

Some General Theorems of Incremental Thermoelectroelasticity

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Abstract

We extend to incremental thermoelectroelasticity with biasing fields certain classical theorems, that have been stated and proved in linear thermopiezoelectricity referred to a natural configuration. A uniqueness theorem for the solutions to the initial boundary value problem, the generalized Hamilton principle and a theorem of reciprocity of work are deduced for incremental fields superposed on finite biasing fields in a thermoelectroelastic body.

Key words Thermoelectroelasticity, Uniqueness of solution, Incremental thermoelectroelasticity, Hamilton principle, Theorem of reciprocity of work.

1 Introduction

In the last decades, with the increasing wide use in sensing and actuation, materials exhibiting couplings between elastic, electric, magnetic and thermal fields have attracted much attention.

In order to give certainty to experimental results and applications, the interest of many researchers turned to the mathematical fitting of these topics.

Many applications have their mathematical formulation within a linear framework, and the theoretical study began from this context.

Foundamental is Nowacki's paper [1], where a uniqueness theorem for the solutions of the initial boundary value problems is proved in linear thermopiezoelectricity referred to a natural state, i.e., without biasing (or initial) fields. Hence Nowacki [2] also deduced a generalized Hamilton principle and a theorem of reciprocity of work.

Li [3] generalized the uniqueness and reciprocity theorems for linear thermo-electro-magneto-elasticity referred to a natural state.

Aouadi [4] establishes a reciprocal theorem for a linear theory in which the heat flux is considered as a constitutive independent variable, a rate-type evolution equation for it is added to the system of constitutive equations, and the entropy inequality is stated in the form proposed by Müller [5].

Iesan [6] uses the Green-Naghdi theory of thermomechanics of continua to derive a linear theory of thermoelasticity with internal structure where in particular a uniqueness result holds.

Related works on thermoelasticity and thermoelectromagnetism can be found in [7] to [11].

The classical linear theory of thermopiezoelectricity assumes infinitesimal deviations of the field variables from a reference state, where there are no initial mechanical and electric fields. In order to describe the response of thermoelectroelastic materials in the presence of initial fields one needs the theory for infinitesimal fields superposed on initial fields, and this can only be derived from the fully nonlinear theory of thermoelectroelasticity. The equations of nonlinear thermoelectroelasticity were given in Tiersten [12]. Yang [13] then derived from [12] the equations for infinitesimal incremental fields superposed on finite biasing fields in a thermoelectroelastic body with no assumption on the biasing fields.

Here we extend the aforementioned three Nowacki's theorems [1], [2] to incremental thermoelectroelasticity with initial fields.

We explicitly refer to the incremental theory [13], hence below we rewrite from this paper, with the same notations, some formulae and results on constitutive equations of incremental thermoelectroelasticity.

Of course, the theorems proved here just reduce to the ones in Nowacki's [2] by neglecting the initial fields.

In the uniqueness theorem in Section 4 we assume that in the initial state entropy does not depend on time and temperature is uniform. For the theorem of reciprocity of work in Section 6 we assume that in the initial state both entropy and temperature fields do not depend on time.

2 Equations of Nonlinear Thermoelectroelasticity

2.1 Balance laws and constitutive equations

Consider a thermoelectroelastic body that, in the reference configuration, occupies a region V with boundary surface S . The motion of the body is described by

$$y_i = y_i(X_L, t),$$

where y_i denotes the present coordinates and X_L the reference coordinates of material points with respect to the same Cartesian coordinate system.

Let K_{Lj} , ρ_o , f_j , Δ_L , ρ_E , θ , η , Q_L and γ respectively denote the first Piola-Kirchoff stress tensor, the mass density in the reference configuration, the body force per unit mass, the reference electric displacement vector, the free charge density per unit undeformed volume, the absolute temperature, the entropy per unit mass, the reference heat flux vector, and the body heat source per unit mass. Then we have the following equations of motion, electrostatics, and heat conduction written in material form with respect to the reference configuration:

$$K_{Li,L} + \rho_o f_i = \rho_o \ddot{y}_i, \quad (1)$$

$$\Delta_{L,L} = \rho_E, \quad (2)$$

$$\rho_o \theta \dot{\eta} = -Q_{L,L} + \rho_o \gamma, \quad (3)$$

The above equations are adjoined by constitutive relations defined by the specification of the free energy ψ and heat flux Q_L :

$$\psi = \psi(E_{MN}, W_M, \theta), \quad Q_L = Q_L(E_{MN}, W_M, \theta, \Theta_M) \quad (4)$$

where

$$E_{MN} = (y_{j,M} y_{j,N} - \delta_{MN})/2, \quad W_M = -\phi_{,M}, \quad \Theta_M = \theta_{,M} \quad (5)$$

are the finite strain tensor, the reference electric potential gradient, and the reference temperature gradient; of course, δ_{MN} is the Kronecker delta, and ϕ is the electric potential. Hence, by using ψ the constitutive relations (4) of [13] are deduced for K_{Li} , Δ_L , η ; here we rewrite them from [13]:

$$\begin{aligned} K_{Li} &= y_{i,A} \rho_o \frac{\partial \psi}{\partial E_{AL}} + J X_{L,j} \varepsilon_o (E_j E_i - \frac{1}{2} E_i E_i \delta_{ji}), \\ \Delta_L &= \varepsilon_o J X_{L,j} E_j - \rho_o \frac{\partial \psi}{\partial W_L}, \quad \eta = -\frac{\partial \psi}{\partial \theta}, \end{aligned} \quad (6)$$

with $E_i = -\phi_{,i}$. Recall that the heat-flux constitutive relation (4)₂ is restricted by

$$Q_L \Theta_L \leq 0. \quad (7)$$

Note that, in particular, (4)₂ includes the case in which Q_M is linear in Θ_L , that is,

$$Q_M = -\kappa_{ML}(\theta, W_A) \Theta_L. \quad (8)$$

2.2 The initial boundary value problem for a thermoelectroelastic body

To describe the corresponding boundary conditions to add to the field equations (1)-(3), three partitions (S_{i1}, S_{i2}) , $i = 1, 2, 3$, of the boundary surface $S = \partial\mathcal{B}$ can be assigned. For mechanical boundary conditions, deformation \tilde{y}_i and traction \tilde{t}_i per unit undeformed area are prescribed, respectively, on S_{11} and S_{12} ; for electric boundary conditions, electric potential $\tilde{\phi}$ and surface-free charge $\tilde{\Delta}$ per unit undeformed area are prescribed, respectively, on S_{21} and S_{22} ; while for thermic boundary conditions, temperature $\tilde{\theta}$ and normal heat flux \tilde{Q} per unit undeformed area are prescribed, respectively, on S_{31} and S_{32} . Hence, we can write

$$y_i = \tilde{y}_i \quad \text{on } S_{11}, \quad K_{Li}N_L = \tilde{K}_i \quad \text{on } S_{12} \quad (\text{'mechanical'}), \quad (9)$$

$$\phi = \tilde{\phi} \quad \text{on } S_{21}, \quad \Delta_L N_L = -\tilde{\Delta} \quad \text{on } S_{22}, \quad (\text{'electric'}) \quad (10)$$

$$\theta = \tilde{\theta} \quad \text{on } S_{31}, \quad Q_L N_L = \tilde{Q} \quad \text{on } S_{32} \quad (\text{'thermic'}), \quad (11)$$

where $\mathbf{N} = (N_L)$ is the unit exterior normal on S and

$$S_{i1} \cup S_{i2} = S, \quad S_{i1} \cap S_{i2} = \emptyset \quad (i = 1, 2, 3). \quad (12)$$

We put

$$\mathcal{A}_{body} := (f_i, \rho_E, \gamma), \quad \mathcal{A}_{surf} := (\tilde{y}_i, \tilde{K}_i, \tilde{\phi}, \tilde{\Delta}, \tilde{\theta}, \tilde{Q}), \quad (13)$$

$$\mathcal{A} := (\mathcal{A}_{body}, \mathcal{A}_{surf}) = (f_i, \rho_E, \gamma, \tilde{y}_i, \tilde{K}_i, \tilde{\phi}, \tilde{\Delta}, \tilde{\theta}, \tilde{Q}). \quad (14)$$

\mathcal{A}_{body} , \mathcal{A}_{surf} , and \mathcal{A} are said to be the (*external*) *body-action*, *surface-action*, and *action*, respectively. The initial conditions have the form

$$\begin{aligned} y_i(\mathbf{X}, 0) &= f_i(\mathbf{X}), & \dot{y}_i(\mathbf{X}, 0) &= g_i(\mathbf{X}), \\ \theta(\mathbf{X}, 0) &= h(\mathbf{X}), & \phi(\mathbf{X}, 0) &= l(\mathbf{X}) \quad (\mathbf{X} \in B, t = 0), \end{aligned} \quad (15)$$

where

$$\mathcal{I} = (f_i, g_i, h, l)$$

are prescribed smooth functions of domain V . The initial boundary value problem is then stated as: *assigned* \mathcal{A}_{body} , *to find the solution* (ϕ, θ, y_i) *in* \mathcal{B} *to the constitutive relations (6) and field equations (1)-(3) which satisfies the boundary conditions (9)-(11) and initial conditions (15) for given* \mathcal{A}_{surf} *and* \mathcal{I} .

3 Biasing and incremental fields

In incremental theories three configurations are distinguished: the reference, initial and present configuration.

3.1 The Reference Configuration

In the reference state the body is undeformed and free of all fields. A generic point at this state is denoted by \mathbf{X} with rectangular coordinates X_N . The mass density in the reference configuration is denoted by ρ_o .

3.2 The Initial Configuration

In the initial state the body is deformed finitely under the action of a prescribed initial action

$$\mathcal{A}^o := (\mathcal{A}_{body}^o, \mathcal{A}_{surf}^o) = (f_i^o, \rho_E^o, \gamma^o, \tilde{y}_i^o, \tilde{K}_i^o, \tilde{\phi}^o, \tilde{\Delta}^o, \tilde{\theta}^o, \tilde{Q}^o), \quad (16)$$

$$\mathcal{A}_{body}^o := (f_i^o, \rho_E^o, \gamma^o), \quad \mathcal{A}_{surf}^o := (\tilde{y}_i^o, \tilde{K}_i^o, \tilde{\phi}^o, \tilde{\Delta}^o, \tilde{\theta}^o, \tilde{Q}^o). \quad (17)$$

The position of the material point associated with \mathbf{X} is given by

$$y_\alpha^o = y_\alpha^o(\mathbf{X}, t),$$

with the Jacobian of the initial configuration denoted by

$$J_o = \det(y_{\alpha,L}^o).$$

The initial fields

$$y_\alpha^o = y_\alpha^o(\mathbf{X}, t), \quad \phi^o = \phi^o(\mathbf{X}, t), \quad \theta^o = \theta^o(\mathbf{X}, t) \quad (18)$$

satisfy the equations of nonlinear thermoelectroelasticity (1)-(12) under the prescribed action \mathcal{A}^o . The electric potential, electric field and temperature field are denoted by $\phi^o(\mathbf{X}, t)$, $W_\alpha^o = -\phi_{,\alpha}^o$ and $\theta^o(\mathbf{X}, t)$, respectively.

In studying the incremental fields the solution to the initial state problem is assumed known.

3.3 The Present Configuration

To the deformed body at the initial configuration, infinitesimal deformations, electric, and thermal fields are applied. The present position of the material point associated with \mathbf{X} is given by $y_i(\mathbf{X}, t)$, with electric potential $\phi(\mathbf{X}, t)$ and temperature $\theta(\mathbf{X}, t)$.

The fields $y_i(\mathbf{X}, t)$, $\phi(\mathbf{X}, t)$, $\theta(\mathbf{X}, t)$ satisfy (1)-(3) under the action of the external action (14).

3.4 Equations for the incremental fields

Let ε be a small and dimensionless number. The incremental process $\varepsilon(y^1, \phi^1, \theta^1)$ for (y, ϕ, θ) superposed to the initial process (y^o, ϕ^o, θ^o) is assumed to be infinitesimal and, therefore, we write:

$$y_i = \delta_{i\alpha}(y_\alpha^o + \varepsilon y_\alpha^1), \quad \phi = \phi^o + \varepsilon \phi^1, \quad \theta = \theta^o + \varepsilon \theta^1, \quad (19)$$

Corresponding to (19), the other quantities of the present state can be written as:

$$\mathcal{A} \cong \mathcal{A}^o + \varepsilon \mathcal{A}^1, \quad (20)$$

where, due to nonlinearity, higher powers of ε may arise. For the incremental action we have

$$\mathcal{A}_{body}^1 := (f_i^1, \rho_E^1, \gamma^1), \quad \mathcal{A}_{surf}^1 := (\tilde{y}_i^1, \tilde{K}_i^1, \tilde{\phi}^1, \tilde{\Delta}^1, \tilde{\theta}^1, \tilde{Q}^1). \quad (21)$$

$$\mathcal{A}^1 := (\mathcal{A}_{body}^1, \mathcal{A}_{surf}^1) = (f_i^1, \rho_E^1, \gamma^1, \tilde{y}_i^1, \tilde{K}_i^1, \tilde{\phi}^1, \tilde{\Delta}^1, \tilde{\theta}^1, \tilde{Q}^1). \quad (22)$$

We want to derive equations governing the incremental process

$$(\mathbf{u} := \mathbf{y}^1, \quad \phi^1, \quad \theta^1).$$

From (19) and (20), we can further write:

$$E_{KL} \cong E_{KL}^o + \varepsilon E_{KL}^1, \quad W_L \cong W_L^o + \varepsilon W_L^1, \quad \Theta_L \cong \Theta_L^o + \varepsilon \Theta_L^1, \quad (23)$$

where

$$\begin{aligned} E_{KL}^o &= (y_{\alpha,K}^o y_{\alpha,L}^o - \delta_{KL})/2, & E_{KL}^1 &= (y_{\alpha,K}^o y_{\alpha,L}^1 + y_{\alpha,L}^o y_{\alpha,K}^1)/2, \\ W_L^o &= -\phi_{,L}^o, & W_L^1 &= -\phi_{,L}^1, & \Theta_L^o &= \theta_{,L}^o, & \Theta_L^1 &= \theta_{,L}^1. \end{aligned} \quad (24)$$

Substituting (19)-(24) into the constitutive relations (1)-(3), with some very lengthy algebra, the following expression are obtained [13]:

$$\begin{aligned} K_{Mi} &\cong \delta_{i\alpha}(K_{M\alpha}^o + \varepsilon K_{M\alpha}^1), & \Delta_M &\cong \Delta_M^o + \varepsilon \Delta_M^1, \\ \eta &\cong \eta^o + \varepsilon \eta^1, & Q_M &\cong Q_M^o + \varepsilon Q_M^1. \end{aligned} \quad (25)$$

where

$$K_{M\alpha}^1 = G_{M\alpha L \gamma} u_{\gamma,L} + R_{LM\alpha} \phi_{,L}^1 - \rho_o \Lambda_{M\alpha} \theta^1, \quad (26)$$

$$\Delta_M^1 = R_{MN\gamma} u_{\gamma,N} - L_{MN} \phi_{,N}^1 + \rho_o P_M \theta^1, \quad (27)$$

$$\eta^1 = \Lambda_{M\gamma} u_{\gamma,M} - P_M \phi_{,M}^1 + \alpha \theta^1, \quad (28)$$

$$Q_M^1 = A_{MN\alpha}u_{\alpha,N} - B_{MN}\phi_{,N}^1 + C_M\theta^1 + F_{MN}\theta_{,N}^1. \quad (29)$$

By putting

$$\kappa_{MN\alpha} = -A_{MN\alpha}, \quad \kappa_{MN}^E = B_{MN}, \quad \kappa_M = -C_M, \quad \kappa_{MN} = -F_{MN},$$

the latter rewrites as

$$Q_M^1 = -\kappa_{MN\alpha}u_{\alpha,N} - \kappa_{MN}^E\phi_{,N}^1 - \kappa_M\theta^1 - \kappa_{MN}\theta_{,N}^1. \quad (30)$$

In (26)-(29), $G_{M\alpha L\gamma}$ are the effective elastic constants, $R_{LM\alpha}$ are the effective piezoelectric constants, $\Lambda_{M\alpha}$ are the effective thermoelastic constants, L_{MN} are the effective dielectric constants, P_M are the effective pyroelectric constants, α is related with the specific heat. Their expressions are [13]:

$$\begin{aligned} G_{K\alpha L\gamma} &= y_{\alpha,M}^o \rho_o \frac{\partial^2 \psi}{\partial E_{KM} \partial E_{LN}}(\theta^o, E_{AB}^o, W_A^o) y_{\alpha,L}^o + \rho_o \frac{\partial \psi}{\partial E_{KL}}(\theta^o, E_{AB}^o, W_A^o) \delta_{\alpha\gamma} + g_{K\alpha L\gamma}, \\ R_{LM\gamma} &= -\rho_o \frac{\partial^2 \psi}{\partial W_K \partial E_{ML}}(\theta^o, E_{AB}^o, W_A^o) y_{\gamma,M}^o + r_{KL\gamma}, \\ \Lambda_{M\gamma} &= -\frac{\partial^2 \psi}{\partial E_{LM} \partial \theta}(\theta^o, E_{AB}^o, W_A^o) y_{\gamma,L}^o, \\ L_{MN} &= -\rho_o \frac{\partial^2 \psi}{\partial W_M \partial W_N}(\theta^o, E_{AB}^o, W_A^o) + l_{MN}, \quad P_M = -\frac{\partial^2 \psi}{\partial W_M \partial \theta}(\theta^o, E_{AB}^o, W_A^o), \\ \alpha &= -\frac{\partial^2 \psi}{\partial \theta^2}(\theta^o, E_{AB}^o, W_A^o), \quad A_{MN\gamma} = \frac{\partial Q_M}{\partial E_{LN}}(\theta^o, E_{AB}^o, W_A^o) y_{\gamma,L}^o = -\kappa_{MN\gamma}, \\ B_{MN} &= \frac{\partial Q_M}{\partial W_N}(\theta^o, E_{AB}^o, W_A^o) = \kappa_{MN}^E, \\ C_M &= \frac{\partial Q_M}{\partial \theta}(\theta^o, E_{AB}^o, W_A^o) = -\kappa_M, \quad F_{MN} = \frac{\partial Q_M}{\partial \Theta_N}(\theta^o, E_{AB}^o, W_A^o) = -\kappa_{MN}, \end{aligned}$$

where

$$\begin{aligned} g_{K\alpha L\gamma} &= \varepsilon_o J_o \left[W_\alpha^o W_\beta^o (X_{K,\beta} X_{L,\gamma} - X_{K,\gamma} X_{L,\beta}) + W_\beta^o W_\gamma^o (X_{K,\alpha} X_{L,\beta} - X_{K,\beta} X_{L,\alpha}) \right. \\ &\quad \left. + W_\beta^o W_\beta^o (X_{K,\gamma} X_{L,\alpha} - X_{K,\alpha} X_{L,\gamma}) / 2 - W_\alpha^o W_\gamma^o X_{K,\beta} X_{L,\beta} \right], \\ r_{KL\gamma} &= \varepsilon_o J_o (W_\alpha^o X_{K,\alpha} X_{L,\gamma} - W_\alpha^o X_{K,\gamma} X_{L,\alpha} - W_\gamma^o X_{K,\alpha} X_{L,\alpha}), \quad l_{MN} = \varepsilon_o J_o X_{M,\alpha} X_{N,\alpha}. \end{aligned} \quad (32)$$

In (29) we have introduced the κ -notation to allow comparison between the proofs written here and those written in [2]. The following symmetries hold:

$$G_{K\alpha L\gamma} = G_{L\gamma K\alpha}, \quad L_{MN} = L_{NM}. \quad (33)$$

3.5 Restriction on the incremental heat flux

Now we show that the restriction (7) on the heat flux (4)₂, together with the condition

$$Q_L^o = 0 \quad \text{for} \quad \Theta_L^o = 0, \quad (34)$$

implies an analogous restriction on the incremental heat flux (29), that is,

$$Q_L^1 \Theta_L^1 \leq 0. \quad (35)$$

Indeed, substituting $Q_L = Q_L^o + \varepsilon Q_L^1$, $\Theta_L = \Theta_L^o + \varepsilon \Theta_L^1$ in (7), we obtain

$$(Q_L^o + \varepsilon Q_L^1)(\Theta_L^o + \varepsilon \Theta_L^1) \leq 0, \quad (36)$$

which for $\Theta_L^o = 0$, by (34), yields (35). Note that the choice (8) for the heat flux response function satisfies (34).

3.6 Incremental field equations

By substituting (19)-(25) into (1)-(3) and (9)-(11), we find the governing equations for the incremental fields

$$K_{M\alpha, M}^1 + \rho_o f_\alpha^1 = \rho_o \ddot{u}_\alpha, \quad (37)$$

$$\Delta_{M, M}^1 = \rho_E^1, \quad (38)$$

$$\rho_o (\theta^o \dot{\eta}^1 + \theta^1 \dot{\eta}^o) = -Q_{M, M}^1 + \rho_o \gamma^1. \quad (39)$$

Introducing the constitutive relations (26)-(29) into the incremental equations of motion (37), the equation of the electric field (38), and the heat equation (39), for $f_\alpha^1 = 0$ we have

$$G_{M\alpha L\gamma} u_{\gamma, LM} + R_{LM\alpha} \phi_{, LM}^1 - \rho_o \Lambda_{M\alpha} \theta_{, M}^1 = \rho_o \ddot{u}_\alpha, \quad (40)$$

$$R_{MN\gamma} u_{\gamma, NM} - L_{MN} \phi_{, NM}^1 + \rho_o P_M \theta_M^1 = \rho_E^1, \quad (41)$$

$$\begin{aligned} & \rho_o \theta^o \left(\Lambda_{M\gamma} \dot{u}_{\gamma, M} - P_M \dot{\phi}_{, M}^1 + \alpha \dot{\theta}^1 \right) + \rho_o \theta^1 \dot{\eta}^o \\ &= \kappa_{MN}^E \phi_{, NM}^1 + \kappa_M \theta_{, M}^1 + \kappa_{MN} \theta_{, NM}^1 + \kappa_{MN\alpha} u_{\alpha, NM} + \rho_o \gamma^1. \end{aligned} \quad (42)$$

4 Uniqueness theorem of the solution of the incremental differential equations

In the present Section we assume $\dot{\eta}^o = 0$ and $\Theta_L^o = 0$, i.e. the initial temperature field θ^o is uniform. This holds true when the initial state is static. We follow step by step the proof of Nowacki [2] and put in evidence any difference when it will appear.

A modified version of energy balance is needed. It follows by substituting the virtual increments by the real increments

$$\delta u_\alpha = \frac{\partial u_\alpha}{\partial t} dt = v_\alpha dt, \quad \delta u_{\alpha,M} = \dot{u}_{\alpha,M} dt, \quad \dots$$

in the principle of virtual work

$$\int_{V^o} (f_\alpha^1 - \rho_o \ddot{u}_\alpha) \delta u_\alpha dV + \int_{S^o} \tilde{K}_\alpha \delta u_\alpha dS = \int_{V^o} K_{M\alpha}^1 \delta u_{\alpha,M} dV. \quad (43)$$

Thus the fundamental energy equation

$$\int_{V^o} (f_\alpha^1 - \rho_o \dot{v}_\alpha) v_\alpha dV + \int_{S^o} \tilde{K}_\alpha v_\alpha dS = \int_{V^o} K_{M\alpha}^1 \dot{u}_{\alpha,M} dV \quad (44)$$

is obtained, where we substitute the constitutive relations (26). Hence

$$\begin{aligned} \int_{V^o} (f_\alpha^1 - \rho_o \dot{v}_\alpha) v_\alpha dV + \int_{S^o} \tilde{K}_\alpha v_\alpha dS \\ = \int_{V^o} (G_{M\alpha L\gamma} u_{\gamma,L} + R_{LM\alpha} \phi_{,L}^1 - \rho_o \Lambda_{M\alpha} \theta^1) \dot{u}_{\alpha,M} dV, \end{aligned} \quad (45)$$

thus

$$\frac{d}{dt} (\mathcal{W} + \mathcal{K}) = \int_{V^o} f_\alpha^1 v_\alpha dV + \int_{S^o} \tilde{K}_\alpha v_\alpha dS + \int_{V^o} (\rho_o \Lambda_{M\alpha} \theta^1 - R_{LM\alpha} \phi_{,L}^1) \dot{u}_{\alpha,M} dV, \quad (46)$$

where \mathcal{W} is the work of deformation and \mathcal{K} is the kinetic energy:

$$\mathcal{W} = \frac{1}{2} \int_{V^o} G_{M\alpha L\gamma} u_{\alpha,M} u_{\gamma,L} dV, \quad \mathcal{K} = \frac{1}{2} \int_{V^o} \rho_o v_\alpha v_\alpha dV. \quad (47)$$

Now, to eliminate the term $\int_{V^o} \rho_o \Lambda_{M\alpha} \theta^1 \dot{u}_{\alpha,M} dV$, we multiply by θ^1 the heat-conduction equation (42), where $\dot{\eta}^o = 0$, and integrate over V^o ; after simple transformations we obtain

$$\begin{aligned} \int_{V^o} \rho_o \theta^1 \Lambda_{M\alpha} \dot{u}_{\alpha,M} dV &= \frac{\kappa_{ML}^E}{\theta^o} \int_{S^o} \theta^1 \phi_{,L}^1 N_M dS + \\ &+ \frac{\kappa_L}{\theta^o} \int_{S^o} \theta^1 N_L dS + \frac{\kappa_{ML}}{\theta^o} \int_{S^o} \theta^1 \theta_{,L}^1 N_M dS + \frac{\kappa_{ML\alpha}}{\theta^o} \int_{S^o} \theta^1 u_{\alpha,L} N_M dS \\ &+ P_L \int_{V^o} \rho_o \theta^1 \dot{\phi}_{,L}^1 dV + \frac{1}{\theta^o} \int_{V^o} \rho_o \theta^1 \gamma^1 dV - \frac{d}{dt} \mathcal{P} - (\chi + \chi_\theta + \chi_\phi + \chi_u), \end{aligned} \quad (48)$$

where

$$\mathcal{P} = \frac{\alpha}{2\theta^o} \int_{V^o} \rho_o \theta^1 \theta^1 dV, \quad (49)$$

$$\begin{aligned} \chi_\phi &= \frac{\kappa_{ML}^E}{\theta^o} \int_{V^o} \theta^1_{,M} \phi^1_{,L} dV, & \chi &= \frac{\kappa_M}{\theta^o} \int_{V^o} \theta^1_{,M} \theta^1 dV, \\ \chi_\theta &= \frac{\kappa_{ML}}{\theta^o} \int_{V^o} \theta^1_{,M} \theta^1_{,L} dV, & \chi_u &= \frac{\kappa_{ML\alpha}}{\theta^o} \int_{V^o} \theta^1_{,M} u_{\alpha,L} dV. \end{aligned} \quad (50)$$

Note that this equation differs from the corresponding Eq.(25) in [2] by the terms χ_ϕ , χ and χ_u . Now, substituting (48) into (46), we are lead to the equation

$$\begin{aligned} \frac{d}{dt}(\mathcal{W} + \mathcal{K} + \mathcal{P}) + (\chi + \chi_\theta + \chi_\phi + \chi_u) &= \int_{V^o} f_\alpha^1 v_\alpha dV + \int_{S^o} \tilde{K}_\alpha v_\alpha dS + \\ &+ \frac{\kappa_{ML}^E}{\theta^o} \int_{S^o} \theta^1 \phi^1_{,L} N_M dS + \frac{\kappa_L}{\theta^o} \int_{S^o} \theta^1 N_L dS + \frac{\kappa_{ML}}{\theta^o} \int_{S^o} \theta^1 \theta^1_{,L} N_M dS + \\ &+ \frac{1}{\theta^o} \int_{V^o} \rho_o \theta^1 \gamma^1 dV - \int_{V^o} (R_{LM\alpha} \phi^1_{,L} \dot{u}_{\alpha,M} - \rho_o P_M \theta^1 \dot{\phi}^1_{,M}) dV. \end{aligned} \quad (51)$$

To eliminate the term

$$\int_{V^o} (R_{LM\alpha} \phi^1_{,L} \dot{u}_{\alpha,M} - \rho_o P_M \theta^1 \dot{\phi}^1_{,M}) dV$$

in Eq.(51) we substitute the constitutive relations (27) into the time-derivative of the equation of the electric field (38) with $\rho_E = 0$. Multiplying the obtained equation by ϕ^1 and integrating over the region of the body, we obtain

$$\int_{S^o} \dot{\Delta}_M \phi^1 N_M dV + \int_{V^o} \dot{\Delta}_M W_M^1 dV = 0. \quad (52)$$

Using the relations (27) and (52), after simple transformations we obtain

$$\begin{aligned} &\int_{V^o} \dot{\Delta}_L W_L^1 dV = \\ &= \int_{V^o} (R_{LM\alpha} \dot{u}_{\alpha,M} W_L^1 + L_{LM} \dot{W}_M^1 W_L^1 + \rho_o P_L \frac{d}{dt}(\theta^1 W_L^1) - \rho_o P_L \theta^1 \dot{W}_L^1) dV = \\ &= - \int_{S^o} \dot{\Delta}_L^1 N_L \phi^1 dS, \end{aligned}$$

from which

$$\begin{aligned} &\int_{V^o} (R_{KM\alpha} \dot{u}_{\alpha,M} W_K^1 - \rho_o P_K \theta^1 \dot{W}_K^1) dV = \\ &= - \int_{S^o} \dot{\Delta}_K^1 N_K \phi^1 dS - \frac{d}{dt} \mathcal{E} - \frac{d}{dt} (\rho_o P_K \int_{V^o} \theta^1 W_K^1 dV) \end{aligned} \quad (53)$$

where

$$\mathcal{E} = \frac{1}{2} L_{KM} \int_{V^o} W_M^1 W_K^1 dV. \quad (54)$$

In view of Eqs.(51) and (53), we arrive at the modified energy balance

$$\begin{aligned} & \frac{d}{dt} \left(\mathcal{W} + \mathcal{K} + \mathcal{P} + \mathcal{E} + \rho_o P_K \int_{V^o} \theta^1 W_K^1 dV \right) + (\chi + \chi_\theta + \chi_\phi + \chi_U) = \\ & = \int_{V^o} f_\alpha^1 v_\alpha dV + \int_{S^o} \tilde{K}_\alpha v_\alpha dS + \\ & + \frac{\kappa_{ML}^E}{\theta^o} \int_{S^o} \theta^1 \phi_{,L}^1 N_M dS + \frac{\kappa_L}{\theta^o} \int_{S^o} \theta^1 N_L dS + \frac{\kappa_{ML}}{\theta^o} \int_{S^o} \theta^1 \theta_{,L}^1 N_M dS + \\ & + \frac{1}{\theta^o} \int_{V^o} \rho_o \theta^1 \gamma^1 dV - \int_{S^o} \hat{\Delta}_K^1 N_K \phi^1 dS. \end{aligned} \quad (55)$$

The energy balance (55) makes possible the proof of the uniqueness of the solution.

We assume that two distinct solutions $(u'_i, \phi^{1'}, \theta^{1'})$ and $(u''_i, \phi^{1''}, \theta^{1''})$ satisfy Eqs.(37)-(39) and the appropriate boundary and initial conditions. Their difference

$$(\hat{u}_i = u'_i - u''_i, \quad \hat{\phi} = \phi^{1'} - \phi^{1''}, \quad \hat{\theta} = \theta^{1'} - \theta^{1''})$$

therefore satisfies the homogeneous equations (37)-(39) and the homogeneous boundary and initial conditions. Equation (55) holds for $(\hat{u}_i, \hat{\phi}, \hat{\theta})$.

In view of the homogeneity of the equations and the boundary conditions, the right-hand side of Eq.(55) vanishes. Hence

$$\frac{d}{dt} \left(\mathcal{W} + \mathcal{K} + \mathcal{P} + \mathcal{E} + \rho_o P_K \int_{V^o} \theta^1 W_K^1 dV \right) = -(\chi + \chi_\theta + \chi_\phi + \chi_u) \leq 0, \quad (56)$$

where the last inequality is true since by (30), (50) and (35) we have

$$-(\chi + \chi_\theta + \chi_\phi + \chi_u) = \frac{1}{\theta^o} \int_{V^o} Q_M^1 \Theta_M^1 dV. \quad (57)$$

The integral in the left-hand side of Eq.(56) vanishes at the initial instant, since the functions $\hat{u}_i, \hat{\phi}, \hat{\theta}$ satisfy the homogeneous initial conditions. On the other hand, by the inequality in (56) the left-hand side is either negative or zero.

Now we assume (*i-iii*) below; note that (*iii*) is the sufficient condition of J. Ignaczak, written in [2] on pages 176-177.

(*i*) The initial deformation y_α^o realizes that the tensor $G_{M\alpha L\gamma}$ is positive-definite, so that $\mathcal{W} \geq 0$ by (47).

(ii) The tensor L_{KN} is positive-definite so that, by (54), $\mathcal{E} \geq 0$.

(iii) L_{IJ} is a known positive-definite symmetric tensor, $g_I = \rho_o P_I$ is a vector, and $c = \rho_o \alpha / 2\theta^o > 0$; consider the function

$$A(\theta^1, W_L) = (\theta^1)^2 + 2\theta^1 g_I W_I^1 + L_{IJ} W_I^1 W_J^1$$

A is nonnegative for every real pair (θ^1, W_k^1) , provided

$$|g_I| \leq c\lambda_m$$

where λ_m is the smallest positive eigenvalue of the tensor L_{IJ} .

Under these three assumptions, (56) implies

$$\hat{u}_{i,L} = 0, \quad \hat{\theta} = 0, \quad \hat{W}_L = 0,$$

which imply the uniqueness of the solutions of the incremental thermoelectroelastic equations, i.e.,

$$u'_i = u''_i, \quad \theta^{1'} = \theta^{1''}, \quad W_I^{1'} = W_I^{1''}.$$

Moreover, from the constitutive relations we have that

$$K_{I\alpha}^{1'} = K_{I\alpha}^{1''}, \quad \Delta_L^{1'} = \Delta_L^{1''}, \quad \eta^{1'} = \eta^{1''}.$$

5 On the generalized Hamilton's principle

We define the free energy, electric enthalpy, and potential of the heat flow respectively by

$$\psi^1 = \frac{1}{2} G_{M\alpha L\gamma} u_{\alpha, M} u_{\gamma, L} + R_{LM\alpha} \phi_{,L}^1 u_{\alpha, M} - \rho_o \theta^1 \left[\Lambda_{M\alpha} u_{\alpha, M} - P_M \phi_{,M}^1 + \frac{\alpha}{2} \theta^1 \right], \quad (58)$$

$$H^1 = \psi^1 - \frac{1}{2} L_{AB} W_A^1 W_B^1 = \psi^1 - \frac{1}{2} L_{AB} \Phi_{,A}^1 \Phi_{,B}^1, \quad \Gamma = Q_M^1 \theta_{,M}^1; \quad (59)$$

note that, by (30) the latter becomes

$$\Gamma = - \left(\kappa_{MN\alpha} u_{\alpha, N} \theta_{,M}^1 + \frac{1}{2} \kappa_{MN} \theta_{,M}^1 \theta_{,N}^1 + \kappa_{MN}^E \theta_{,M}^1 \phi_{,N}^1 + \kappa_M \theta^1 \theta_{,M}^1 \right). \quad (60)$$

Whence

$$\frac{\partial H^1}{\partial u_{\alpha, M}} = K_{M\alpha}^1, \quad \frac{\partial H^1}{\partial W_L^1} = -\Delta_L^1, \quad \frac{\partial H^1}{\partial \theta} = -\rho_o \eta^1, \quad (61)$$

$$Q_M^1 = \frac{\partial \Gamma}{\partial \theta^1_{,M}}. \quad (62)$$

Lastly we define two functionals

$$\Pi = \int_{V^o} (H^1 + \rho_o \eta^1 \theta^1 - f_\alpha^1 u_\alpha) dV - \int_{S^o} (\tilde{K}_\alpha^1 u_\alpha - \tilde{\Delta}^1 \phi^1) dS \quad (63)$$

and

$$\Psi = \int_{V^o} (\Gamma - \rho_o(\eta^1 \theta^o \dot{\theta}^1 + \eta^1 \dot{\theta}^o \theta^1 + \eta^o \theta^1 \dot{\theta}^1 + \gamma^1 \theta^1)) dV + \int_{S^o} \theta^1 \tilde{Q} dS, \quad (64)$$

Eqs.(58)-(64) generalize Eqs.[2, (36)-(38)].

The generalized Hamilton's principle has the form

$$\delta \int_{t_1}^{t_2} (\mathcal{K} - \Pi) dt = 0, \quad \delta \int_{t_1}^{t_2} \Psi dt = 0 \quad (65)$$

The virtual processes

$$(\delta u_\alpha, \delta \theta^1, \delta \phi^1)$$

of the body must be compatible with the conditions restricting the process of the body. Moreover the virtual processes must satisfy the conditions

$$\delta u_\alpha(\mathbf{x}, t_1) = \delta u_\alpha(\mathbf{x}, t_2) = 0, \quad \delta \theta^1(\mathbf{x}, t_1) = \delta \theta^1(\mathbf{x}, t_2) = 0, \quad \delta \phi^1(\mathbf{x}, t_1) = \delta \phi^1(\mathbf{x}, t_2) = 0.$$

Hence, performing the variations in the second of Eqs.(65) and observing that

$$\delta H^1 = K_{M\alpha}^1 \delta u_{\alpha,M} - \rho_o \eta^1 \delta \theta^1 + \Delta_L^1 \delta \Phi_{,L}^1, \quad (66)$$

and

$$\begin{aligned} & \int_{t_1}^{t_2} (\mathcal{K} - \Pi) dt = \\ & = \int_{t_1}^{t_2} dt \left[\int_{V^o} \left(\frac{\rho_o}{2} \dot{u}_\alpha \dot{u}_\alpha - H^1 - \rho_o \eta^1 \theta^1 + f_\alpha^1 u_\alpha \right) dV + \int_{S^o} (\tilde{K}_\alpha^1 u_\alpha - \tilde{\Delta}^1 \phi^1) dS \right], \quad (67) \end{aligned}$$

we have

$$\begin{aligned} \delta \int_{t_1}^{t_2} (\mathcal{K} - \Pi) dt = & \int_{t_1}^{t_2} dt \left[\int_{V^o} \left(-\rho_o \ddot{u}_\alpha \delta u_\alpha - K_{M\alpha}^1 \delta u_{\alpha,M} - \Delta_L^1 \delta \Phi_{,L}^1 + f_\alpha^1 \delta u_\alpha \right) dV \right. \\ & \left. + \int_{S^o} (\tilde{K}_\alpha^1 \delta u_\alpha - \tilde{\Delta}^1 \delta \phi^1) dS \right]. \quad (68) \end{aligned}$$

Hence by the identities

$$\begin{aligned} -K_{L\alpha}^1 (\delta u_\alpha)_{,L} &= -(K_{L\alpha}^1 \delta u_\alpha)_{,L} + (K_{L\alpha,L}^1) \delta u_\alpha, \\ \Delta_L^1 (\delta \phi^1)_{,L} &= (\Delta_L^1 \delta \phi^1)_{,L} - (\Delta_{L,L}^1) \delta \phi^1, \quad (69) \end{aligned}$$

we have

$$\begin{aligned} \delta \int_{t_1}^{t_2} (\mathcal{K} - \Pi) dt &= \int_{t_1}^{t_2} dt \left[\int_{V^o} \left[(-\rho_o \ddot{u}_\alpha \delta u_\alpha + K_{M\alpha, M}^1 + f_\alpha^1) \delta u_\alpha + \Delta_{M, M}^1 \delta \phi^1 \right] dV \right. \\ &\quad \left. + \int_{S^o} \left(-K_{M\alpha}^1 \delta u_\alpha N_M dS - \Delta_M^1 \delta \phi^1 N_M \right) dS + \int_{S^o} \left(\tilde{K}_\alpha^1 \delta u_\alpha - \tilde{\Delta}^1 \delta \phi^1 \right) dS \right]. \end{aligned} \quad (70)$$

Thus we have

$$\begin{aligned} &\int_{t_1}^{t_2} dt \left[\int_{V^o} \left(-\rho_o \ddot{u}_\alpha + K_{M\alpha, M}^1 + f_\alpha^1 \right) \delta u_\alpha dV + \int_{V^o} \Delta_{M, M}^1 \delta \phi^1 dV \right. \\ &\quad \left. + \int_{S^o} \left(\tilde{K}_\alpha^1 - K_{M\alpha}^1 N_M \right) \delta u_\alpha dS - \int_{S^o} \left(\tilde{\Delta}^1 + \Delta_M^1 N_M \right) \delta \phi^1 dS \right] = 0. \end{aligned} \quad (71)$$

Since the variations δu_α and $\delta \phi^1$ are arbitrary, Eq.(71) is equivalent to the equations governing the incremental motion and electric field, completed by the appropriate boundary conditions. These equations and boundary conditions coincide with those written above.

Next we perform the required variation in the second of Eqs.(65) by observing that

$$\begin{aligned} \delta \Gamma &= \frac{\partial \Gamma}{\partial u_{\alpha, N}} \delta u_{\alpha, N} + \frac{\partial \Gamma}{\partial \theta_{, L}^1} \delta \theta_{, L}^1 + \frac{\partial \Gamma}{\partial \phi_{, L}^1} \delta \phi_{, L}^1 + \frac{\partial \Gamma}{\partial \theta^1} \delta \theta^1 \\ &= -\kappa_{MN\alpha} \theta_{, M}^1 \delta u_{\alpha, N} + Q_L^1 \delta \theta_{, L}^1 - \kappa_{MN}^E \theta_{, M}^1 \delta \phi_{, L}^1 - \kappa_M \theta_{, M}^1 \delta \theta^1. \end{aligned} \quad (72)$$

By (64) we have

$$\begin{aligned} &\delta \int_{t_1}^{t_2} \Psi dt = \\ &= \int_{t_1}^{t_2} dt \left[\int_{V^o} \left(\delta \Gamma - \rho_o \eta^1 (\theta^o \delta \dot{\theta}^1 + \dot{\theta}^o \delta \theta^1) - \rho_o \eta_o (\theta^1 \delta \dot{\theta}^1 + \dot{\theta}^1 \delta \theta^1) - \rho_o \gamma^1 \delta \theta^1 \right) dV \right. \\ &\quad \left. + \int_{S^o} \delta \theta^1 \tilde{Q} dS \right] \\ &= \int_{t_1}^{t_2} dt \left[\int_{V^o} \left(-\kappa_{ML\alpha} \theta_{, M}^1 \delta u_{\alpha, L} + Q_L^1 \delta \theta_{, L}^1 - \kappa_{ML}^E \theta_{, M}^1 \delta \phi_{, L}^1 - \kappa_M \theta_{, M}^1 \delta \theta^1 \right. \right. \\ &\quad \left. \left. + \rho_o [\dot{\eta}^1 \theta^o \delta \theta^1 - \overline{(\eta^1 \theta^o \delta \theta^1)}] + \rho_o [\dot{\eta}^o \theta^1 \delta \theta^1 - \overline{(\eta^o \theta^1 \delta \theta^1)}] - \rho_o \gamma^1 \delta \theta^1 \right) dV \right. \\ &\quad \left. + \int_{S^o} \delta \theta^1 \tilde{Q} dS \right]. \end{aligned} \quad (73)$$

Note that

$$\int_{t_1}^{t_2} \overline{(\eta^\nu \theta^\tau \delta \theta^1)} dt = \left[\eta^\nu \theta^\tau \delta \theta^1 \right]_{t_1}^{t_2} = 0 \quad (\nu, \tau = 0, 1), \quad (74)$$

since $\delta\theta^1 = 0$ at t_1 and t_2 . Also by using the identity

$$(a_L b)_{,L} = a_{L,L} b + a_L b_{,L} \quad (75)$$

we obtain

$$\begin{aligned} & \delta \int_{t_1}^{t_2} \Psi dt = \\ &= \int_{t_1}^{t_2} dt \left[\int_{V^o} (Q_{L,L}^1 + \rho_o[\dot{\eta}^1 \theta^o + \dot{\eta}^o \theta^1 - \gamma^1]) \delta\theta^1 dV - \int_{S^o} (Q_L^1 N_L - \tilde{Q}) \delta\theta^1 dS \right] \\ & \quad - \int_{t_1}^{t_2} dt \left[\int_{V^o} (\kappa_{ML\alpha} \theta_{,M}^1 \delta u_{\alpha,L} + \kappa_{IJ}^E \theta_{,I}^1 \delta\phi_{,J}^1 + \kappa_L \theta_{,L}^1 \delta\theta^1) dV \right] \end{aligned} \quad (76)$$

with

$$\int_{V^o} \kappa_{ML\alpha} \theta_{,M}^1 \delta u_{\alpha,L} dV = \kappa_{ML\alpha} \left[- \int_{V^o} \theta_{,ML}^1 \delta u_{\alpha} dV + \int_{S^o} \theta_{,M}^1 N_L \delta u_{\alpha} dS \right], \quad (77)$$

$$\int_{V^o} \kappa_{ML}^E \theta_{,M}^1 \delta\phi_{,L}^1 dV = \kappa_{ML}^E \left[- \int_{V^o} \theta_{,ML}^1 \delta\phi^1 dV + \int_{S^o} \theta_{,M}^1 N_L \delta\phi^1 dS \right]. \quad (78)$$

Hence, by performing the variation (76) with the variations $\delta u_{\alpha}, \delta\phi^1$ that vanish, and with $\delta\theta^1$ arbitrary, we obtain that (76) reduces to

$$\begin{aligned} \delta \int_{t_1}^{t_2} \Psi dt = \int_{t_1}^{t_2} dt \left[\int_{V^o} (Q_{L,L}^1 - \kappa_L \theta_{,L}^1 + \rho_o[\dot{\eta}^1 \theta^o + \dot{\eta}^o \theta^1 - \gamma^1]) \delta\theta^1 dV \right. \\ \left. - \int_{S^o} (Q_L^1 N_L - \tilde{Q}) \delta\theta^1 dS \right]. \end{aligned} \quad (79)$$

Thus (i) the variational equation (65)₂ performed with

$$\delta u_{\alpha} = 0 = \delta\phi^1 \quad (80)$$

is equivalent to the entropy balance

$$Q_{L,L}^1 + \rho_o(\dot{\eta}^1 \theta^o + \dot{\eta}^o \theta^1 - \gamma^1) = 0 \quad (81)$$

and the boundary condition for the heat flow

$$Q_L^1 N_L = \tilde{Q}, \quad (\mathbf{x} \in S) \quad (82)$$

if and only if

$$\kappa_L = 0. \quad (83)$$

Alternatively, by performing the variation (65)₂ with all the variations $\delta u_{\alpha}, \delta\phi^1, \delta\theta^1$ arbitrary, we deduce that

(ii) the variational equation (65)₂ is equivalent to the entropy balance (81) and the boundary condition for the heat flow (82) if and only if

$$\kappa_L = 0, \quad \kappa_{ML}^E = 0, \quad \kappa_{ML\alpha} = 0.$$

6 Theorem of Reciprocity of Work

Next we extend the theorem of reciprocity of work following some steps in [2] on pages 179-182, where it is referred to linear thermoelectroelasticity in a natural configuration. Here there are some essential changes imposed by the presence of the initial fields. We assume that the body is homogeneous and moreover that the initial state is static, so that in particular $\dot{\theta}^o = 0$, $\dot{\eta}^o = 0$. Here we do not assume that θ^o is uniform.

The Laplace transform of functions $\nu = \nu(\mathbf{x}, t)$,

$$\bar{\nu}(\mathbf{x}, p) = \int_0^\infty e^{-pt} \nu(\mathbf{x}, t) dt, \quad (84)$$

will be used below.

Consider two sets of causes \mathcal{A}^1 , $\mathcal{A}^{1'}$ for incremental processes, and respective effects (u_α, ϕ, θ) , $(u'_\alpha, \phi', \theta')$. Starting from the equations of motion

$$K_{L\alpha,L}^1 + \rho_o f_\alpha = \rho_o \ddot{u}_\alpha, \quad K_{L\alpha,L}^{1'} + \rho_o f'_\alpha = \rho_o \ddot{u}'_\alpha, \quad (85)$$

taking their Laplace transform, multiplying each by $\bar{\theta}^o$, then multiplying the first by \bar{u}'_α and the second by \bar{u}_α , and making the difference of their integrals over the instantaneous region V , assuming that the initial conditions for the displacements are homogeneous, we obtain the integral equation

$$\int_{V^o} \bar{\theta}^o (\bar{F}_\alpha \bar{u}'_\alpha - \bar{F}'_\alpha \bar{u}_\alpha) dV + \int_{V^o} \bar{\theta}^o (\bar{K}_{L\alpha,L}^1 \bar{u}'_\alpha - \bar{K}_{L\alpha,L}^{1'} \bar{u}_\alpha) dV = 0, \quad (86)$$

where $F_\alpha = \rho_o f_\alpha$, $F'_\alpha = \rho_o f'_\alpha$. Now, by the identity (75) and the divergence theorem, we have

$$\begin{aligned} \int_{V^o} \bar{\theta}^o (\bar{K}_{L\alpha,L}^1 \bar{u}'_\alpha - \bar{K}_{L\alpha,L}^{1'} \bar{u}_\alpha) dV &= \int_{S^o} \bar{\theta}^o (\bar{K}_{L\alpha}^1 \bar{u}'_\alpha - \bar{K}_{L\alpha}^{1'} \bar{u}_\alpha) N_L dS \\ &\quad - \int_{V^o} (\bar{K}_{L\alpha}^1 (\bar{\theta}^o \bar{u}'_\alpha)_{,L} - \bar{K}_{L\alpha}^{1'} (\bar{\theta}^o \bar{u}_\alpha)_{,L}) dV, \end{aligned}$$

hence

$$\begin{aligned} \int_{V^o} \bar{\theta}^o (\bar{K}_{L\alpha,L}^1 \bar{u}'_\alpha - \bar{K}_{L\alpha,L}^{1'} \bar{u}_\alpha) dV &= \int_{S^o} \bar{\theta}^o (\bar{K}_{L\alpha}^1 \bar{u}'_\alpha - \bar{K}_{L\alpha}^{1'} \bar{u}_\alpha) N_L dS \\ - \int_{V^o} (\bar{\theta}^o)_{,L} (\bar{K}_{L\alpha}^1 \bar{u}'_\alpha - \bar{K}_{L\alpha}^{1'} \bar{u}_\alpha) dV &- \int_{V^o} \bar{\theta}^o (\bar{K}_{L\alpha}^1 (\bar{u}'_\alpha)_{,L} - \bar{K}_{L\alpha}^{1'} (\bar{u}_\alpha)_{,L}) dV. \end{aligned} \quad (87)$$

Hence by the latter equation and the constitutive relations (26), Eq.(86) becomes

$$\begin{aligned} \int_{V^o} \bar{\theta}^o (\bar{F}_\alpha \bar{u}'_\alpha - \bar{F}'_\alpha \bar{u}_\alpha) dV + \int_{S^o} \bar{\theta}^o (\bar{K}_{L\alpha}^1 \bar{u}'_\alpha - \bar{K}_{L\alpha}^{1'} \bar{u}_\alpha) N_L dS \\ + \int_{V^o} \bar{\theta}^o [\rho_o \Lambda_{L\alpha} (\bar{\theta}^{1'} \bar{u}_{\alpha,L} - \bar{\theta}^1 \bar{u}'_{\alpha,L}) + R_{LN\gamma} (\bar{u}_{\gamma,N} \bar{W}_L^{1'} - \bar{u}'_{\gamma,N} \bar{W}_L^1)] dV \\ - \int_{V^o} (\bar{\theta}^o)_{,L} (\bar{K}_{L\alpha}^1 \bar{u}'_\alpha - \bar{K}_{L\alpha}^{1'} \bar{u}_\alpha) dV = 0, \end{aligned} \quad (88)$$

which is the analogue of Eq.(54) in [2].

Next we shall make use of the heat-conduction equation (81) for both the systems of loadings, rewritten in the form

$$-\overline{\left(\frac{1}{\theta^o} Q_{M,M}^1\right)} - \rho_o \overline{\dot{\eta}^1} = -\rho_o \overline{\left(\frac{\gamma^1}{\theta^o}\right)}, \quad (89)$$

since we have

$$\overline{\dot{\eta}^o} = 0. \quad (90)$$

Hence by Eqs.(30) and (28) we obtain

$$\begin{aligned} & \left(\kappa_{LN\alpha} \frac{\overline{u_{\alpha,NL}}}{\theta^o} + \kappa_{MN}^E \frac{\overline{\phi_{,NM}^1}}{\theta^o} + \kappa_L \frac{\overline{\theta_{,L}^1}}{\theta^o} + \kappa_{MN} \frac{\overline{\theta_{,NM}^1}}{\theta^o} \right) \\ & - p \rho_o \left(\Lambda_{M\gamma} \overline{u_{\gamma,M}} - P_M \overline{\phi_{,M}^1} + \alpha \overline{\theta^1} \right) = -\rho_o \overline{\left(\frac{\gamma^1}{\theta^o}\right)}. \end{aligned} \quad (91)$$

Multiplying the latter by $\overline{\theta^o}$ we have

$$\begin{aligned} & \overline{\theta^o} \left(\kappa_{LN\alpha} \frac{\overline{u_{\alpha,NL}}}{\theta^o} + \kappa_{MN}^E \frac{\overline{\phi_{,NM}^1}}{\theta^o} + \kappa_L \frac{\overline{\theta_{,L}^1}}{\theta^o} + \kappa_{MN} \frac{\overline{\theta_{,NM}^1}}{\theta^o} \right) \\ & - p \rho_o \overline{\theta^o} \left(\Lambda_{M\gamma} \overline{u_{\gamma,M}} - P_M \overline{\phi_{,NM}^1} + \alpha \overline{\theta^1} \right) = -\overline{\theta^o} \rho_o \overline{\left(\frac{\gamma^1}{\theta^o}\right)}. \end{aligned} \quad (92)$$

Write the latter equality for both the states, multiply the first equation by $\overline{\theta^{1'}}$ and the second by $\overline{\theta^1}$; we obtain

$$\begin{aligned} & \overline{\theta^{1'} \theta^o} \left(\kappa_{LN\alpha} \frac{\overline{u_{\alpha,NL}}}{\theta^o} + \kappa_{MN}^E \frac{\overline{\phi_{,NM}^1}}{\theta^o} + \kappa_L \frac{\overline{\theta_{,L}^1}}{\theta^o} + \kappa_{MN} \frac{\overline{\theta_{,NM}^1}}{\theta^o} \right) \\ & - p \rho_o \overline{\theta^{1'} \theta^o} \left(\Lambda_{M\gamma} \overline{u_{\gamma,M}} - P_M \overline{\phi_{,NM}^1} + \alpha \overline{\theta^1} \right) = -\overline{\theta^{1'} \theta^o} \rho_o \overline{\left(\frac{\gamma^1}{\theta^o}\right)}, \end{aligned} \quad (93)$$

and

$$\begin{aligned} & \overline{\theta^1 \theta^o} \left(\kappa_{LN\alpha} \frac{\overline{u_{\alpha,NL'}}}{\theta^o} + \kappa_{MN}^E \frac{\overline{\phi_{,MN'}^1}}{\theta^o} + \kappa_L \frac{\overline{\theta_{,L'}^1}}{\theta^o} + \kappa_{MN} \frac{\overline{\theta_{,MN'}^1}}{\theta^o} \right) \\ & - p \rho_o \overline{\theta^1 \theta^o} \left(\Lambda_{M\gamma} \overline{u'_{\gamma,M}} - P_M \overline{\phi_{,M'}^1} + \alpha \overline{\theta^{1'}} \right) = -\overline{\theta^1 \theta^o} \rho_o \overline{\left(\frac{\gamma^{1'}}{\theta^o}\right)}. \end{aligned} \quad (94)$$

By taking the integral over V of the difference between the last two equations, we obtain the analogue of Eq.(57) in [2], that is,

$$\kappa_{LN\alpha} \int_{V^o} \overline{\theta^o} \left(\overline{\theta^{1'} \frac{u_{\alpha,NL}}{\theta^o}} - \overline{\theta^1 \frac{u'_{\alpha,NL}}{\theta^o}} \right) dV + \kappa_{MN}^E \int_{V^o} \overline{\theta^o} \left(\overline{\theta^{1'} \frac{\phi_{,MN}^1}{\theta^o}} - \overline{\theta^1 \frac{\phi_{,M'}^1}{\theta^o}} \right) dV +$$

$$\begin{aligned}
& \kappa_L \int_{V^o} \bar{\theta}^o \left(\overline{\theta^{1'} \frac{\theta^1}{\theta^o}} - \overline{\theta^1 \frac{\theta^{1'}}{\theta^o}} \right) dV + \kappa_{MN} \int_{V^o} \bar{\theta}^o \left(\overline{\theta^{1'} \frac{\theta^{1, NM}}{\theta^o}} - \overline{\theta^1 \frac{\theta^{1', M}}{\theta^o}} \right) dV + \\
& + p \int_{V^o} \bar{\rho}_o \bar{\theta}^o \left[\overline{\theta^{1'}} \left(-\Lambda_{M\gamma} \bar{u}_{\gamma, M} - P_M \bar{W}_M \right) + \overline{\theta^1} \left(\Lambda_{M\gamma} \bar{u}'_{\gamma, M} + P_M \bar{W}'_M \right) \right] dV + \\
& + \int_{V^o} \rho_o \bar{\theta}^o \left(\overline{\theta^1 \frac{\gamma^{1'}}{\theta^o}} - \overline{\theta^{1'} \frac{\gamma^1}{\theta^o}} \right) dV = 0.
\end{aligned} \tag{95}$$

Finally, we make use of the equation for the electric field

$$\overline{\Delta^1}_{L,L} = 0, \quad \overline{\Delta^{1'}}_{L,L} = 0. \tag{96}$$

Multiplying both by $\bar{\theta}^o$, the first by $\bar{\phi}'$, the second by $\bar{\phi}$, subtracting the results and integrating over the region of the body, we obtain

$$\int_{V^o} \left(\overline{\Delta^1}_{L,L} (\bar{\theta}^o \bar{\phi}^{1'}) - \overline{\Delta^{1'}}_{L,L} (\bar{\theta}^o \bar{\phi}^1) \right) dV = 0. \tag{97}$$

By the identity (75) we have

$$\int_{S^o} \bar{\theta}^o \left(\overline{\Delta^1}_L \bar{\phi}^{1'} - \overline{\Delta^{1'}}_L \bar{\phi}^1 \right) N_L dS - \int_{V^o} \left[\overline{\Delta^1}_L (\bar{\theta}^o \bar{\phi}^{1'})_{,L} - \overline{\Delta^{1'}}_L (\bar{\theta}^o \bar{\phi}^1)_{,L} \right] dV = 0, \tag{98}$$

and thus

$$\begin{aligned}
& \int_{S^o} \bar{\theta}^o \left(\overline{\Delta^1}_L \bar{\phi}^{1'} - \overline{\Delta^{1'}}_L \bar{\phi}^1 \right) N_L dS - \int_{V^o} (\bar{\theta}^o)_{,L} \left(\overline{\Delta^1}_L \bar{\phi}^{1'} - \overline{\Delta^{1'}}_L \bar{\phi}^1 \right) dV \\
& - \int_{V^o} \bar{\theta}^o \left[\overline{\Delta^1}_L (\bar{\phi}^{1'})_{,L} - \overline{\Delta^{1'}}_L (\bar{\phi}^1)_{,L} \right] dV = 0, \tag{99}
\end{aligned}$$

$$\begin{aligned}
& \int_{S^o} \bar{\theta}^o \left(\overline{\Delta^1}_L \bar{\phi}^{1'} - \overline{\Delta^{1'}}_L \bar{\phi}^1 \right) N_L dS - \int_{V^o} (\bar{\theta}^o)_{,L} \left(\overline{\Delta^1}_L \bar{\phi}^{1'} - \overline{\Delta^{1'}}_L \bar{\phi}^1 \right) dV \\
& + \int_{V^o} \bar{\theta}^o \left(\overline{\Delta^1}_L \bar{W}_L^{1'} - \overline{\Delta^{1'}}_L \bar{W}_L^1 \right) dV = 0. \tag{100}
\end{aligned}$$

Now we substitute the constitutive relation

$$\overline{\Delta^1}_L = R_{LN\gamma} \bar{u}_{\gamma, N} - L_{LN} \bar{\phi}^1_{,N} + \rho_o P_L \bar{\theta}^1$$

in the third integral of the last equation. We obtain

$$\begin{aligned}
& \int_{S^o} \bar{\theta}^o \left(\overline{\Delta^1}_L \bar{\phi}^{1'} - \overline{\Delta^{1'}}_L \bar{\phi}^1 \right) N_L dS - \int_{V^o} (\bar{\theta}^o)_{,L} \left(\overline{\Delta^1}_L \bar{\phi}^{1'} - \overline{\Delta^{1'}}_L \bar{\phi}^1 \right) dV + \\
& \int_{V^o} \bar{\theta}^o \left[\left(R_{LN\gamma} \bar{u}_{\gamma, N} - L_{LN} \bar{\phi}^1_{,N} + \rho_o P_L \bar{\theta}^1 \right) \bar{W}_L^{1'} - \left(R_{LN\gamma} \bar{u}'_{\gamma, N} - L_{LN} \bar{\phi}^{1'}_{,N} + \rho_o P_L \bar{\theta}^{1'} \right) \bar{W}_L^1 \right] dV = 0 \tag{101}
\end{aligned}$$

Thus

$$\begin{aligned} & \int_{S^o} \bar{\theta}^o (\overline{\Delta^1_L \phi^{1'}} - \overline{\Delta^1_L \phi^1}) N_L dS - \int_{V^o} (\bar{\theta}^o)_{,L} (\overline{\Delta^1_L \phi^{1'}} - \overline{\Delta^1_L \phi^1}) dV \\ & + \int_{V^o} \bar{\theta}^o [R_{LN\gamma} (\overline{u_{\gamma,N} W^{1'}_L} - \overline{u'_{\gamma,N} W^1_L}) + \rho_o P_L (\overline{\theta^1 W^{1'}_L} - \overline{\theta^{1'} W^1_L})] dV = 0. \end{aligned} \quad (102)$$

This equation is the analogue of Eq.[2, (61)].

Taking the expression for

$$\int_{V^o} \bar{\theta}^o R_{LN\gamma} (\overline{u_{\gamma,N} W^{1'}_L} - \overline{R_{LN\gamma} u'_{\gamma,N} W^1_L}) dV \quad (103)$$

deduced from (102) and inserting this into (88) yields

$$\begin{aligned} & - \int_{V^o} \bar{\theta}^o [\rho_o \Lambda_{L\alpha} (\overline{\theta^1 u'_{\alpha,L}} - \overline{\theta^{1'} u_{\alpha,L}})] dV = \\ & \int_{V^o} \bar{\theta}^o (\overline{F_\alpha u'_\alpha} - \overline{F'_\alpha u_\alpha}) dV + \int_{S^o} \bar{\theta}^o (\overline{K^1_{L\alpha} u'_\alpha} - \overline{K^{1'}_{L\alpha} u_\alpha}) N_L dS \\ & + \int_{S^o} \bar{\theta}^o (\overline{\Delta^1_L \phi^{1'}} + \overline{\Delta^1_L \phi^1}) N_L dS - \int_{V^o} (\bar{\theta}^o)_{,L} (\overline{\Delta^1_L \phi^{1'}} - \overline{\Delta^1_L \phi^1}) dV \\ & - \int_{V^o} \bar{\theta}^o \rho_o P_L (\overline{\theta^1 W^{1'}_L} - \overline{\theta^{1'} W^1_L}) dV - \int_{V^o} (\bar{\theta}^o)_{,L} (\overline{K^1_{L\alpha} u'_\alpha} - \overline{K^{1'}_{L\alpha} u_\alpha}) dV. \end{aligned} \quad (104)$$

Now inserting (104) in (95) yields

$$\begin{aligned} & \kappa_{LN\alpha} \int_{V^o} \bar{\theta}^o (\overline{\theta^{1'} \frac{u_{\alpha,NL}}{\theta^o}} - \overline{\theta^1 \frac{u'_{\alpha,NL}}{\theta^o}}) dV + \kappa_{MN}^E \int_{V^o} \bar{\theta}^o (\overline{\theta^{1'} \frac{\phi^1_{MN}}{\theta^o}} - \overline{\theta^1 \frac{\phi^{1'}_{MN}}{\theta^o}}) dV + \\ & \kappa_L \int_{V^o} \bar{\theta}^o (\overline{\theta^{1'} \frac{\theta^1_{,L}}{\theta^o}} - \overline{\theta^1 \frac{\theta^{1'}_{,L}}{\theta^o}}) dV + \kappa_{MN} \int_{V^o} \bar{\theta}^o (\overline{\theta^{1'} \frac{\theta^1_{,NM}}{\theta^o}} - \overline{\theta^1 \frac{\theta^{1'}_{,NM}}{\theta^o}}) dV + \\ & + p \int_{V^o} \bar{\rho}_o \bar{\theta}^o (-\overline{\theta^{1'} P_M W^1_M} + \overline{\theta^1 P_M W^{1'}_M}) dV \\ & + p [\int_{V^o} \bar{\theta}^o (\overline{F_\alpha u'_\alpha} - \overline{F'_\alpha u_\alpha}) dV + \int_{S^o} \bar{\theta}^o (\overline{K^1_{L\alpha} u'_\alpha} - \overline{K^{1'}_{L\alpha} u_\alpha}) N_L dS \\ & + \int_{S^o} \bar{\theta}^o (\overline{\Delta^1_L \phi^{1'}} - \overline{\Delta^1_L \phi^1}) N_L dS - \int_{V^o} (\bar{\theta}^o)_{,L} (\overline{\Delta^1_L \phi^{1'}} - \overline{\Delta^1_L \phi^1}) dV \\ & - \int_{V^o} \bar{\theta}^o \rho_o P_L (\overline{\theta^1 W^{1'}_L} - \overline{\theta^{1'} W^1_L}) dV - \int_{V^o} (\bar{\theta}^o)_{,L} (\overline{K^1_{L\alpha} u'_\alpha} - \overline{K^{1'}_{L\alpha} u_\alpha}) dV + \\ & + \int_{V^o} \rho_o \bar{\theta}^o (\overline{\theta^1 \frac{\gamma^{1'}}{\theta^o}} - \overline{\theta^{1'} \frac{\gamma^1}{\theta^o}}) dV = 0. \end{aligned} \quad (105)$$

Next in the latter equality we transform the sum of the first four integrals.

Firstly note that by (84) we have

$$\bar{1} = \int_0^\infty e^{-pt} dt = 1/p,$$

$$\begin{aligned}
\theta^o &= \theta^o(\mathbf{x}) \Rightarrow \overline{\theta^o} = \theta^o/p, \\
\overline{\left(\frac{h(\mathbf{x}, t)}{f(\mathbf{x})}\right)} &= \frac{1}{f(\mathbf{x})} \int_0^\infty e^{-pt} h(\mathbf{x}, t) dt = \frac{1}{f(\mathbf{x})} \overline{h(\mathbf{x}, t)}, \\
\kappa_{\dots} \int_{V^o} \overline{\theta^o} \left(\overline{\frac{f'_{\dots}}{\theta^o}} - \overline{\theta^1} \overline{\frac{f'_{\dots}}{\theta^o}} \right) dV &= \frac{\kappa_{\dots}}{p} \int_{V^o} \left(\overline{\theta^{1'}} \overline{f'_{\dots}} - \overline{\theta^1} \overline{f'_{\dots}} \right) dV.
\end{aligned} \tag{106}$$

Hence by these equalities and the constitutive relation for the incremental heat flux (30), the aforementioned sum of the four integrals equals

$$\frac{1}{p} \int_{V^o} \left(\overline{\theta^{1'}} \overline{Q_{L,L}^1} - \overline{\theta^1} \overline{Q_{L,L}^1} \right) dV. \tag{107}$$

Again by the identity

$$ab_{,ML} = (ab_{,M})_{,L} - a_{,L}b_{,M}$$

and the divergence theorem, the sum (107) equals

$$\frac{1}{p} \left[\int_{S^o} \left(\overline{\theta^{1'}} \overline{Q_L^1} - \overline{\theta^1} \overline{Q^{1'}_L} \right) N_L dS - \int_{V^o} \left(\overline{\theta^{1'}_{,L}} \overline{Q_L^1} - \overline{\theta^1_{,L}} \overline{Q^{1'}_L} \right) dV \right]. \tag{108}$$

By substituting the sum of the first four integrals in Eq.(105) by (108), we obtain

$$\begin{aligned}
&\frac{1}{p} \left[\int_{S^o} \left(\overline{\theta^{1'}} \overline{Q_L^1} - \overline{\theta^1} \overline{Q^{1'}_L} \right) N_L dS - \int_{V^o} \left(\overline{\theta^{1'}_{,L}} \overline{Q_L^1} - \overline{\theta^1_{,L}} \overline{Q^{1'}_L} \right) dV \right] \\
&\quad + pP_M \int_{V^o} \overline{\rho_o} \overline{\theta^o} \left(-\overline{\theta^{1'} W_M^1} + \overline{\theta^1 W_M^{1'}} \right) dV \\
&\quad + p \left[\int_{V^o} \overline{\theta^o} \left(\overline{F_\alpha} \overline{u'_\alpha} - \overline{F'_\alpha} \overline{u_\alpha} \right) dV + \int_{S^o} \overline{\theta^o} \left(\overline{K_{L\alpha}^1} \overline{u'_\alpha} - \overline{K_{L\alpha}^{1'}} \overline{u_\alpha} \right) N_L dS \right. \\
&\quad + \int_{S^o} \overline{\theta^o} \left(\overline{\Delta^1_L} \overline{\phi^{1'}} - \overline{\Delta^{1'}_L} \overline{\phi^1} \right) N_L dS - \int_{V^o} (\overline{\theta^o})_{,L} \left(\overline{\Delta^1_L} \overline{\phi^{1'}} - \overline{\Delta^{1'}_L} \overline{\phi^1} \right) dV \\
&\quad \left. - \int_{V^o} \overline{\theta^o} \rho_o P_L \left(\overline{\theta^1} \overline{W_L^{1'}} - \overline{\theta^{1'}} \overline{W_L^1} \right) dV - \int_{V^o} (\overline{\theta^o})_{,L} \left(\overline{K_{L\alpha}^1} \overline{u'_\alpha} - \overline{K_{L\alpha}^{1'}} \overline{u_\alpha} \right) dV + \right. \\
&\quad \left. + \int_{V^o} \rho_o \left(\overline{\theta^1} \overline{\gamma^{1'}} - \overline{\theta^{1'}} \overline{\gamma^1} \right) dV = 0. \tag{109}
\end{aligned}$$

The latter is the final form of the *theorem of reciprocity of work*, containing all causes and effects. It generalizes Eq.[2, (62)], and reduces exactly to the latter in case of vanishing initial fields, that is, when the initial configuration is natural.

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