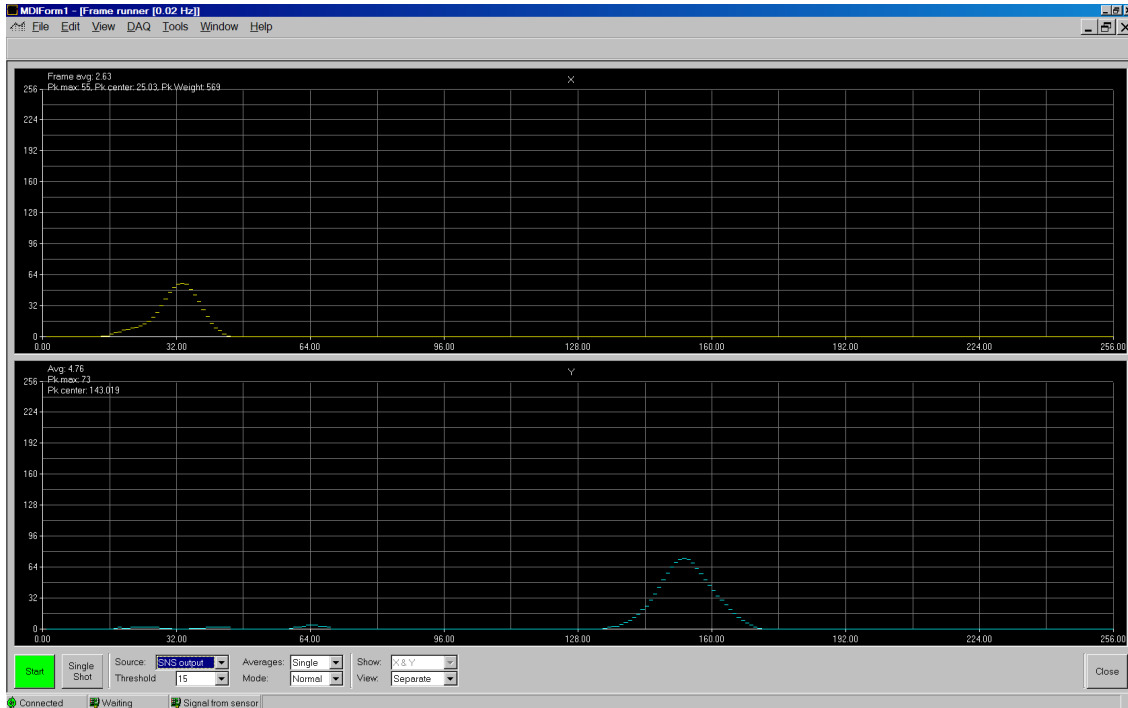
Any way vibrations are not at the origin of the unsatisfactory spatial resolution we found in the IEEM mode.

### *A study of the signal profile of the NMOS sensors*

We then analyzed whether the algorithms used by STIDE to provide the coordinates of the ion impact points may introduce some errors due to differences between the real and the expected luminous signals converted in electric signals by the NMOS sensors.

The experiment was performed with the UV source (IEEM in the PEEM mode) since no more ion beam was available and STRIDE does not record the shapes of the luminous signals but only the calculated charge centroids. Actually an inspection of

the pixel outputs of individual events (*single shot* acquisitions) present asymmetric peaks in many events.

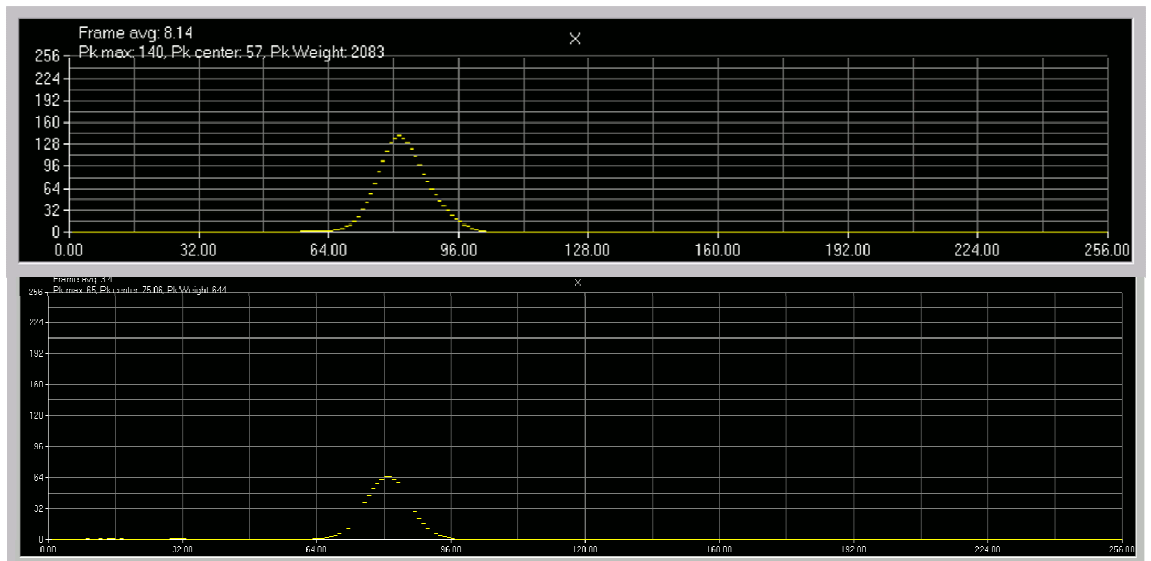


**Figure 6.16** The X- and Y-coordinate pixel profiles of a UV event that is slightly asymmetric in both X (top) and Y (bottom) coordinates. The position detection algorithm of STRIDE uses only pixels above threshold (16 units on the vertical axis) so in this case the algorithm sees a symmetric pixel distribution.

Figure 6.16 shows the pixel output of the NMOS sensors of STRIDE and represents the impact of a UV photo-electron. In this case the pixel profile of the event is slightly asymmetric in both X (top) and Y (bottom) coordinates. However, when the position detection algorithm of STRIDE calculates the centroid (weighted mean) of the peaks, it uses only pixels above threshold (16 units on the vertical axis). Hence in this case the algorithm sees symmetric pixel distributions and the centroids coincide with the positions of the maxima of the peaks.

Figure 6.17 shows the X-coordinate pixel profile of two distinct UV-events in the same portion of the NMOS sensor. In this case the position detection algorithm sees the asymmetry of the first event even above threshold (manifest asymmetry). Asymmetric peaks are very frequent (about 40% of the total) and are distributed somewhat uniformly. It is important to note that the asymmetry does not depend on the X-coordinate.

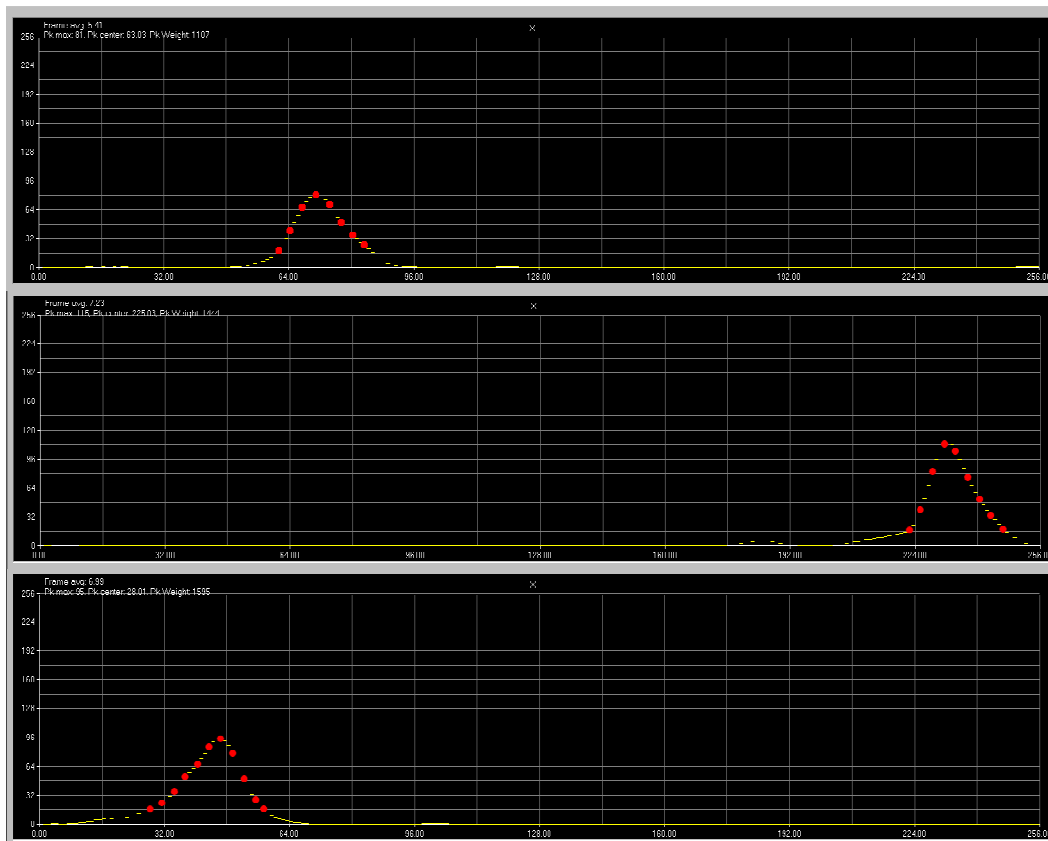




**Figure 6.17** This picture shows the X-coordinate pixel profiles of two distinct events in the same portion of the NMOS sensor. The top one is manifestly asymmetric while the bottom one isn't.

Figure 6.18 shows the pixel X-coordinate outputs of three very asymmetric UV events. To guide the eye, red dots highlight one out of every 3 pixels above threshold. In these cases the distribution of the pixels above threshold are still quite asymmetric and the centroid reconstructed by STRIDE is shifted compared to the position of the maxima.

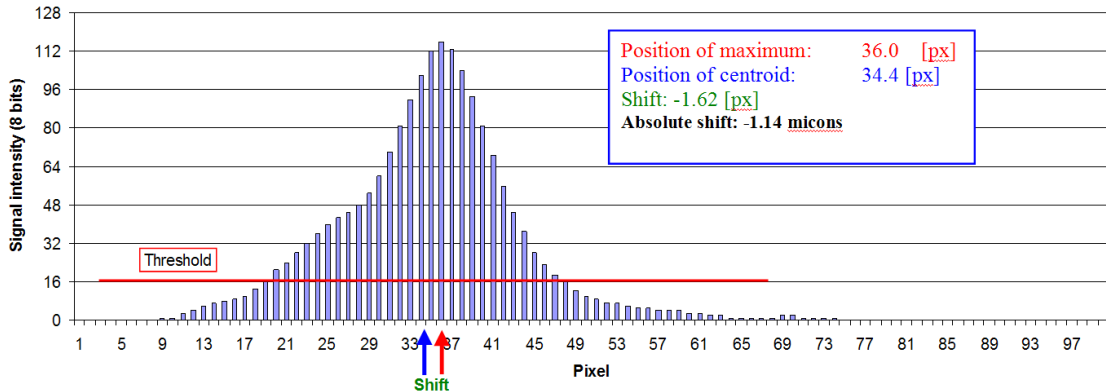
Figure 6.19 shows in detail the pixel profile of a UV event and reports the values of the calculated centroid, the maximum and the shift, namely the difference of the centroid from maximum (*skewness*). In this case the centroid is to the left of the maximum: the shift of -1.6 pixels corresponds to an absolute shift of the X-coordinate of -1.1  $\mu\text{m}$  in the reconstructed image. This shift, statistically meaningless, is nevertheless evocative as it is comparable to the discrepancy in the resolution of our PEEM with the nominal one.



**Figure 6.18** The X-coordinate pixel profiles of three very asymmetric UV events (X coordinates). In these cases the distribution of the pixels above threshold are still quite asymmetric. To guide the eye, red dots highlight one out of every 3 above threshold pixels.

These considerations are preliminary and a more extensive investigation of the pixel profiles of both coordinates is called for, especially to study the correlation between the position of the profile in a coordinate and the skewness of the profile in the other coordinate.

In the IEEM mode this effect could be larger since we have not a single photoelectron emitted by the UV excitation but a cloud of secondary electrons emitted by a single heavy ion impact. This cloud which could be not homogeneously focused on the MCP. The energy distribution of the secondary electrons emitted in an ion impact has a high-energy tail and chromatic aberrations of the IEEM will disperse the occasional energetic electrons out of the cloud causing them to fall asymmetrically on the MCP. This could give rise to an asymmetric excitation of the phosphor.



**Figure 6.19** The pixel contents of an asymmetric UV event that is skewed to the left. The difference between the centroid (blue arrow) and the maximum (red arrow) corresponds to a shift of  $-1 \mu\text{m}$  in the reconstructed image.

Until the cause of the asymmetry is understood and accounted for, it is uncertain if the centroid is the best estimator of the impact position.

## Conclusions

Vibrations and optical distortions are not responsible for the still high value of the spatial resolution and an extensive study of the pixel profile of single events in the PEEM and IEEM modes is needed, in order to investigate the cause of the asymmetry and eventually optimize the algorithm that calculates the position of the light spot. This should improve the resolution of the system.

We will first implement a new feature in STRIDE that will return not only the centroid of each peak, but also the position of the maximum. With such a feature it will be possible to distinguish between events with symmetric pixel profiles and skewed ones.

The resolution studies previously described in this work (correlation peak analysis in Chapter 5) should be repeated to study how the resolution of a given image is affected by using different position estimators.

Further studies of resolution as a function of skewness will allow us to assign a tailored position uncertainty to every event: i.e. the best estimator of the position of a light spot could be assigned on an event-by-event basis, for example by weighing the

centroids and maxima according to where the light spot is detected. In particular images obtained using only events with symmetric pixel distributions will allow us to perform a bench-mark measurement of the PEEM/IEEM resolution with which we will more precisely evaluate other contributions to the degradation of the resolution of the PEEM/IEEM system such vibrations, membrane scattering and SDRAM mapping.

## 7 An IEEM-imaged and time resolved IBICC experiment with a power MOSFET.

### **7.1 Introduction**

In this chapter we describe an Ion Beam Induced Charge Collection (IBICC) type experiment using a power MOSFET device. This experiment was performed together with a research group led by Prof. G. Busatto of the University of Cassino (Italy). The purpose of the experiment was to demonstrate the ability of the IEEM system to associate precise locations in space and time of the ion impacts with the ion-induced effects in the MOSFET devices; i.e. to perform time-resolved IBICC experiments.

In this chapter we discuss in some detail the effects of single ion impacts on power MOSFETs, the need to know the position of the ion impact (hence the motivation to use the IEEM), the experimental setup and finally a time resolved IBICC map.

#### **7.1.1 Power MOSFETs**

As of 1998, the Cassino group studies the effects of heavy ion irradiation on power electronic devices. This research has been performed in collaboration both with INFN and industry (Siemens/Infineon and STMicroelectronics in Catania, Italy) and carried out at many laboratories (INFN Laboratories of Legnaro and Catania and UCL, Louvain-la-Neuve, Belgium).

In particular, the longstanding relationship of the Cassino group with STMicroelectronics has brought the development and systematic experimental study and testing of two types of radiation tolerant power MOSFETs. The group significantly contributed to the identification of causes of Single Event Burnout (SEB) in power MOSFETs, suggested mitigating strategies and tested the new

generation of SEB-tollerant devices that belong to two categories: 100V-Nchannel power MOSFETs and 200V-Nchannel power MOSFETs<sup>24</sup>.

In what follows we describe the experimental setup and the scientific approach used to study SEB in these devices.

It is important to recall and keep in mind that MOSFET devices may manifest Single-Event Gate Rupture (SEGR), another failure mechanism that must be confronted before a device can be considered radiation tolerant.

### **7.1.2 MOSFET irradiation experiments: device, setup and instrumentation**

Figure 7.1 is the photograph of typical power MOSFET ready for irradiation. The die of the device under test, with an area of several square millimeters, is glued on the rhomboid TO-3 package using a silver electro-thermal conductive paste. The conductive glue ensures that the metallic package is at the same potential of the drain electrode (the bottom side metallization of the silicon die), while the gate and source terminals are wire-bonded to the external rheophores (the two blue circles in Figure 7.1).



**Figure 7.1** MOSFET device ready for irradiation. The die is housed a TO-3 package.

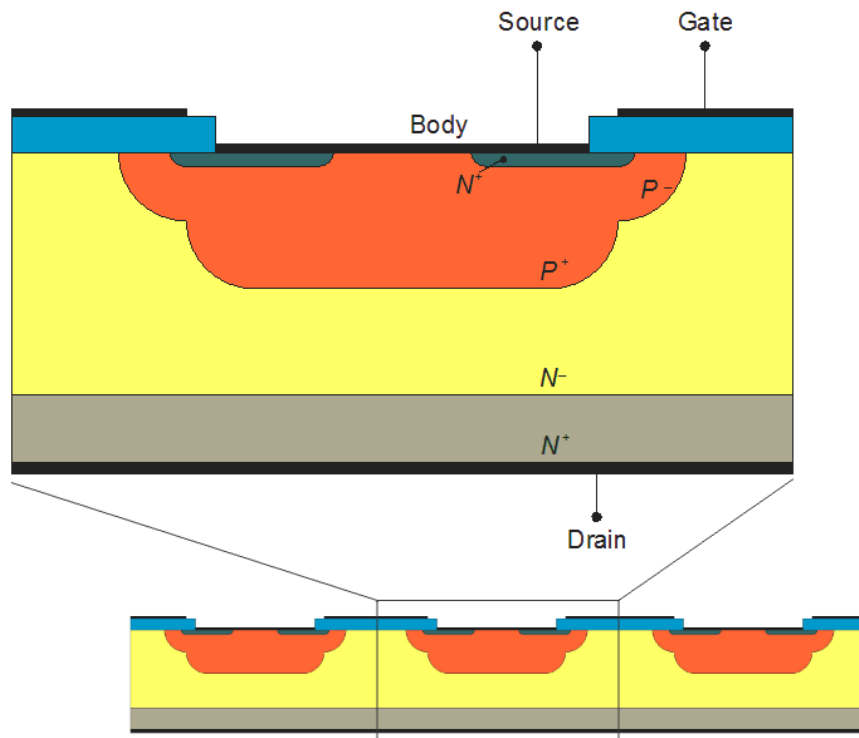
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<sup>24</sup> The work was performed within the GALILEO project (the European GPS project) and commissioned by the European Space Agency (ESA).

Figure 7.2 shows the symmetric structure of the elementary unit cell of the power MOSFET under test. The lateral size of the characteristic objects of the structure shown is of the order of tens of microns. The size of the unit cell in the dimension orthogonal to the page can be accurately thought of as being indefinite. A MOSFET device is made of hundreds of these unit cells.

The different regions of the elementary unit cell are shown in different colors. They are, going from bottom to the top: the drain contact (black); the drain region (light green and yellow); the body or the base region (orange); the source region (dark green); the oxide region (blue); the surface contacts, body-source and gate (black).

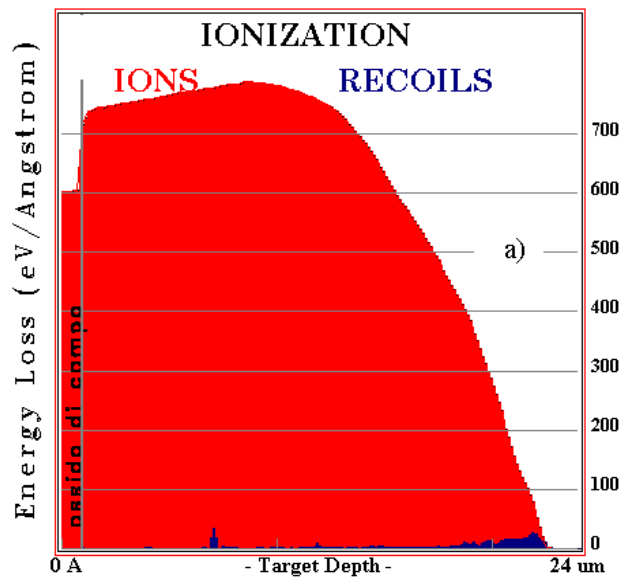
The active volume of the elementary unit cell, the “channel region”, is located in the base region just below the oxide; inside it, a region of electronic states can be formed that conducts electrons.



**Figure 7.2** The internal structure of the elementary unit cell of a power MOSFET. The structure is described in the text.

The device is glued to the TO-3 package on the drain side (the bottom side; see Figure 7.2) so that, during the ion irradiation experiment, the ions impact the device from above.

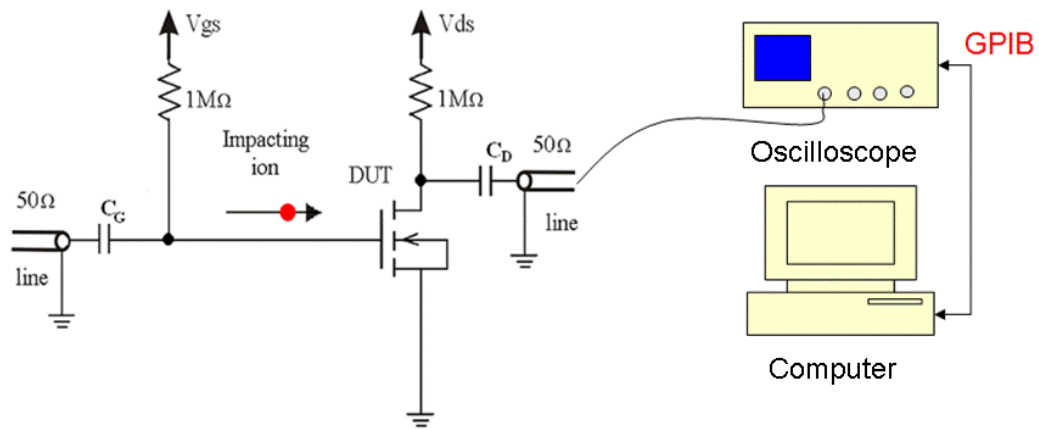
As the ion range and the energy deposit along its path in a given material depend on the ion species and initial energy, we report, as an example, in Figure 7.3 the Linear Energy Transfer (LET), expressed in eV/Å, as a function of ion depth for a 139 MeV  $^{58}\text{Ni}$  ion in bulk silicon with a thin oxide layer. The range is of the order of tens of microns (23 $\mu\text{m}$ , in this case) and this implies that most of the ionization energy loss of the ion occurs inside the impacted unit cell. The figure shown is a standard SRIM output [63].



**Figure 7.3** The LET profile (red) of a 139 MeV  $^{58}\text{Ni}$  ion as it penetrates through a thin silicon oxide layer into bulk silicon.

Before an ion impact occurs the device is OFF (no channel is open): the standard polarization of the device puts the source electrode at the reference potential (ground), the control electrode (gate) at zero potential and the drain electrode at a positive potential. When an ion enters the unit cell, the electron-holes created along the ion track are subject to the electric field inside the device: the electrons move towards the positive electrode, the holes move towards the relatively negative ones. The motion of these charges produces a very short transitory signal on the drain electrode that can be detected and analyzed by an external acquisition system. The characteristics of the signal depend on the parameters of the effective circuit.





**Figure 7.4** The conceptual schematic of the circuit used to test the behaviour of the drain signal of the irradiated MOSFET. The signal waveforms on the drain electrode are acquired and memorized by a fast digital oscilloscope and then computer analyzed.

Figure 7.4 shows the schematic of the circuit used to analyze the drain signal during irradiation. Note that both the drain and gate electrodes are statically polarized (typically  $V_{gs}=0$  e  $V_{ds}>0$ ), but they are capacitively coupled, each with a decoupling capacitor, to two transmission lines that send waveform signals to the acquisition system.

The acquisition system of the drain signal waveform on the drain transmission line is based on a high sampling rate digital oscilloscope (LECROY WavePro WP7100A, 10 M points/Channel). The waveforms are acquired and memorized and computer analyzed (post-processed). The impulses on the gate transmission line are generally uninteresting and are usually ignored. On the other hand the current on the biasing line of the gate is monitored as it is a direct measure of the ion-induced damage to the oxide layer.

In summary, during the experiment all the ion-induced drain waveforms are acquired, as well as the gate bias gate current as a function of time and the ion fluence.

### 7.1.3 MOSFET experiments: typical results

When exposed to heavy ions, MOSFET devices show a threshold behaviour: the activation of a single event damage effect (e.g. SEB) may occur only when certain minimal electrical conditions are imposed.

As an example Figure 7.5 (a) shows some typical ion-induced drain current-pulses of a 200 V MOSFET device for a given ion species and energy (in this case 139 MeV  $^{58}\text{Ni}$  ions): the pulse duration is of the order of tens of nanoseconds and the wave-forms vary in amplitude. For certain electrical conditions (e.g. a certain static drain voltage) one can measure the average integrated charge of the ion-induced drain current-waveforms. Figure 7.5(b) shows the average integrated charge of the drain-waveforms at different static drain voltages for three different types of MOSFET devices. In this experiment the drain-voltage on the devices was increased and the increasing average charge of each device was recorded until it was destroyed by a SEB event (red points in the figure). The particular dependence of the charge with drain-voltage depends on the device type; it also depends on the ion species and energy. For the experimental data shown the gate voltage was kept at the reference value ( $V_{gs} = 0\text{V}$ ).

As can be seen in Figure 7.5(b), for a SEB to occur the drain-voltage must be high enough: for drain-voltages above the threshold value, the probability of a SEB is significant and increases with voltage. For drain-voltages comparable to the breakdown voltage, the probability of destruction approaches certainty; i.e. a SEB will almost certainly occur at the very first ion impact. For voltages below the threshold values the probability of a SEB is negligible and the device can survive the impacts of many ions.

Figure 7.6 shows the typical experimental distribution of the integrated charge of the drain-pulse (dark-blue) for a certain drain voltage. The distribution is composed of two types of event: in this case, there is a large population peaked at 5 pC and a smaller second population with a higher charge (peak at  $\sim 7.5$  pC). The relative size and peak charge of the second population increase with drain-voltage, while the peak charge of the first population does not significantly change. The bimodal form of the experimental distribution can be modelled using two  $\Gamma$ -probability distribution functions (pdf): the light-blue histogram in Figure 7.6 is obtained by generating random numbers from the two  $\Gamma$ -pdfs in an opportune proportion (6 to 1).

Studies performed by the Cassino group have shown, with the help of finite-element simulations, that the second larger-charge population of drain-pulses is due to the transitory activation of a parasitic N-P-N structure inside the MOSFET with a probability of activation that increases with the drain voltage. These studies allowed

the group to propose mitigation strategies that solved the SEB problem by raising the activation threshold of the parasitic transistor in the MOSFET devices.

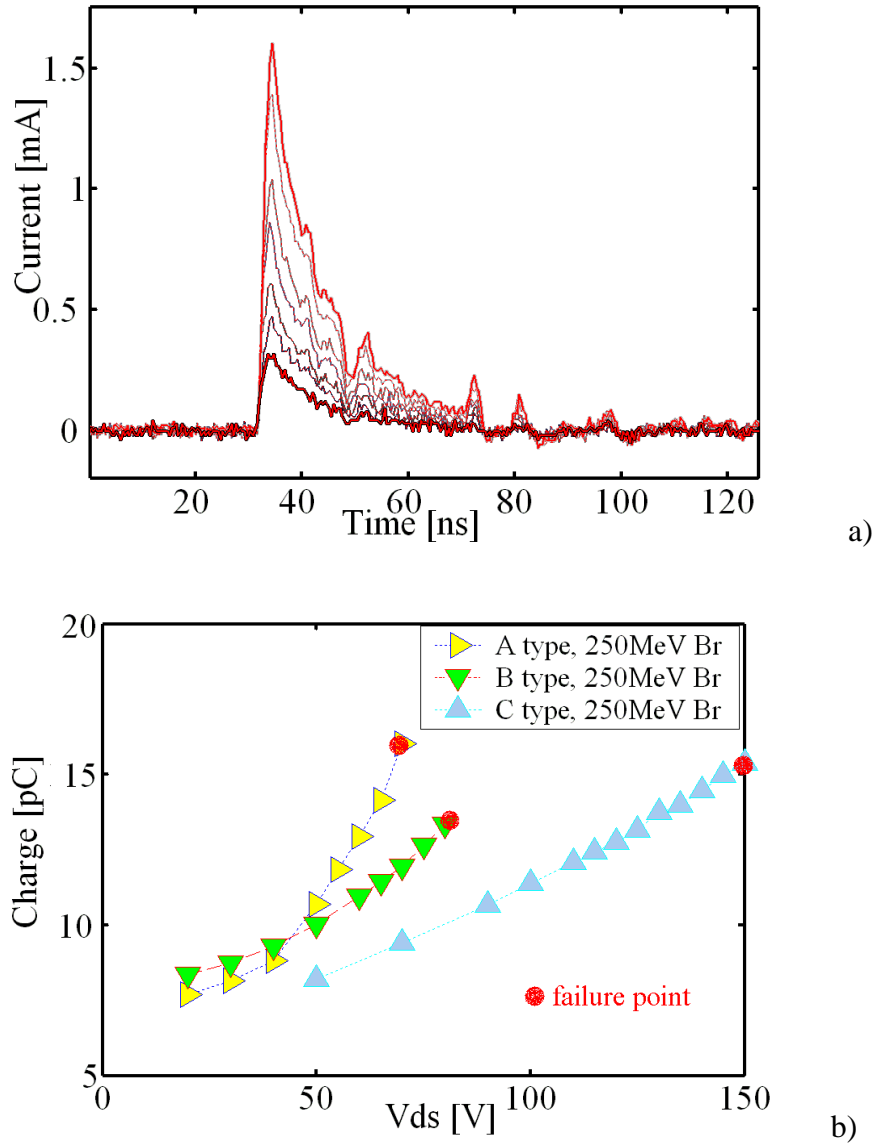


Figure 7.5 a) several overlaid drain-electrode impulses of a 200 V MOSFET impacted by 139 MeV  $^{58}\text{Ni}$  ions. Conditions:  $V_{ds} = 40$  V,  $V_{gs}=0$ V. b) The dependence of the average integrated charge of three device types under test for different drain voltages ( $V_{ds}$ ) with  $V_{gs}=0$ . The red points indicate when the corresponding device was destroyed by SEB.

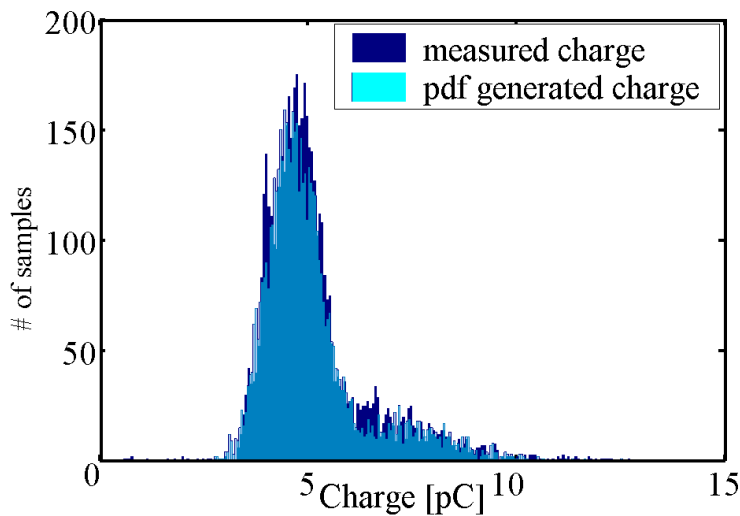


Figure 7.6 In dark blue the experimental distribution of the integrated charge of the current pulses on the drain electrode due to ion impacts for a given drain-voltage. In light blue a numerical distribution composed of two  $\Gamma$ -like populations.

#### 7.1.4 Motivation to obtain ion-impact position information

It must be stressed, at this point, that the SEB problem of power MOSFETs has been extensively discussed over the years and solved. On the contrary, the vulnerability to Single Event Gate Rupture (SEGR) shows several aspects that still need to be further studied.

The rupture of the gate oxide can occur even at reduced drain voltages and with zero or very small gate voltages (few volts). In addition the gate rupture is a delayed phenomenon; it may occur hours after a single ion impact and it is usually accompanied by instabilities (telegraph noise) in the leakage current through the oxide.

To better understand this phenomenon two- and three-dimensional finite-element simulations have been performed over the years to study the effect of a heavy ion impacts in a elementary cell of a MOSFET.

Figure 7.7 shows the *mix-mode circuit* of the device; i.e. part is finite-element (the elementary cell of the MOSFET) while part is with discrete components. The discrete part accounts for the parasitic effects of the package and the connections of the device to the external world. Three ion trajectories are considered (shown in the figure as dashed lines): (a) at the centre of elementary cell (neck region); (b) at the

drain-side edge of the conductive channel; (c) at the source-side of the conductive channel.

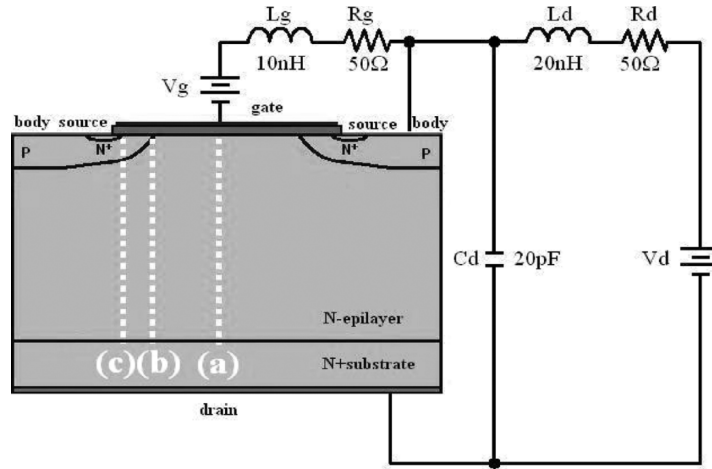


Figure 7.7 Mixed-mode circuit used for the finite-element analysis. The dashed lines represent three trajectories of incident ions. The discrete part accounts for parasitic effects due to the package and real-world connections.

The goal of simulations is to study the electrical connections (static and dynamic) and the characteristics of the incident ion (species, energy, position of impact) that cause significant stress to the oxide layer. To model the effect of a 139 MeV  $^{58}\text{Ni}$  ion impact, a charge of a few pC is deposited along a trajectory with a longitudinal dependence given by the LET-vs-depth distribution shown in Figure 7.3.

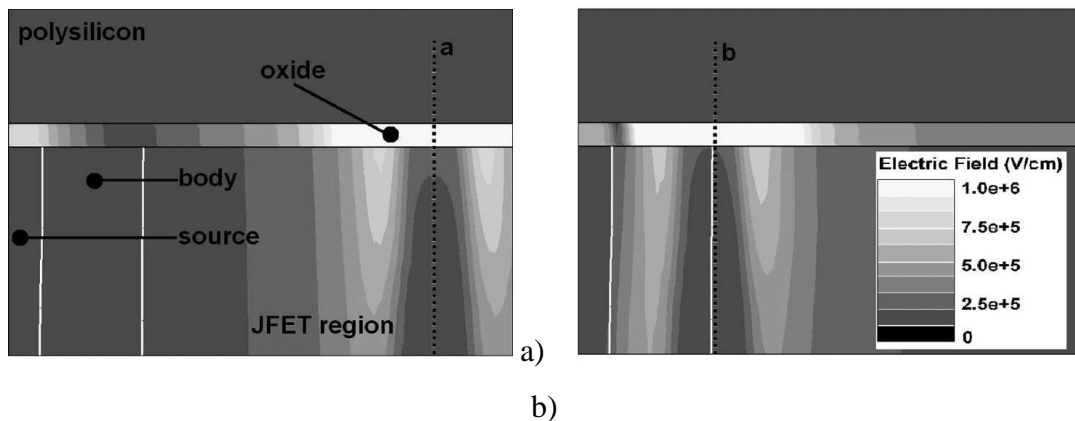
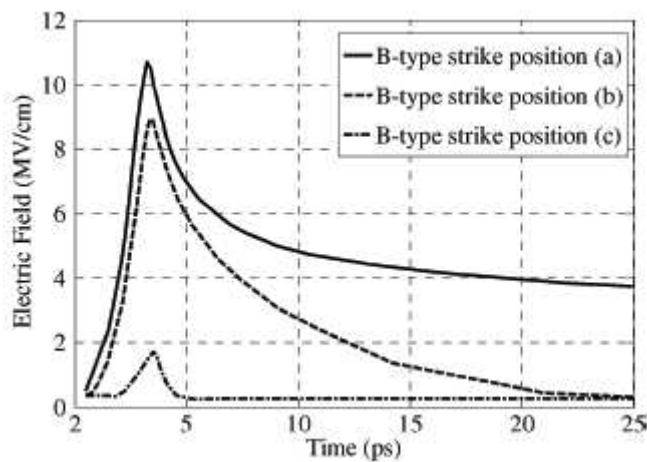


Figure 7.8 2D distribution of the electric field inside the device at the instant of maximum electric stress, a few picoseconds after an ion impact. a): ion trajectory (a) of Figure 7.7. b): ion trajectory (b).

Figure 7.8(a) and 9.8(b) show the 2D distribution of the electric field inside the device at the instant of maximum electric stress, a few picoseconds after the modelled ion impact, along the trajectories (a) and (b) shown in Figure 7.7 [64]. As one can see from the figure, the simulated electric field reaches  $10^6$  V/cm inside the oxide layer, in correspondence to the impact point of the ion, above the neck region (a), or above the channel region (b). Such values of electric field, close to the dielectric strength<sup>25</sup> of the SiO<sub>2</sub> may favour the formation of a permanent damage to the structure of the oxide. This is at present the best theory to explain the damage of the oxide layer during ion irradiation. Unfortunately the finite-element simulations are limited as they do not implement the local ion-induced breakdown mechanism of an oxide layer (a stochastic phenomenon). For this reason the formulation of a definitive model of the oxide damage and eventually the SEGR breakdown is not yet reached.

Figure 7.9 shows the time dependence of the maximum electric field for the three ion impact points shown in Figure 7.7. The effect of the impact position is very significant: the peak of the E-field is higher when the ion impacts the centre of the elementary cell (point a, the neck region).



**Figure 7.9** The time dependence of the maximum electric field for the three ion impact positions shown in Figure 7.7.

The simulations have only been partially successful: they gave important results, like showing that SEGR has a strong dependence on the impact position of the ion,

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<sup>25</sup> The maximum electric field an insulating material can withstand without breaking down.

but they also proved to be limited by the great difficulty to model the oxide layer and the phenomena that take place in it. The oxide layer may manifest percolative damage (that is, a constant and significant leakage current), or multi-hop quantum tunnelling effects that show a threshold behaviour and that degenerate with time. In addition, the holes in the oxide have a very small mobility (of the order of a micron/year) and they may accumulate, especially at the interface with the underlying semiconductor, and alter its conductivity.

The phenomenology of the damage to the oxide layer is complex and experimentally varied. Figure 7.10(a) shows the behaviour of the gate leakage current of a non-irradiated device under static polarization while Figure 7.10(b) shows the post-irradiation time dependence of the gate leakage of a device just after it has been exposed to 30 ion impacts. The leakage current of the irradiated device is not only higher and noisier, but it worsens over a time scale of an hour with peculiar characteristics:

- the leakage current does not increase continuously but gets worse in discrete jumps;
- the amount of the current jump and the instant it occurs are not predictable (stochastic);
- the noise of the leakage current is telegraphic (stochastic spikes);
- the peak-to-peak noise amplitude increases with the leakage current (the noise worsens for each new discrete jump);
- the process is irreversible (no annealing) and the oxide is permanently damaged.

To further complicate the phenomenon, it sometimes happens that the post-irradiation time dependence of the gate leakage current is almost linear (Figure 7.11), until a sudden catastrophic failure of the gate occurs: the leakage current goes out of control and the gate, for all practical purposes, is short-circuited.

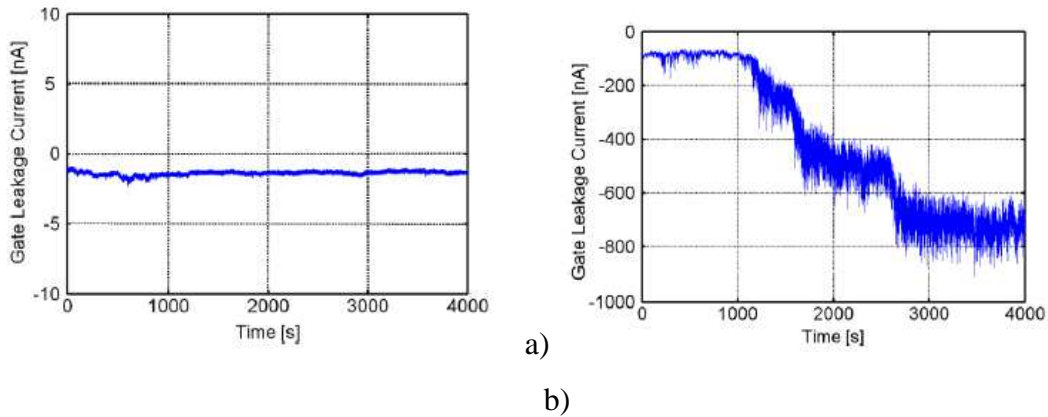


Figure 7.10 a) The time dependence of the gate leakage current of a non-irradiated (fresh) device. b) The post-irradiation time dependence of the gate leakage current just after exposure to 30 ions.

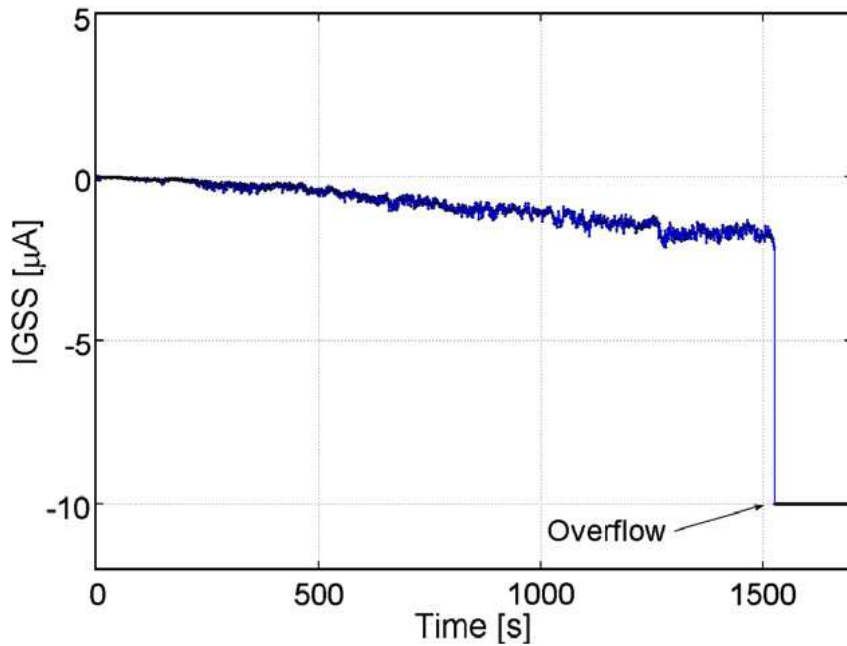


Figure 7.11 The post-irradiation gate leakage of an irradiated device that shows an unpredictable catastrophic failure of the gate oxide (the current is out of control).

This experimental behaviour leads to the theory of *latent gate oxide damages* [65]. The oxide layer stressed by the high electric field is not destructively damaged: only a very localized region (few Å) of the oxide is weakened. This weakened region gradually degenerates until high values of leakage or until breakdown. In this hypothesis, the stochastic behaviour can be due to:

- the position of the ion impact respect to the elementary cell;
- the impact of a new ion near a region weakened by a previous ion impact.



In this confusing setting, it is clearly very useful to have an experimental system to recognize the impact point of a heavy ion in an elementary cell with a precision of at least a few microns.

Energetic heavy ion microbeams are very useful, but are not easy to come by.

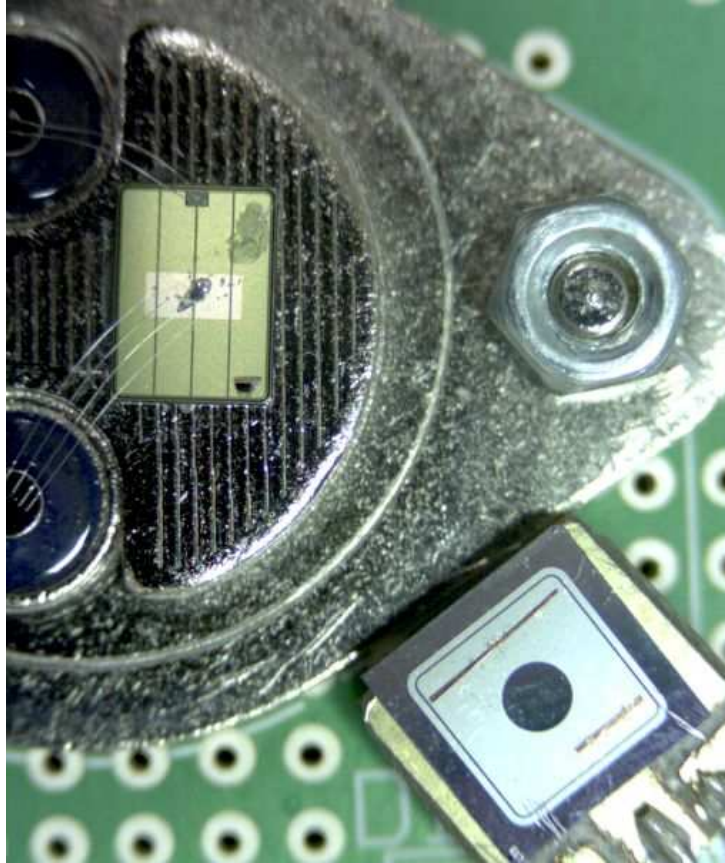
The availability of the IEEM has now opened up new interesting opportunities.

### **7.1.5 The IEEM experiment**

The first step when using the IEEM of the SIRAD facility is to adapt the device under study (DUT) to the mechanical and electrical constraints of the IEEM system. However the volume of the experimental vacuum chamber is enough to accommodate large devices and electronic boards.

The most important constraint of the IEEM system is the need to minimize the distance of the DUT from the ultra-thin Au-Si<sub>3</sub>N<sub>4</sub> membrane. In practice this means that ideally the DUT should be the closest object to the plane of the membrane; i.e. no feature of the device board with any ancillary electronics should stick out more than the surface of the DUT. In many cases this is not possible, for example: the wire bonds that connect the DUT to the board cannot be removed or arbitrarily shortened. Therefore the distance between the membrane and the DUT has to be adjusted to accommodate the bonds. In this experiment the distance of the MOSFET from the ultra-thin Au-Si<sub>3</sub>N<sub>4</sub> membrane was comfortably set at 0.8 mm.

Figure 7.12 shows the MOSFET with its TO-3 package mounted on a board we purposely designed for the IEEM experiment. Two gate micro-wires from the top rheophore are bonded to a small rectangular pad visible at the top of the MOSFET; four source wires from the bottom rheophore are bonded to the centre of the MOSFET (the backside drain connection is made inside the TO-3 package). The figure also shows the PIN diode we use to perform beam setup.



**Figure 7.12** A photograph of the MOSFET with its TO-3 package mounted the test board. A PIN diode (bottom right) with reference copper strips on top is used for beam setup and for determining reference positions.

The beam setup procedure consists in moving the PIN diode into the field of view of the IEEM. The beam transport is verified and adjusted: ion flux is set and the beam quality (mono-chromaticity) is checked. We recall that the diode has small copper strips placed on top that partially screen the sensitive area (Figure 7.12); a IEEM sensitivity map of diode is made (see Chapter 5) and the extremities of the copper strips are used as reference points that are needed to identify points of interest on the MOSFET.

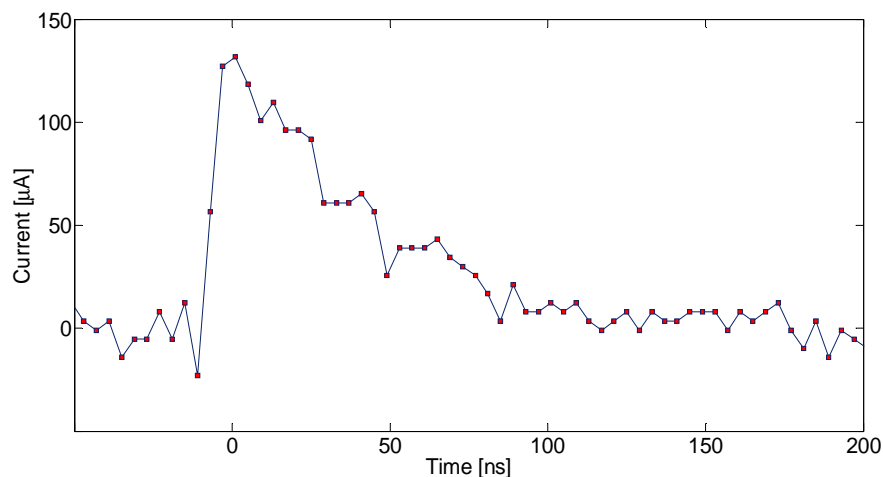
We performed the experiment using 223 MeV  $^{79}\text{Br}$  ions. To image the copper strips on the PIN diode, we use a high flux of  $\sim 1000$  ions/s in the field of view of the IEEM. Once the copper reference points were reconstructed, the ion flux was lowered to  $\sim 20$  ions/s in the IEEM field of view. The beam was then interrupted while the MOSFET was moved into the field of view.

The MOSFET drain-source voltage  $V_{ds}$  was initially set to 10 V, a cautionary value low enough to avoid large destructive effects.

Current transients on the drain of the MOSFET, above an adjustable threshold, were used to generate LVDS signals that were used by STRIDE to tag the ion impact signals. Figure 7.13 shows a typical wave-form. The threshold was set at  $V_{th} = 6$  mV over  $50 \Omega$  (corresponding to a peak current of  $120 \mu\text{A}$ ).

At this voltage only the drain signals of the areas of the MOSFET where the electrical field is the highest are above threshold and can tag STRIDE events. Therefore ions that strike the gate distribution line and the polysilicon fingers shown in Figure 7.14(a) cannot produce drain-transients above threshold as expected by the model discussed in 9.1.5 (see Figure 7.7 and Figure 7.8). The STRIDE events tagged by above threshold drain signals quickly built up a sensitivity map in real time, allowing us to immediately recognize the sensitive areas: the metal lines of the source contacts (Figure 7.14(b)).

Figure 7.15(a) shows the map of tagged IEEM ion impacts: the gate distribution line and the polysilicon fingers are evident. Events were also analyzed off line searching for time coincidences between the drain recorded signal set and the STRIDE event one in a 106 ms window (the readout time of STRIDE) . Figure 7.15(b) shows the subset of the tagged IEEM events of 9.15(a) time correlated with the drain signals.



**Figure 7.13** A drain-waveform with  $V_{ds} = 10$  V due to an 223 MeV  $^{79}\text{Br}$  ion. The signal is above the tagging threshold of  $V_{th} = 6$  mV and was used to tag a STRIDE event.

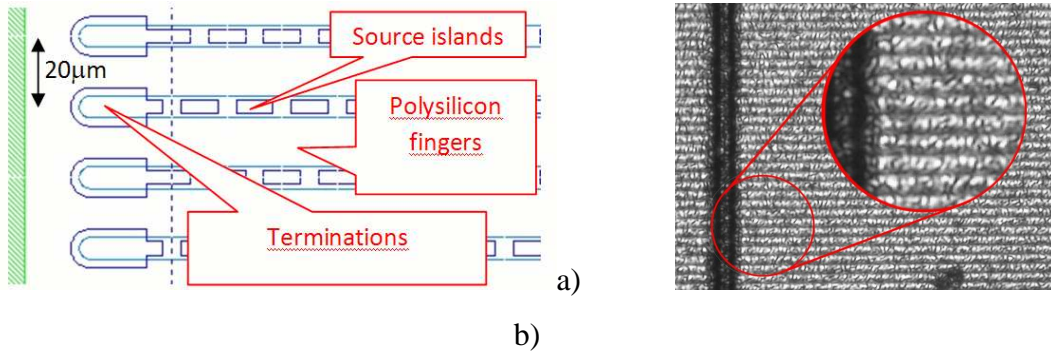


Figure 7.14 a) Layout of the 200 V power MOSFET used in this experiment. b) Microphotograph of the metalized surface of the device. In the circle the detail of the surface metallization at the edge of the gate distribution line (the thick vertical line). The horizontal thin white lines correspond to the polysilicon fingers.

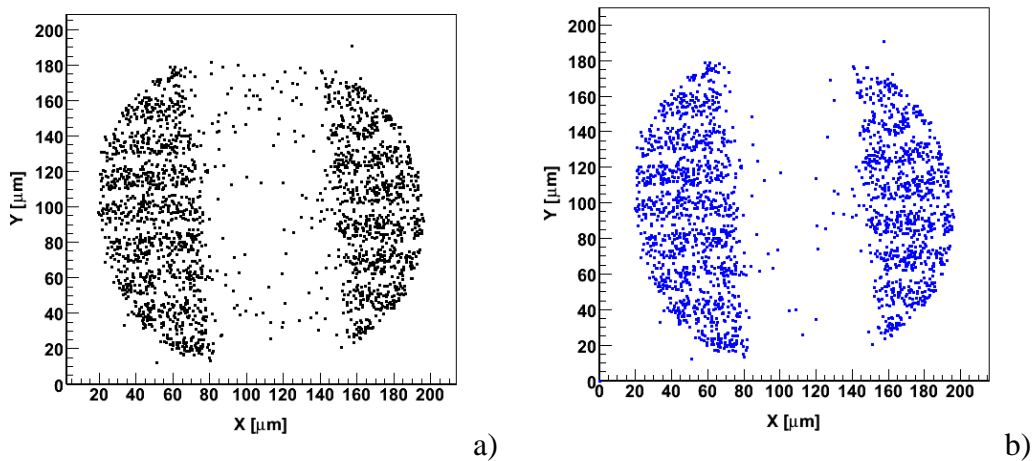


Figure 7.15 a) On line image with the tagged STRIDE events (2333 events). The gate distribution line and the polysilicon fingers are evident. b) The events of (a) that are time-correlated with an above threshold drain signal (off-line analysis).

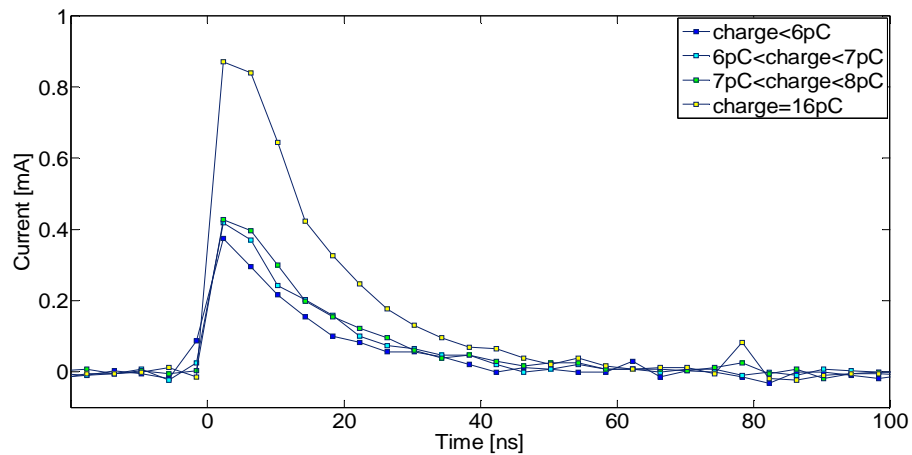
The numbers of recorded drain signals, of tagged STRIDE events and of their coincidences are summarized in the following table:

Drain signals over threshold	Tagged STRIDE events	Coincidences
3691	2333	2235

The fraction of the tagged STRIDE events that are in coincidence with a LeCroy drain-waveform is 95.8%; the fraction of LeCroy drain-waveforms that are found to be in coincidence with a STRIDE event is 61%. Of the tagged STRIDE events, a small number of events (123) are not found among the events saved by the digital

oscilloscope. A fraction of the drain-current transients above threshold (that tag the STRIDE events) are not recorded by the LeCroy oscilloscope. This occurs when the buffer memory of the LeCroy is full and the buffered wave-forms are copied to the hard disk drive; during the writing time the oscilloscope does not save new waveforms, but the trigger continues to work and STRIDE continues to acquire tagged events.

Once the interesting region of the MOSFET was recognized and the tagging system verified, the working voltage of the MOSFET was raised from the 10 V cautionary value to a more realistic and hence interesting value (70 V). The drain-waveforms were now correspondingly more robust: Figure 7.16 shows waveforms recorded by the LeCroy digital oscilloscope when exposed to the 223 MeV  $^{79}\text{Br}$  ions (the figure also reports the integrated charge). In these working conditions almost all the STRIDE events are tagged and an online sensitivity mapping does not show any features as all the drain signals are now over threshold.

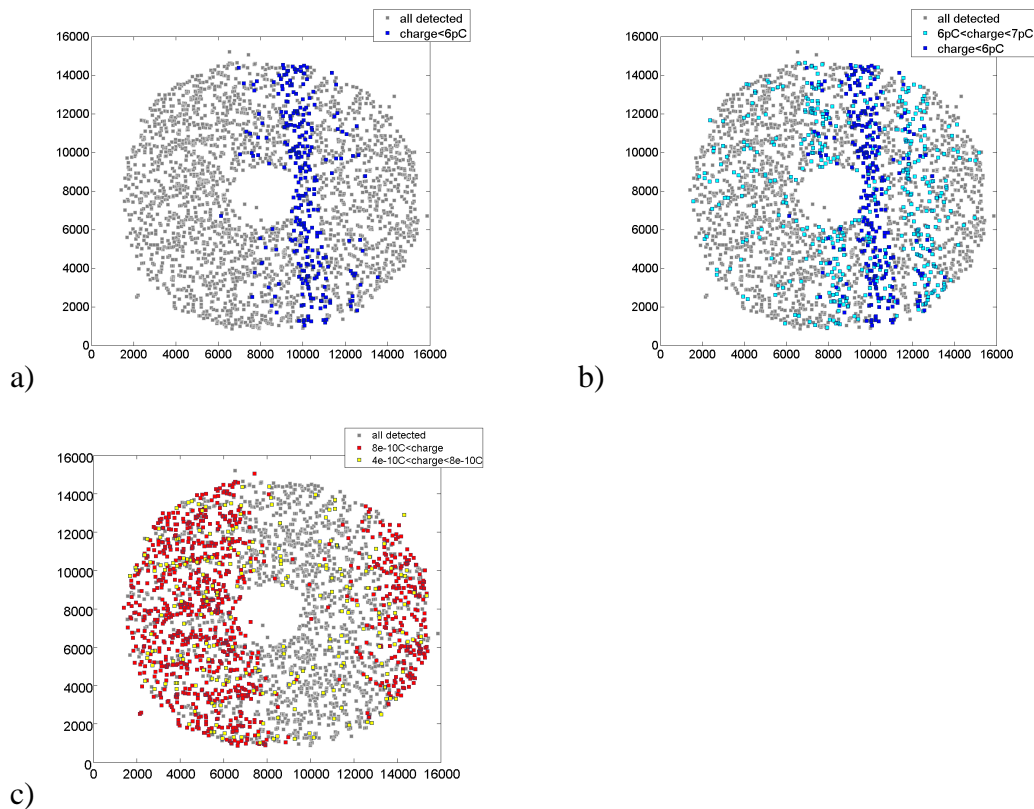


**Figure 7.16** Four 223 MeV  $^{79}\text{Br}$  ion induced drain-waveforms recorded during the experiment. All four transients generated a tag signal.

The off-line time-correlation analysis of drain signals and STRIDE events has been performed as a function of the integrated charge of the drain-waveforms. The evolution of the STRIDE image is reported in Figure 7.17 from (a) to (c) for different charge intervals and  $V_{ds}=70$  V. The distribution of events with integrated charge < 6pC of Figure 7.17(a) shows the gate distribution line already observed in Figure 7.15. However the line is heavily shrunk. Figure 7.17(b) shows that the events with integrated charge between 6 pC and 7 pC come to populate two bands parallel to that

observed in Figure 7.17(a). These three bands almost recover the area of the gate distribution line of Figure 7.15, but they are clearly separated among them indicating a threefold structure of the electrical field below the gate. All this structure becomes insensitive when only high charge events are selected (Figure 7.17(c)). The gate-contact polysilicon lines are still discernible as areas of small drain signals.

Data must be further analyzed and compared with careful simulations of the MOSFET. By the way these first results demonstrate the capability of the IEEM system to provide in-deep information of the structure of state-of-the-art electronic devices.



**Figure 7.17** Reconstructed positions of ion impacts; for different charge pulses induced in the drain terminal: small charges (a) ,medium (b) and large charges (c). Arbitrary units on the axes.



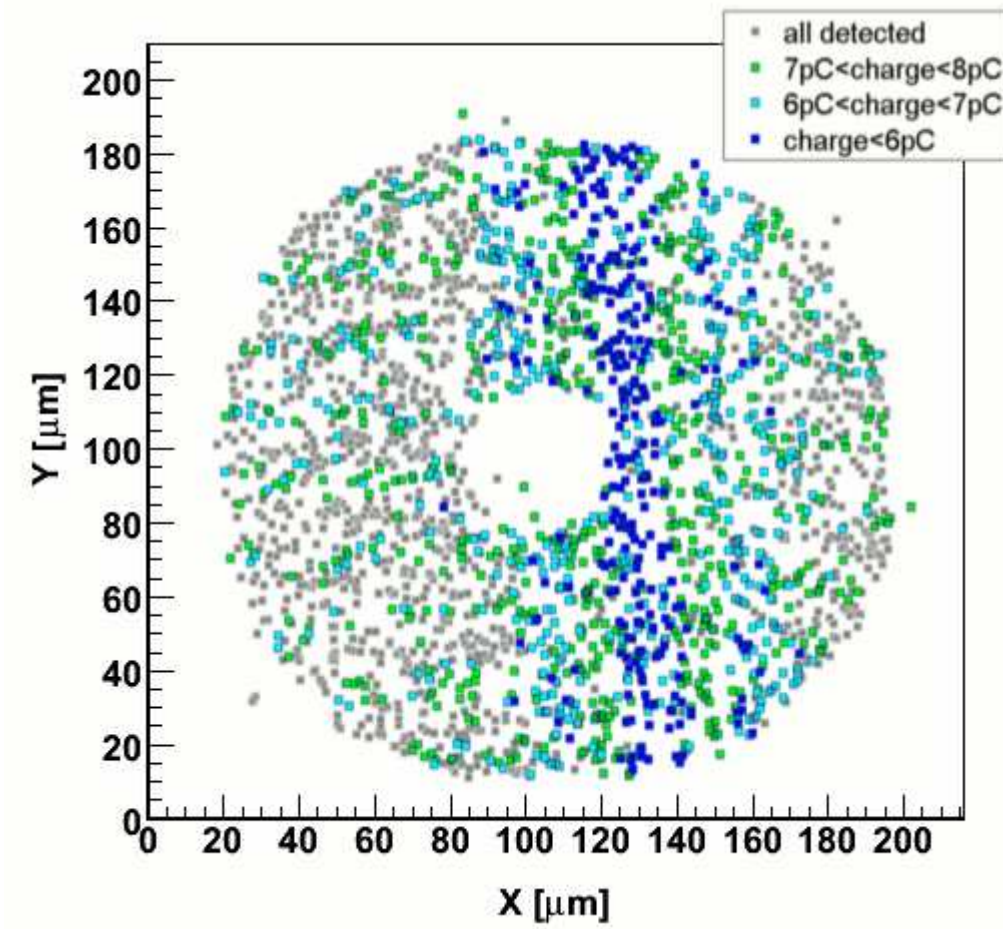


Figure 7.18 Reconstructed positions of ion impacts; the different colours accounts for different charge pulses induced in the drain terminal.

This preliminary experiment demonstrates the ability of the IEEM system to study ion-induced charge collection effects.





## 8 SOI Imager Shift Register SEU map

### 8.1 *Introduction*

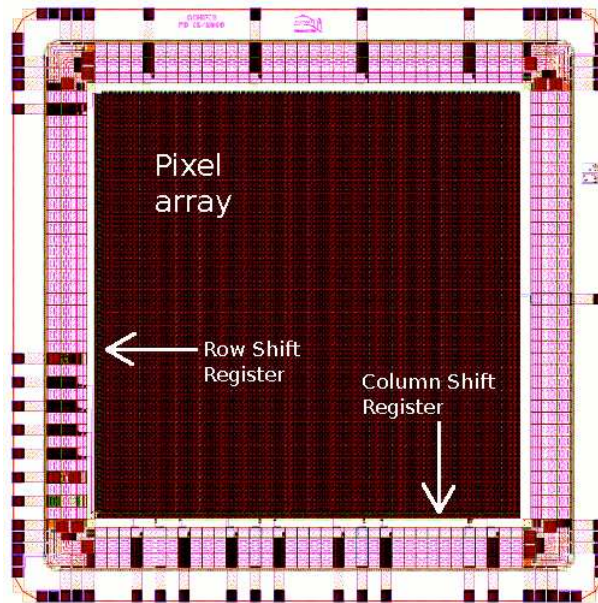
The SOI Imager is a prototype monolithic pixel detector for charged particle detection and imaging applications, designed and fabricated using a commercially, deep-submicron Silicon-On-Insulator (SOI) process, in a 0.20  $\mu\text{m}$  technology [66]. In this process, a buried oxide layer (BOX) is employed to insulate a thin layer of integrated full CMOS electronics from a high-resistivity substrate. The substrate allows pixel implanting and reverse biasing and is contacted from the electronics layer through vias etched in the buried oxide. The sensitivity to SEUs of the whole chip is high, because at this stage of the project no caution by design was adopted to limit it. In this way the chip is a good test bench to measure the performances of the IEEM in mapping the Single Event Upset (SEU) sensitivity.

### 8.2 *SOI Imager Shift Register*

The IEEM system was recently used to map the sensitivity to SEU of the Shift Register (SR) of the SOI Imager chip (the schematic in Figure 8.1; a microphotograph in Figure 8.2).

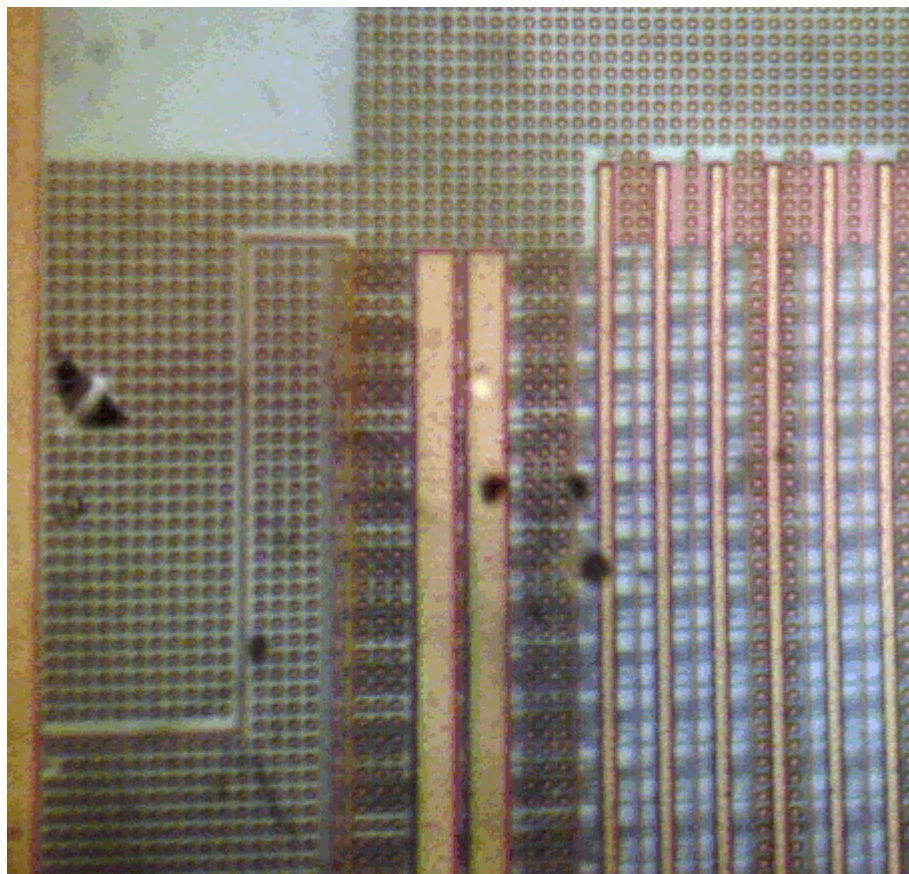
In this chip, the sensitive area is a  $3.5 \times 3.5 \text{ mm}^2$  array of  $256 \times 256$  equally spaced pixels (13.75  $\mu\text{m}$  pitch) driven in a standard serial readout scheme. To increase the readout speed, the pixel matrix is divided into 4 parallel arrays of 64 columns each connected to 4 identical parallel output analog stages, external to the pixel matrix. Besides the analog stages, in the periphery of the pixel matrix the electronics for row and column selection is also implemented. Five SR are used to access one by one the

256×256 pixels in which the sensitive area is partitioned: one SR is for the rows addressing and four SR (one for each sector) for the columns addressing; they consist of a chain of cells (256 for the row SR and 64 for the column SR), each connected to one row (column) of the pixel array.



**Figure 8.1** Layout of the SOI-Imager chip. The position of the row and column SR is marked by the arrows.

During the readout operation, all the cells of the SR are in the same inactive logic state, except one, which activates the relative row (column). At every clock cycle, the active column-SR cell deactivates, inducing the activation of the subsequent one. The process continues until the deactivation of the last cell that re-initializes the activation succession from the first column in the column-SR. At the same time a pulse signal is sent at the clock gate of the row-SR that selects a new row. In this way the whole sensitive area of the sensor is read in a line-by-line fashion.



**Figure 8.2** Microphotograph of the upper portion of the SR of the SOI-Imager chip. The cells of the SR are hidden below the two thick vertical metallisation lines at the centre. On the right the pixel array of the Imager is visible. During the experiments the pixels were shielded and not exposed to the ion beam.

### **8.3** *SEU global cross section measurement*

With respect to SEU, SOI devices were traditionally considered more radiation hardened than the ones manufactured in standard bulk CMOS technology. In fact the charge collection volume was assumed to be much smaller, as only carriers generated in the top thin silicon layer were believed to contribute to the charge induction build-up. In the past, SEU tests seemed to support this assumption [2]. Most recently, new SEU tests on SOI static random access memories (with BOX thicknesses less than 200 nm) showed unexpectedly high SEU cross-sections [3]. This can be correlated to Ion Beam Induced Charge Collection (IBICC) measurements which revealed that the amount of induced charge is much larger than just the charge deposited onto the top silicon layer above the BOX [4][5]. There is a clear indication that charge induction,

at least for some technologies, occurs not only when the carriers move in the top silicon layer but also when they move below the BOX. These considerations show that a detailed study of the behavior of SOI pixels is required in order to measure their effective SEU sensitivity, assess their application limits in radiation environments and to define a possible R&D path towards radiation tolerant sensors.

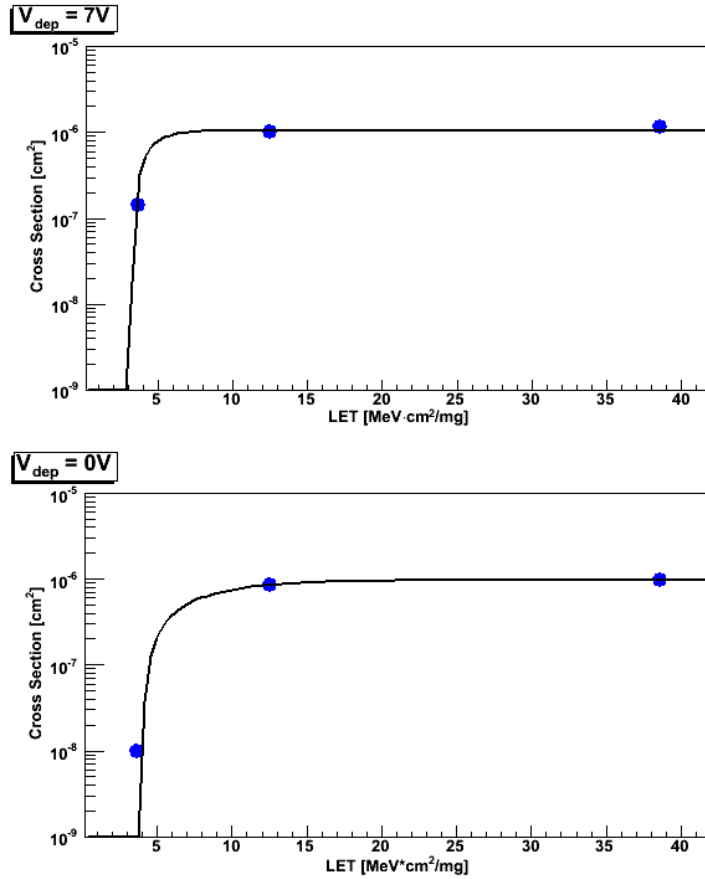
The SEU cross section has been measured for the SOI-Imager chip at the SIRAD broad-beam irradiation facility (sez. 4.5). In our prototype chip, the row-SR is provided with pad connections to control it independently from the rest of the chip and to monitor the output activity. A microcontroller is used to drive the SR and read its output with a 125 kHz clock frequency. The pattern loaded in the SR is a sequence of 255 cells at “0” and only one cell at “1”, the only one allowed by design (an arbitrary sequence cannot be written). Once completely loaded, the SR was exposed to heavy ion irradiation and its content read-out. Any logic value which differed from the loaded one was assumed to be caused by a SEU that occurred in the cells. Irradiations were performed using three different ions in the order of decreasing LET ( $^{79}\text{Br}$ ,  $^{35}\text{Cl}$ , then  $^{19}\text{F}$ ; see Table 10.1). For each ion beam, two irradiations were made: one with substrate bias conditions  $V_{\text{bias}} = 0 \text{ V}$  (i.e. no bias applied to the detector) and one with  $V_{\text{bias}} = 7 \text{ V}$  ( $\sim 20 \mu\text{m}$  of depletion depth in the substrate). For all ion beams, the maximum of ionization (the Bragg peak) occurs in the high resistivity bulk, below the BOX.

Ion species	Energy (MeV)	Range in Si ( $\mu\text{m}$ )	LET <sub>0</sub> in Si (MeV·cm <sup>2</sup> /mg)
$^{19}\text{F}$	118	93	3.67
$^{35}\text{Cl}$	170	49	12.5
$^{79}\text{Br}$	240	32	38.6

**Table 8.1 Energy, range in Silicon and surface LET values for the ion species used in the global irradiation experiment.**

In this experiment no “1” → “0” were detected, while  $\sim 66\%$  of the times the SR was readout a “0” → “1” transition was detected. As only one cell of the SR is in the logic state “1”, the transitions from the logic state “1” to the logic state “0” are rare compared to the “0” → “1” transitions. Due to lack of statistics we cannot state that

the SEU probability might depend on the logic state of the irradiated cell. Fear for possible total dose effects has drastically limited the collected statistics.



**Figure 8.3** SEU cross section measurements of the SOI-Imager with bias (top) and with no bias (bottom) applied to the detector. Circles are experimental data, the continuous line is the Weibull fit [6].

The measured SEU cross sections are shown in Figure 8.3 for the two bias conditions previously described. No significant differences can be observed in the LET threshold ( $LET_{thr} \sim 4 \text{ MeV cm}^2/\text{mg}$ ), nor in the saturated cross section ( $\sigma_{sat} \sim 10^{-6} \text{ cm}^2$ ). However, the same chip was used for all the irradiations and the total dose damage, up to 140 kRad at the end of the irradiation, cannot be neglected. At the end of the irradiation, pixels exposed to the ion beam show a significantly higher noise level than the non-exposed pixels, due to an increase in the leakage current. We also noticed that the device supply current also increased, and we couldn't apply a  $V_{bias} >$

1 V, confirming that total dose effects were turned on (high leakage current in the transistors).

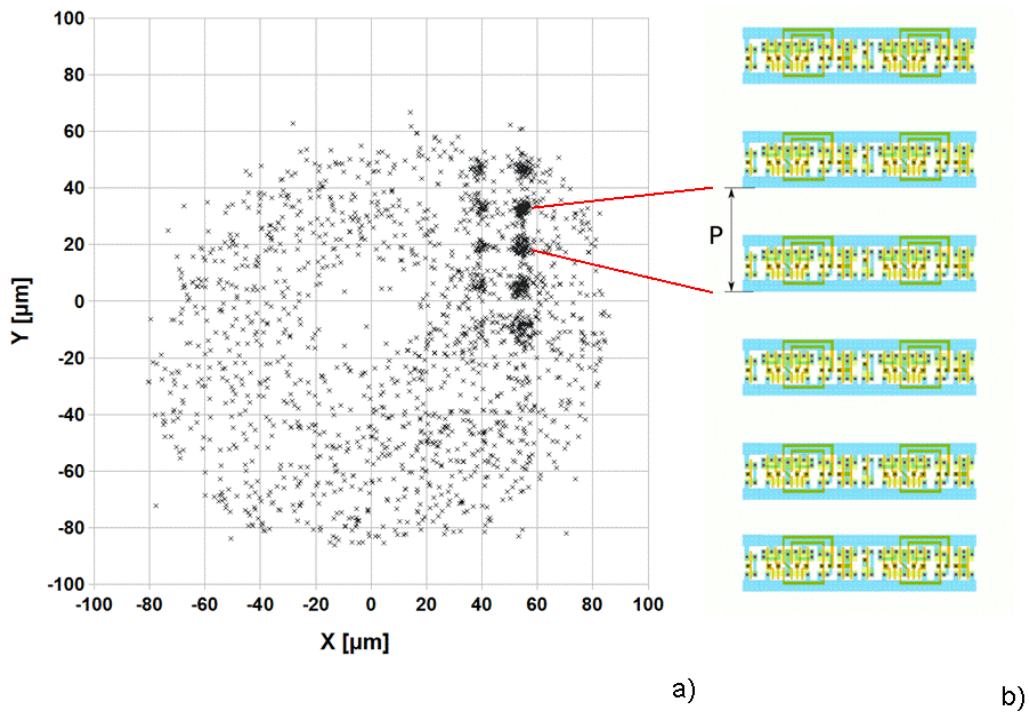
In evaluating the above results, it must be recalled that the chip was designed with no radiation tolerance in mind at all, so it does not sport any specific hardening toward both total dose and single event upset. On the contrary, this feature was crucial to get unambiguous evidence that the SOI technology is very sensitive to single high charge depositions below a 200 nm BOX.

## 8.4 *SEU micro-mapping*

The SIRAD IEEM system was used to map the sensitivity to Single Event Upset (SEU) of the Shift Register (SR) of the SOI-Imager detector. The row shift register (below the vertical metallization lines of Figure 8.2) was positioned in the field of view of the IEEM using the standard copper-profile reference point technique described in Chapter 7. A microcontroller was used to drive and readout the SR. In this experiment the chip was placed at a distance of  $\sim 450 \mu\text{m}$  from the ultra-thin Au-Si<sub>3</sub>N<sub>4</sub> membrane, and was irradiated with a 241 MeV <sup>79</sup>Br ion beam. The ion impact rate used in the experiment was 1 kHz.

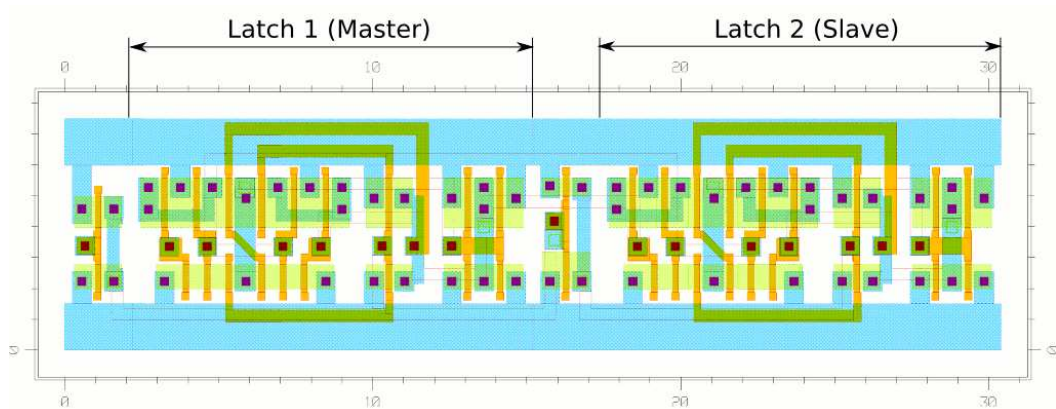
In the absence of upsets, we expect to find the SR output in the inactive state (“0”) during the first 255 clock pulses following the initialization procedure and to find it in an active state (“1”) only during the next clock pulse, which closes the readout process and re-initializes the device. When ever an upset is found in the readout sequence, the microcontroller enables the flag signal delivered to STRIDE for 10 ms; during this period, all the events detected by the DAQ are flagged. During offline analysis, the flag signal is used to select all the ions previously recorded by the IEEM system in a time-interval of 2 ms: the readout time of the whole register. The impact positions of all these selected ions feed a histogram used to plot the SEU map (Figure 8.4).





**Figure 8.4** a) Ion impact position of all the ions detected by the IEEM system in a time-interval of 2 ms prior the readout of an upset in Shift Register. b) Schematic layout of the SOI shift register. The nominal pitch  $P = 13.75 \mu\text{m}$ , the measured value is  $13.9 \pm 0.5 \mu\text{m}$ .

In Figure 8.4-a) the SR SEU map is represented: four pairs of hot spots are clearly visible (the rest of the device in the field of view is masked by a misalignment of the membrane window). Each pair corresponds to a single SR cell and the two spots highlight the two Flip-Flop D structure of the cell (Figure 8.5).



**Figure 8.5** Layout of the design of one SR cell; the position of the Master and Slave latch is shown.

The different number of upsets in the two columns is due to the fact that, although the two Flip-Flop are identical, the logical states are not: the Slave Flip-Flop is always complimentary to the Master Flip-Flop.

The distance among the centroids of the four pairs amounts to  $13.9 \pm 0.5 \mu\text{m}$  and  $15.1 \pm 0.5 \mu\text{m}$ , in the Y and X axis of Figure 8 respectively, to be compared to the  $13.75 \mu\text{m}$  and  $15.2 \mu\text{m}$  design values (Figure 8.4-b). The spots show a Gaussian distribution ( $\sigma \sim 2.5 \mu\text{m}$ ). The present resolution of the IEEM does not allow us to untangle the most sensitive nodes inside the cell (we cannot say what transistor is responsible for an upset), but it is sufficient to distinguish the two Flip-Flops and characterize their relative sensitivity: the Master Flip-Flop is  $2.6 \pm 0.1$  times more sensitive than the Slave.



## Conclusions

The SIRAD axial IEEM is now a mature system and we have entered a new phase. The experience with the SDRAM diagnostic system was very important; having to solve many and diverse problems (from mechanical to electronic) allowed us then to be able to quickly change focus and gears and finally perform original and interesting experiments, such as the one with the power MOSFET. A new vigorous collaboration with the Cassino group has begun and new IEEM experiments are planned. The issue of the effective resolution of the IEEM needs more work but it was very important for us to prove, to avoid chasing a red herring, that the SDRAM needs to be completely mapped. However at this point a far more interesting option is to change the type of pixelated device to measure the resolution. We have already begun a collaboration with a group with the Department of Information Engineering (DEI) of the University of Padova that studies the effects of single ion impacts in FLASH devices. The resolution degradation studies were successful as they point the way for effective upgrades, for example the STRIDE firmware must be changed to allow the possibility to improve the position estimator off-line. We are confident we can measure and somewhat improve the resolution with minor changes, but we also strongly feel that the best strategy is to make the IEEM system more flexible, user friendly and hence an attractive tool to users.

One way to make the IEEM system much more flexible is already under design: the ultra-thin Au-Si<sub>3</sub>N<sub>4</sub> membrane will be used to partition space into two volumes: a high vacuum portion with the IEEM, and a low vacuum volume with the device under test. A high vacuum is needed to put high voltage on the MCP inside the IEEM. At present any out-gassing of the device under test makes the pump-down time very long (3-5 hours, if not more with some types of DUTs with complex boards). In the new partitioning the MCP would always be in high-vacuum and can be turned on at any time, while the DUT chamber would require short pump-down times: the DUT would be moved close to the membrane so that the vacuum required before irradiation could be achieved in minutes. At higher energy accelerators the DUT irradiation could be done in air (the membrane can withstand air-pressure). The

membrane/DUT distance does affect the effective resolution but our work has shown that interesting values can be achieved with millimetric distances (~1-2mm) that could easily accommodate almost any type of device, posing almost no mechanical and electrical constraints to the user.

We have crossed many hurdles, learned a great deal and with persistence have successfully reared the IEEM at SIRAD. In retrospect we remain confident in believing that the IEEM system will now make the already successful facility even more attractive: SIRAD now offers both global and micrometric possibilities for a wide selection of heavy ions. The facility suffers much from too little beam time, but we hope that the success of the latest experiments will help make matters improve.

An IEEM system is non-invasive, flexible and only slightly worse than that of the very best energetic heavy ion microbeams. The traditional microbeam approach is arguably the preferred one, as one can decide where the next ion is going to strike, but it certainly needs far greater development as it is challenging to focus a wide variety of energetic heavy ion beams down to micron size. On the other hand an IEEM can be easily installed by a small group of people on a pre-existing and successful beam-line at any high energy heavy ion accelerator (cyclotron, post-accelerators,...) that can deliver ions with greater range and are more suitable to test the latest microelectronic devices.

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